

Geneviève Comte-Bellot

Fifty Years of Research on Turbulence and Acoustics

SHOCK IMPINGEMENT AND TURBULENT WALL-BOUNDED FLOW DYNAMICS

M. F. Shahab¹, T. B. Gatski^{1,2} and P. Comte¹

¹Laboratoire d'Études Aérodynamiques

Université de Poitiers, ENSMA, CNRS

86962 Futuroscope Chasseneuil Cedex, France

²Center for Coastal Physical Oceanography and Ocean, Earth and Atmospheric Sciences

Old Dominion University, Norfolk, Virginia 23529 USA

SHOCK BOUNDARY LAYER INTERACTION (SWBLI)

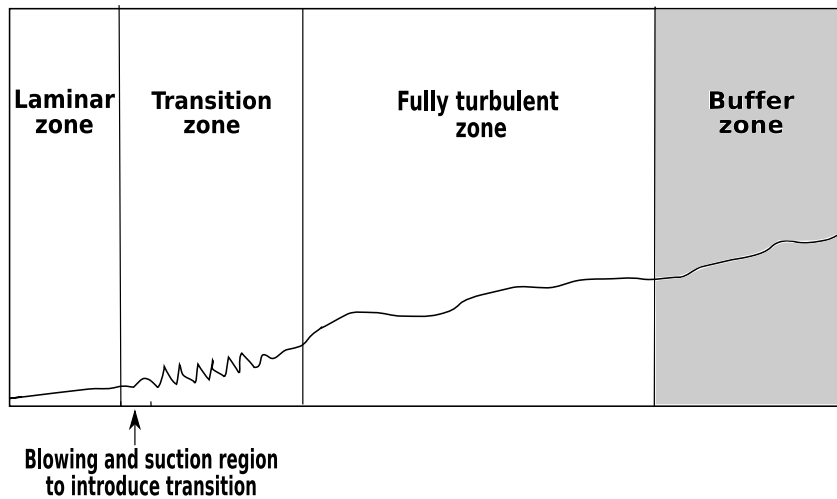
- One of the most challenging problems of high speed flow dynamics (aircrafts, rockets, and projectiles)
- Detailed understanding of phenomenon essential for efficient aerodynamics and design of propulsion system
- Characteristics
 - Unsteady, three dimensional behavior
 - Large thermodynamic fluctuation levels
 - Large variations on velocity fluctuation correlations

OBJECTIVES

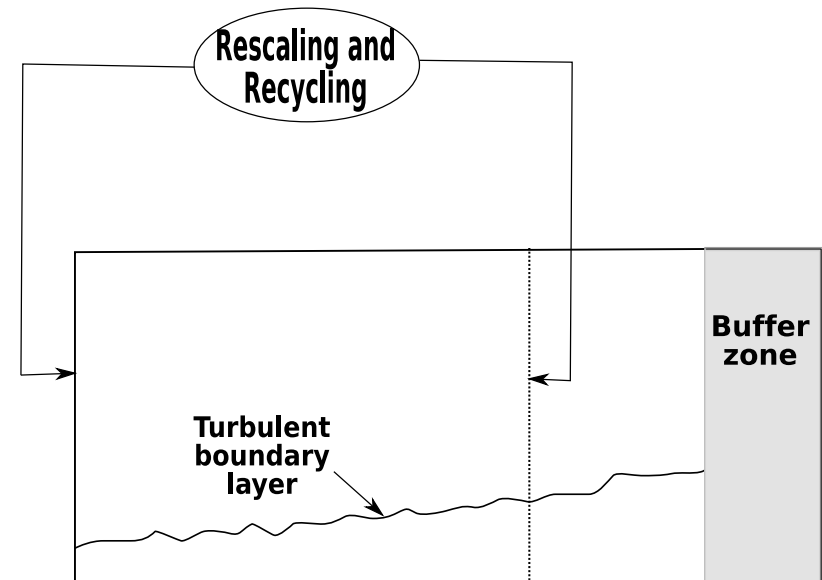
- To compare higher-order statistical moments with experimental and simulation results
- To analyze variation of turbulent structural dynamics due to interaction with shock (anisotropy invariant map and intermittency distribution)
- To show how turbulent statistical moments altered due to shock presence
- To highlight the alteration of mass and heat flux terms are influenced by shocks
- To study influence on shock wave interaction under isothermal wall conditions

DEVELOPED AND SUSTAINED TURBULENCE

- Two different techniques to generate turbulent inflow conditions for shock boundary layer interaction simulations



