



MOD 3^eA, ECL'16 & École doctorale MEGA

Physique des écoulements turbulents

Christophe Bailly

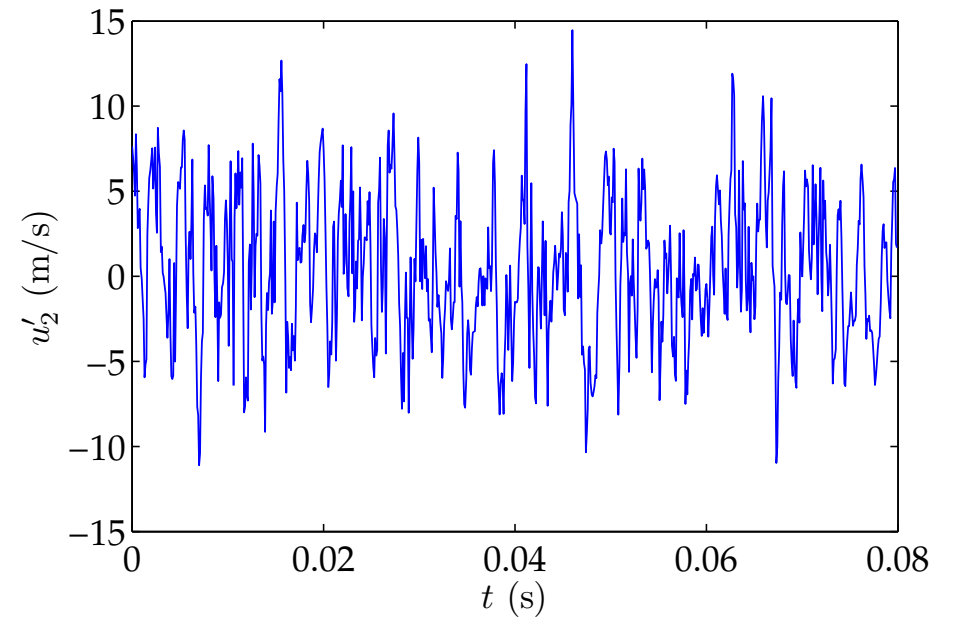
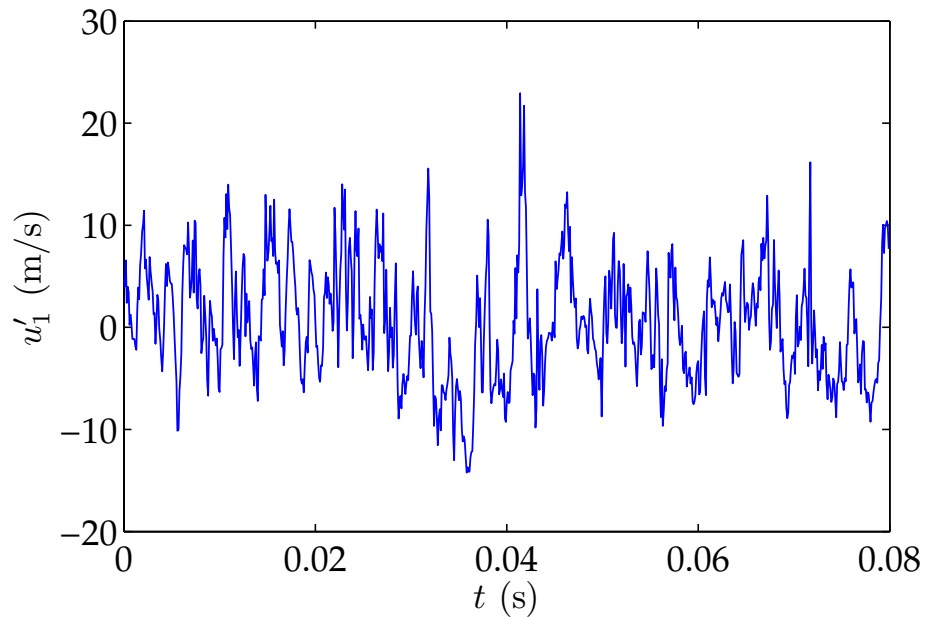
Université de Lyon, Ecole Centrale de Lyon & LMFA - UMR CNRS 5509

<http://acoustique.ec-lyon.fr>

- Subsonic round jet, nozzle diameter $D = 50$ mm, exit velocity $U_j = 30$ m.s⁻¹
 \leadsto Reynolds number $Re_D = 10^5$

$u'_1(t)$ and $u'_2(t)$ at $x_2 = D/2$ and $x_3 = 0$ ($x_1 = 2D$)

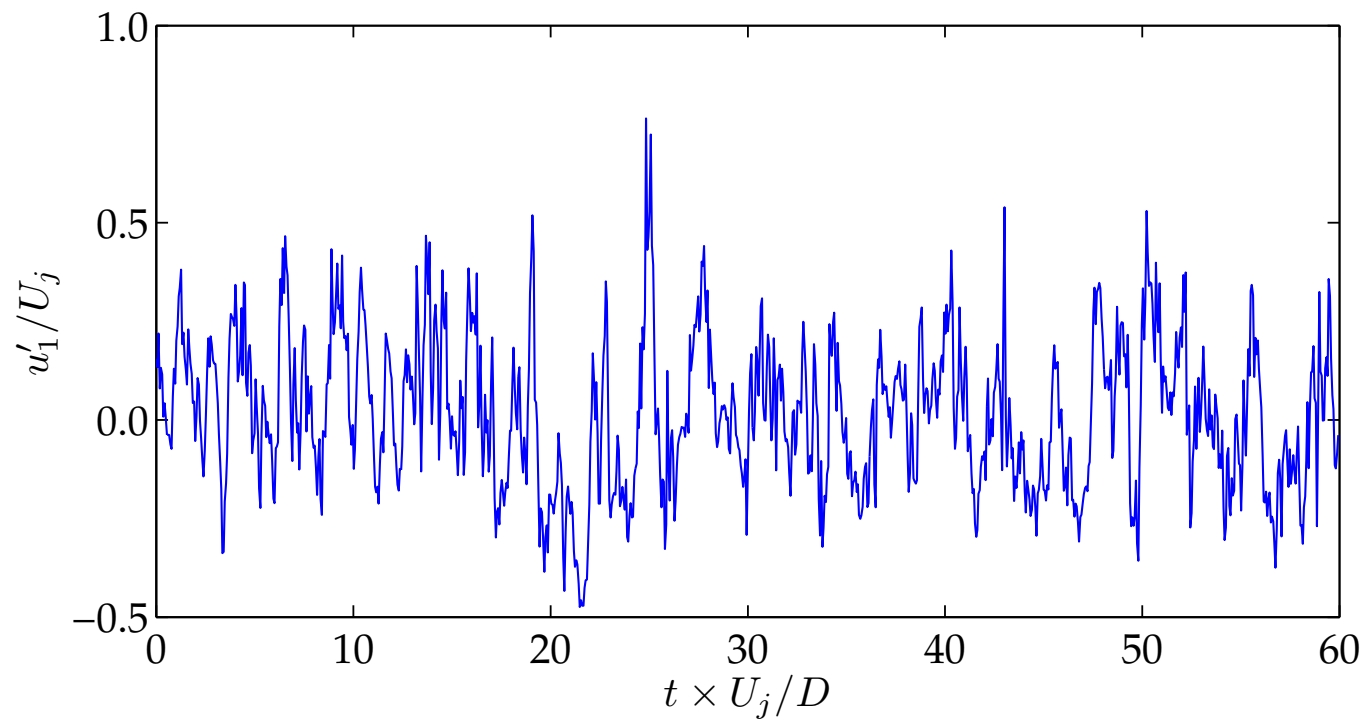
measured by crossed-wire probes (hot wire anemometer)