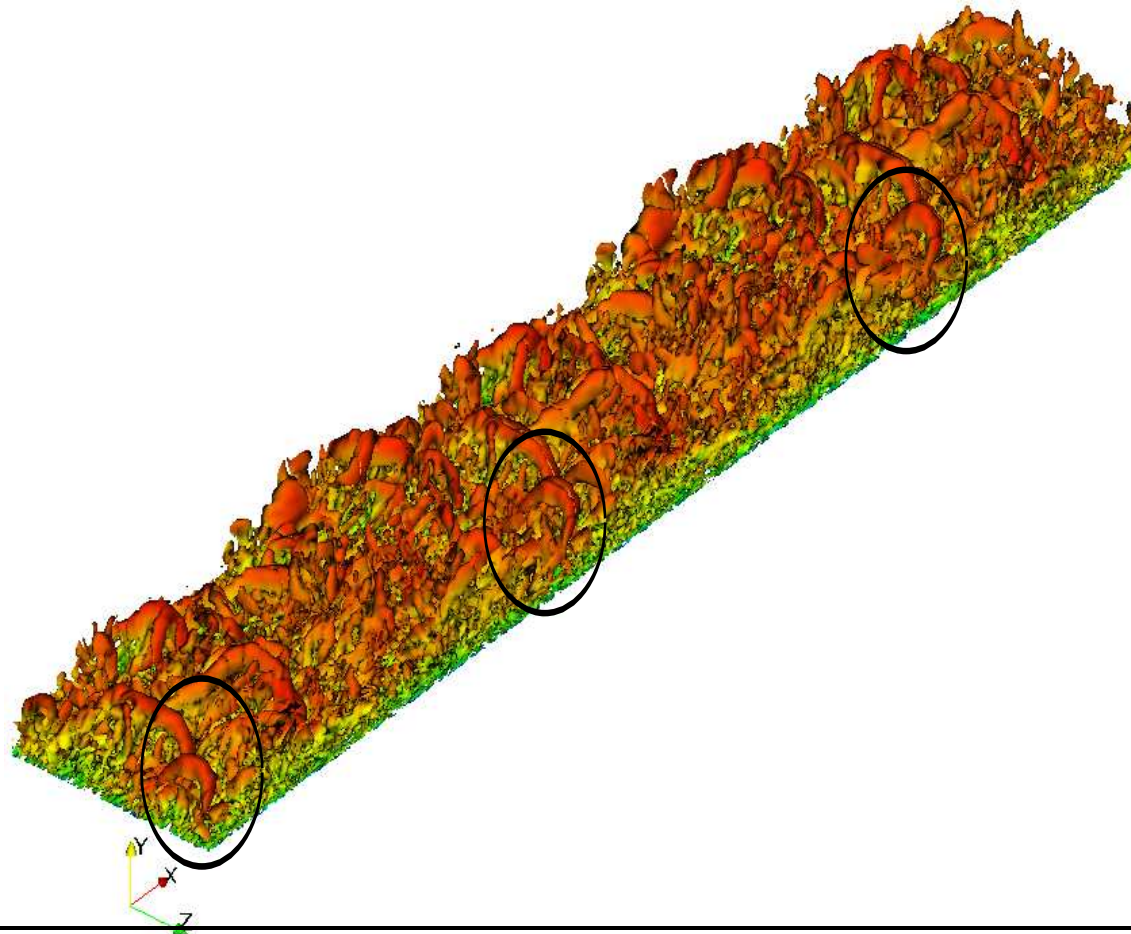
Developed



Sustained

SUSTAINED TURBULENCE CASE STUDY

- Case study based on rescaling and recycling technique proposed by Stolz and Adams (Phys. Fluids, 2003)