Courtesy of Emmanuel Jondeau (LMFA) for the data

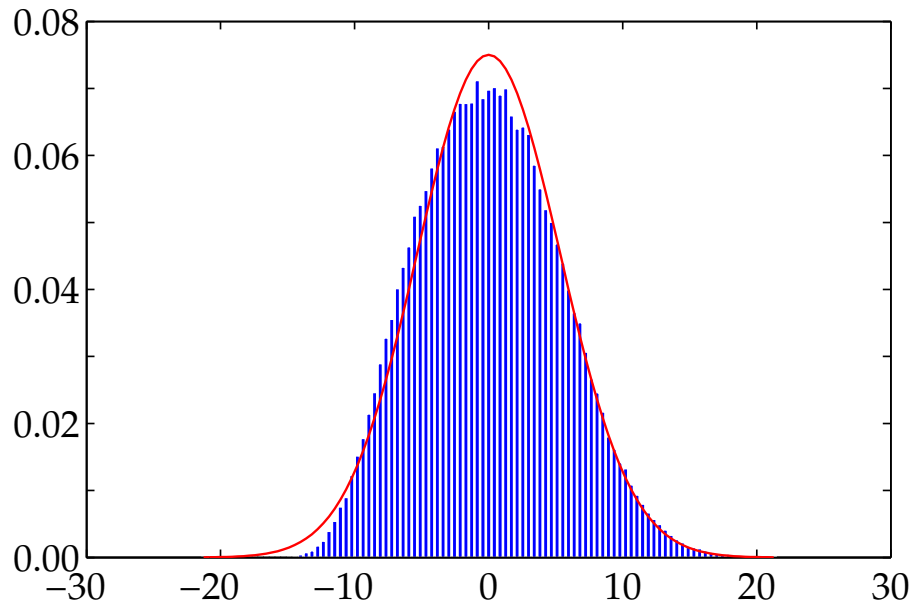
- Subsonic round jet, nozzle diameter $D = 50$ mm, exit velocity $U_j = 30$ m.s⁻¹
 \leadsto Reynolds number $Re_D = 10^5$

$$u'_1(t) \text{ at } x_2 = D/2 \text{ and } x_3 = 0 \quad (x_1 = 2D)$$

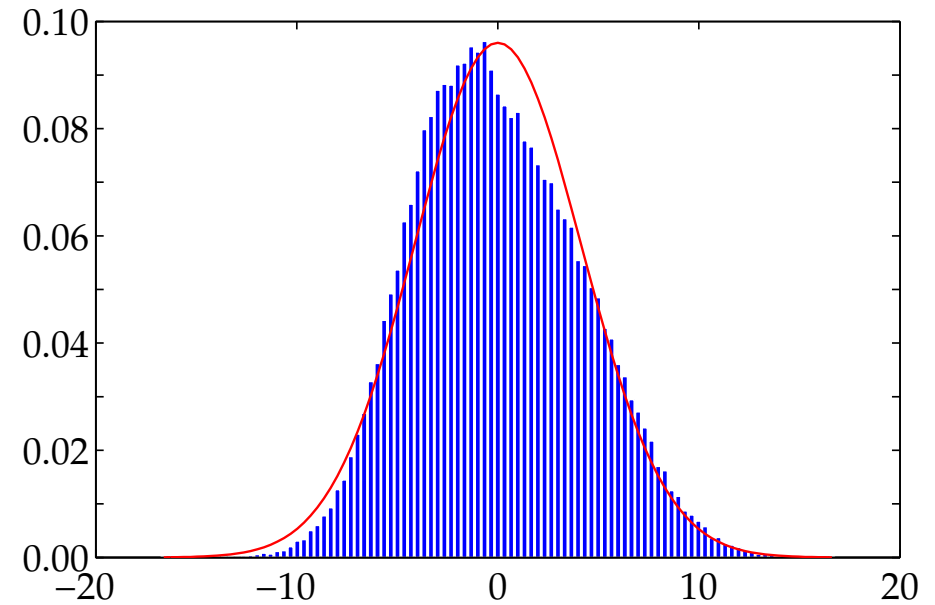


● Probability density functions

pdf of $u'_1(t)$ and $u'_2(t)$ at $x_2 = D/2$ and $x_3 = 0$



$$S_{u'_1} \simeq 0.21 \quad T_{u'_1} \simeq 2.74$$



$$S_{u'_2} \simeq 0.24 \quad T_{u'_2} \simeq 2.76$$

— Gaussian or normal distribution $p(\xi) = \frac{1}{\sqrt{2\pi}\sigma_\xi} \exp\left(-\frac{\xi^2}{2\sigma_\xi^2}\right)$

$$\sigma_\xi \equiv \sqrt{(\xi - \bar{\xi})^2} \quad S_\xi = 0 \quad T_\xi = 3$$

● **Skewness and flatness or kurtosis factors**

centered variable $x'_i = x_i - \bar{X}_i$, $x'_{i,rms} = \sqrt{\overline{x_i'^2}} = \sigma_{x_i}$

$$S_{x_i} \equiv \frac{\overline{x_i'^3}}{x_{i,rms}^3} \quad T_x \equiv \frac{\overline{x_i'^4}}{x_{i,rms}^4}$$

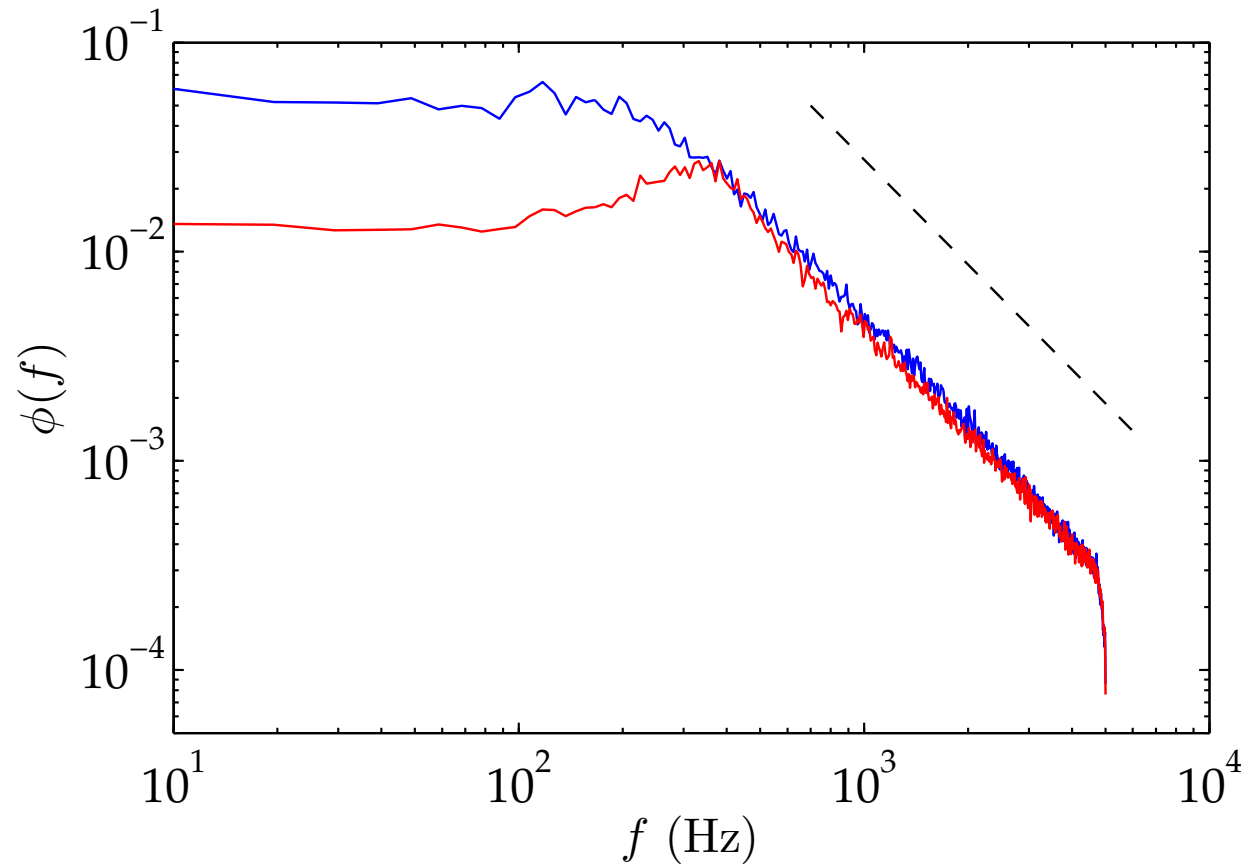
● **Reynolds stress tensor in the shear layer**

$$\frac{\sqrt{\overline{|u'_i u'_j|}}}{U_j} \simeq \begin{pmatrix} 0.18 & 0.10 & 0.10 \\ 0.10 & 0.14 & - \\ 0.10 & - & 0.13 \end{pmatrix}$$

- $\overline{u'_1 u'_2} > 0$, in agreement with Boussinesq's hypothesis
 $-\overline{u'_1 u'_2} = \nu_t \partial \bar{U}_1 / \partial x_2$ (okay, at least for the sign!)
- The Schwarz inequality is (must be!) satisfied, $|\overline{u'_1 u'_2}|^2 \leq \overline{u_1'^2} \times \overline{u_2'^2}$
- Turbulence intensity $u'/U_j \simeq 0.18$

- Spectra of u'_1 and u'_2

$f_s = 1/\Delta t = 10^4$ Hz, $n_{\text{fft}} = 1024$, $\Delta f = f_s/n_{\text{fft}}$, $f_{\text{max}} = f_s/2 = 5$ kHz