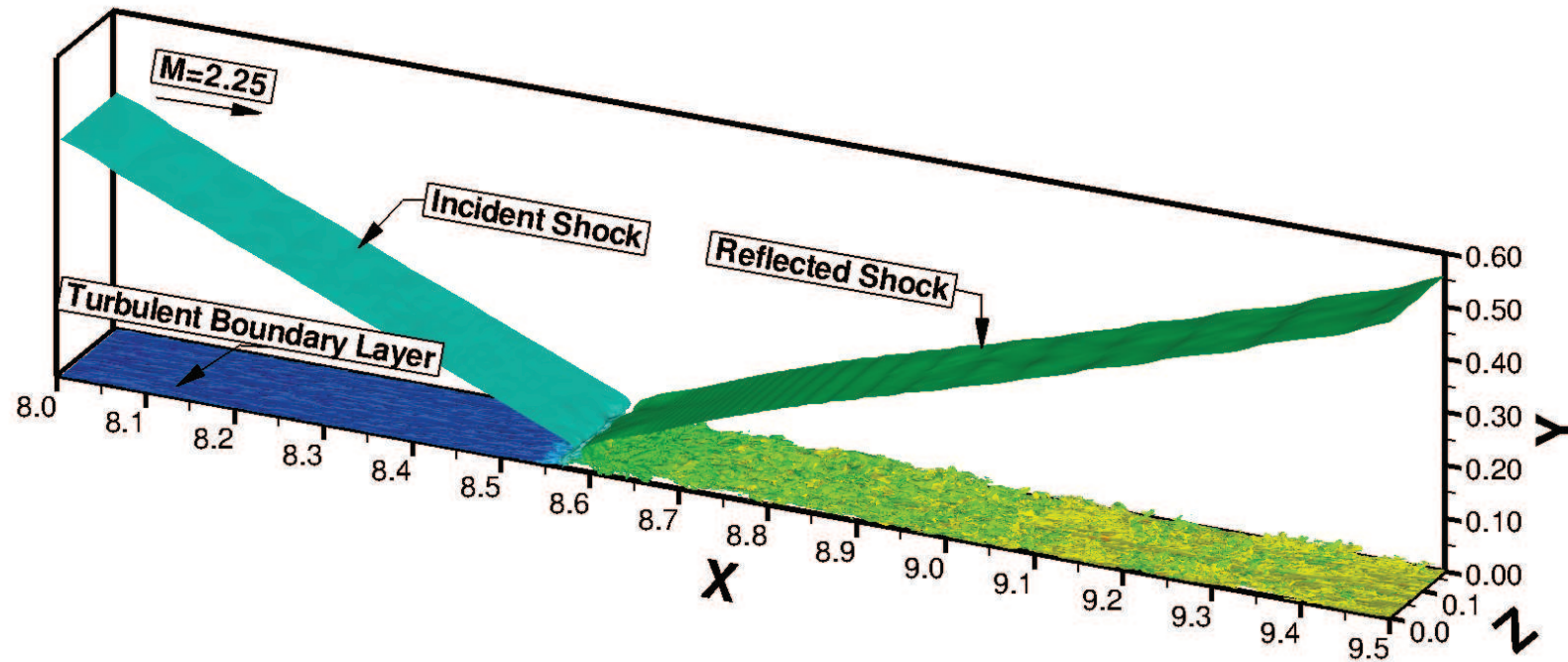


SIMULATION PARAMETERS

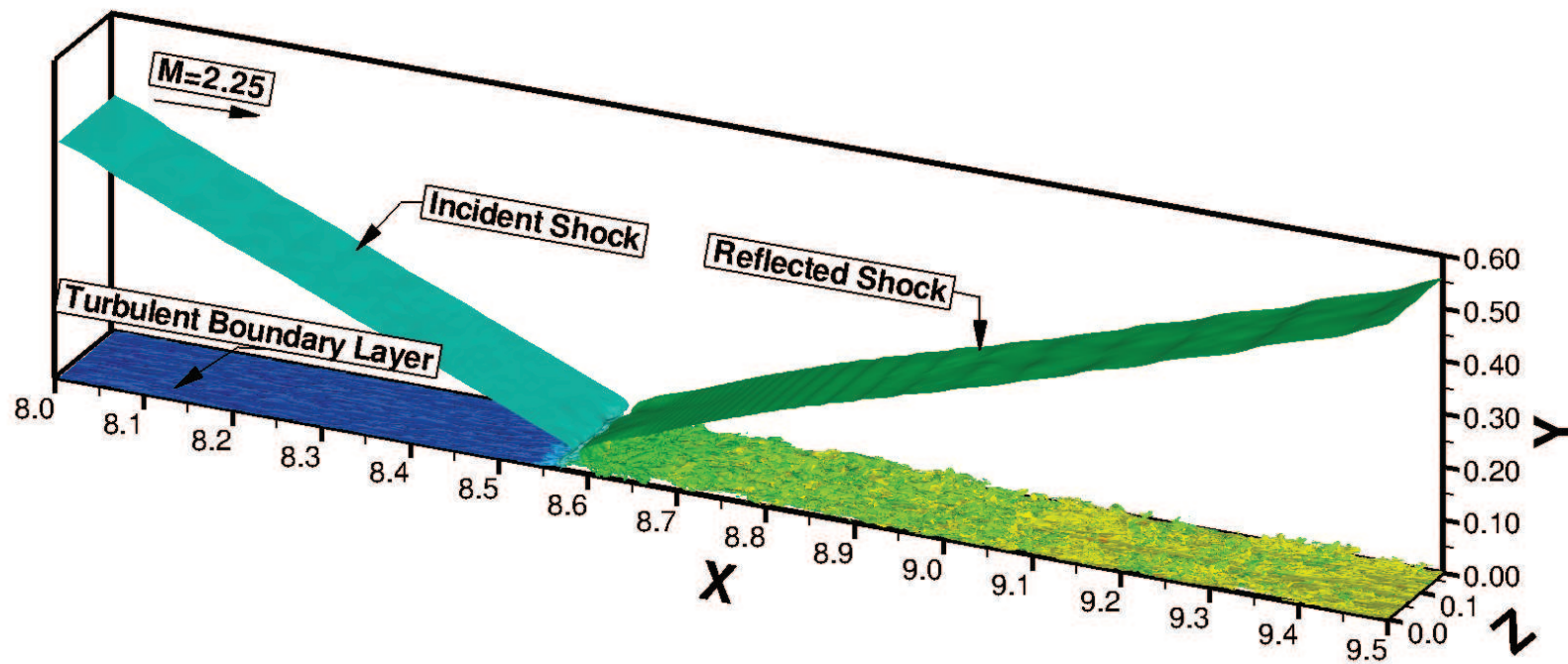
- Freestream Mach Number $M_\infty = 2.25$
- Freestream unit Reynolds number $Re/m. = 25 \times 10^6$
- Momentum Thickness Reynolds number $Re_\theta = 3133$
(*plane1*)
- Grid Points $(N_x, N_y, N_z) = (2650 \times 111 \times 255)$
- Mesh spacing in well resolved region $(\Delta x^+, \Delta y^+, \Delta z^+) = (14.1, 1.01, 6.6)$
- Shock angle α (w.r.t horizontal) = 33.2°