- Spectra of u'_1 and u'_2

```
%.. number of points for the Fourier transform
nfft = 1024;
```

```
dt = t(2)-t(1);
fs = 1./dt;
```

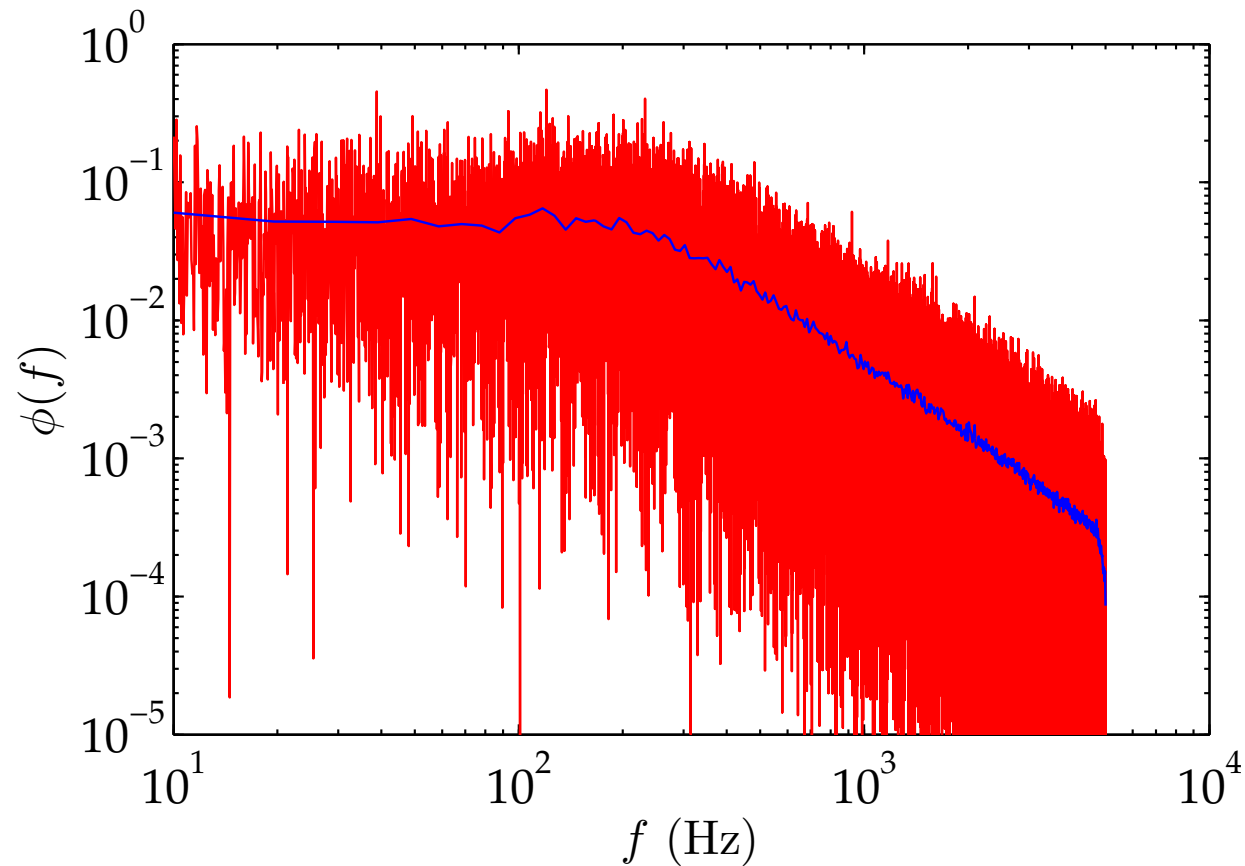
```
%.. Power spectral density
window = ones(nfft,1);
noverlap = nfft/2;
```

```
[PSDu f] = pwelch(u,window,noverlap,nfft,1./dt);
PSDu_int = trapz(f,PSDu);
```

```
disp(['PSD - Welch E = ',num2str(PSDu_int)]);
disp(['df = ',num2str(1/(nfft*dt)), ' fmax = ',num2str(1/(2*dt))]);
```

- FFT² of $u'_1(t)$ over $n_{\text{fft}} = 150000$ points (all the signal)

FFT² \neq PSD power spectral density $\phi(f)$!



● Power spectral density for a stationary random process

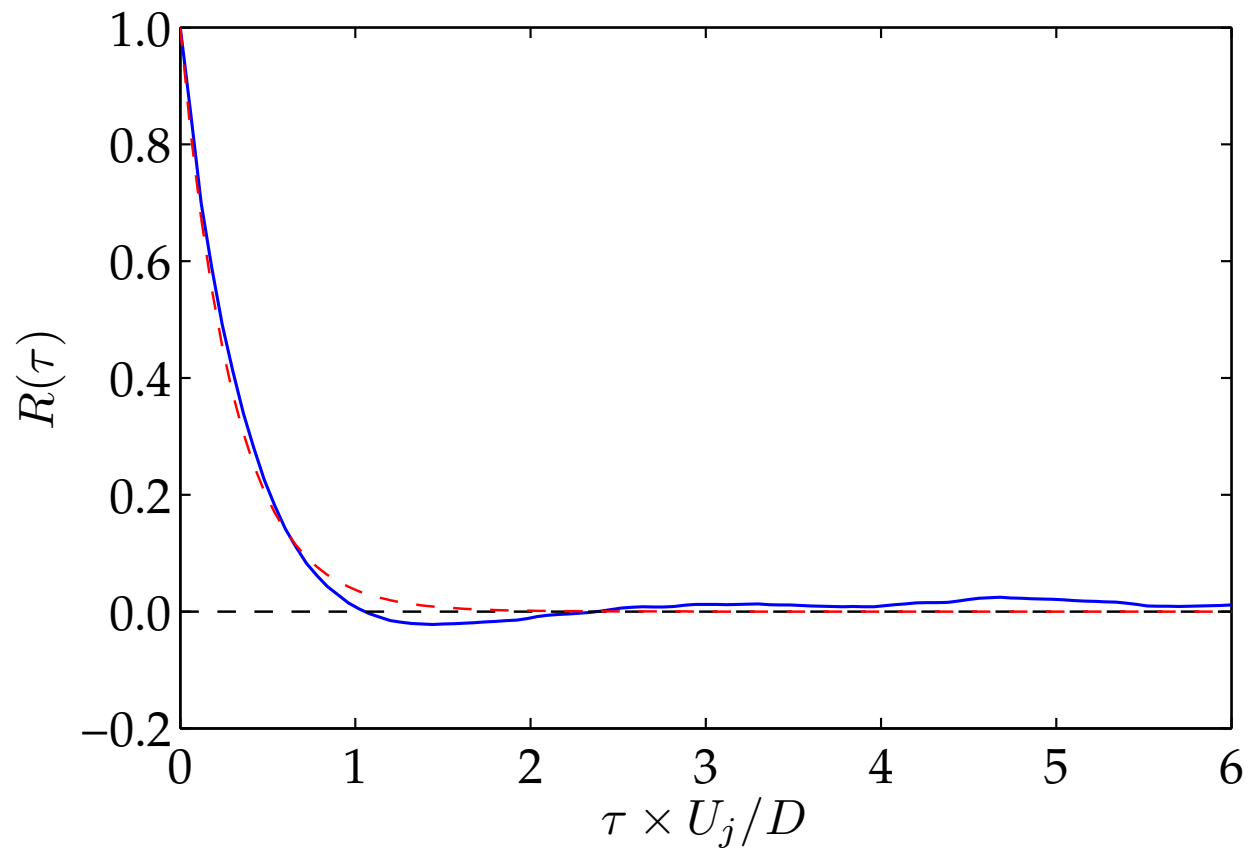
$\hat{u}_1(f, k)$ is the DFT of $u_1(t)$ for the k -th block, n_K block averages

One-sided power spectral density ($f > 0$)

$$\phi_{u_1 u_1}(f) = \lim_{T \rightarrow \infty} \frac{2}{T} E[\hat{u}_1^*(f, k) \hat{u}_1(f, k)] \simeq \frac{2}{n_K T} \sum_{k=1}^{n_K} \hat{u}_1^*(f, k) \hat{u}_1(f, k)$$

$$\int_0^{\infty} \phi_{u_1 u_1}(f) df = u_{u_1, \text{rms}}'^2 \quad (\text{Parseval})$$

● Autocorrelation function of u'_1



$$R(\tau) = \frac{\overline{u'_1(t)u'_1(t + \tau)}}{u_{1\text{rms}}'^2}$$

— $R(\tau)$

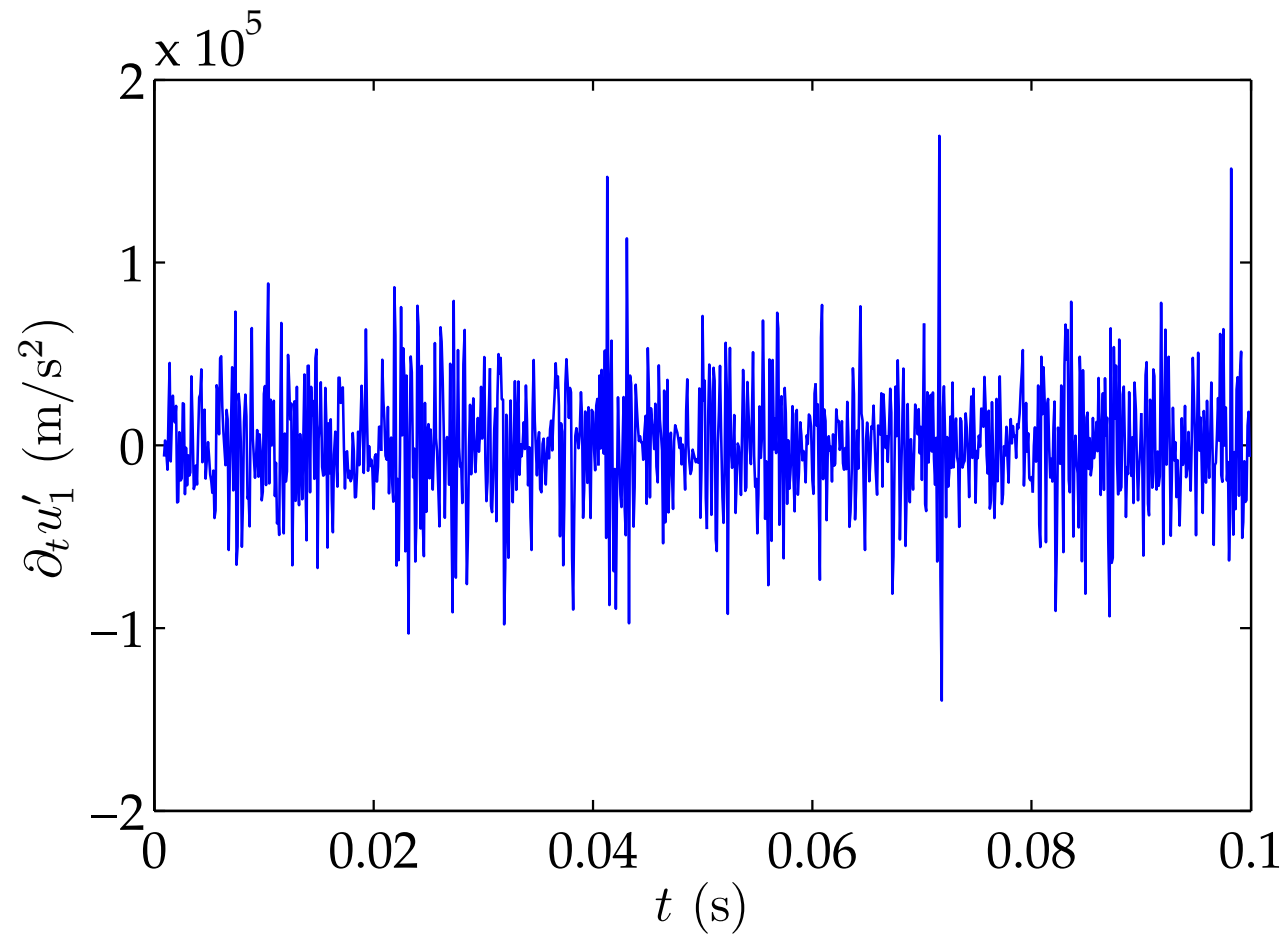
--- $\exp(-\tau/\Theta)$

$$\theta = \int_{-\infty}^{+\infty} R(\tau) d\tau$$

$$\Theta = 5 \times 10^{-4} \text{ s}, L_f \simeq \bar{U}_1 \times \Theta \simeq 1.5 \times 10^{-2} \text{ m}$$

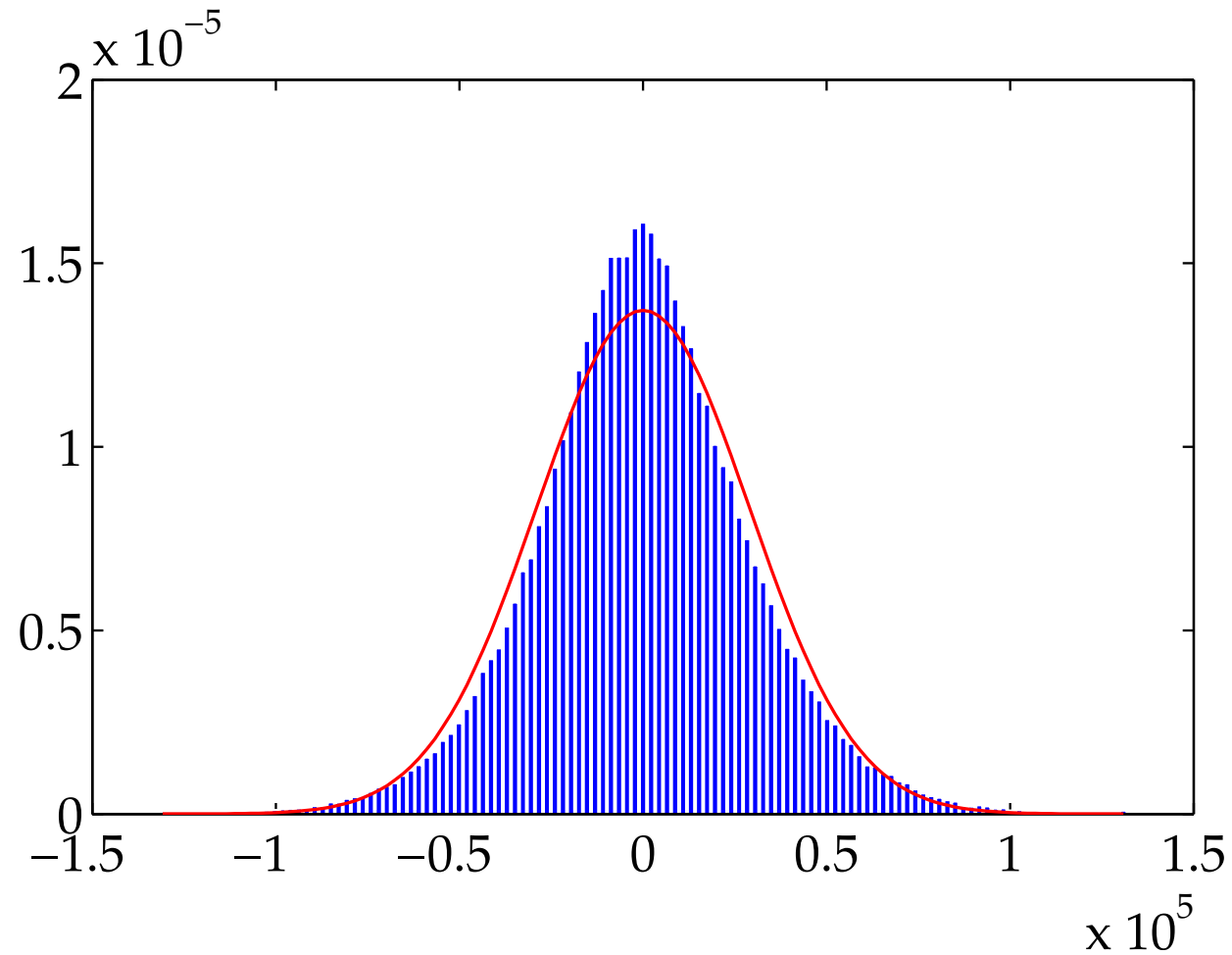
$$l_\eta \simeq 2.4 \times 10^{-5} \text{ m}, f_\eta = 2.6 \times 10^4 \text{ Hz}$$

- Time derivative of u'_1



● Probability density function of du'_1/dt

$$S_{\partial_t u'_1} \simeq 0.07 \quad T_{\partial_t u'_1} \simeq 4.03$$



● Spectrum of du'_1/dt

directly computed from du'_1/dt using a finite difference scheme (11 pts, 4th order),
 and from the spectrum of u'_1 using $\phi_{\partial_t u'_1}(f) = (2\pi f)^2 \phi_{u'_1}(f)$