COMPUTATIONAL SUB-DOMAIN

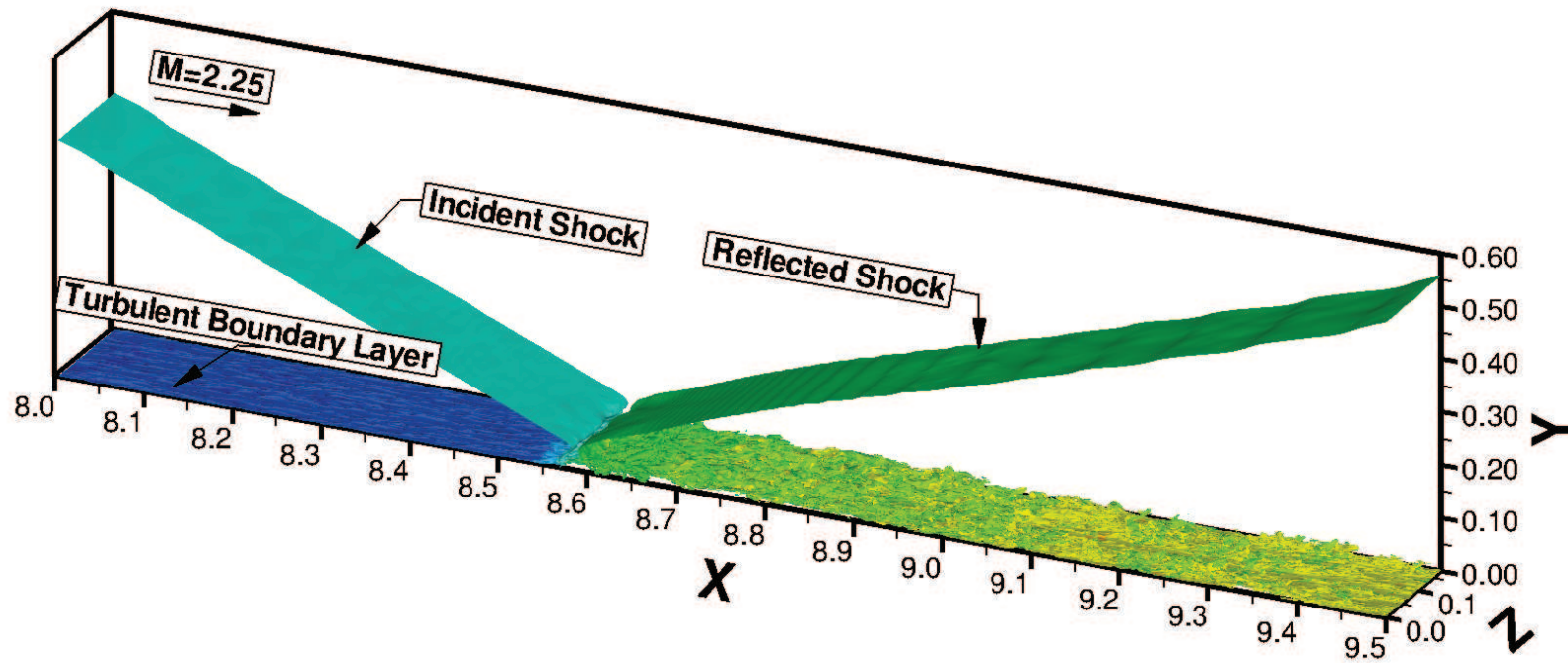
- Computational sub-domain in vicinity of the incident/reflected shock intersection (shading based on pressure levels)



SHOCK INDUCED FLOW ALTERATION

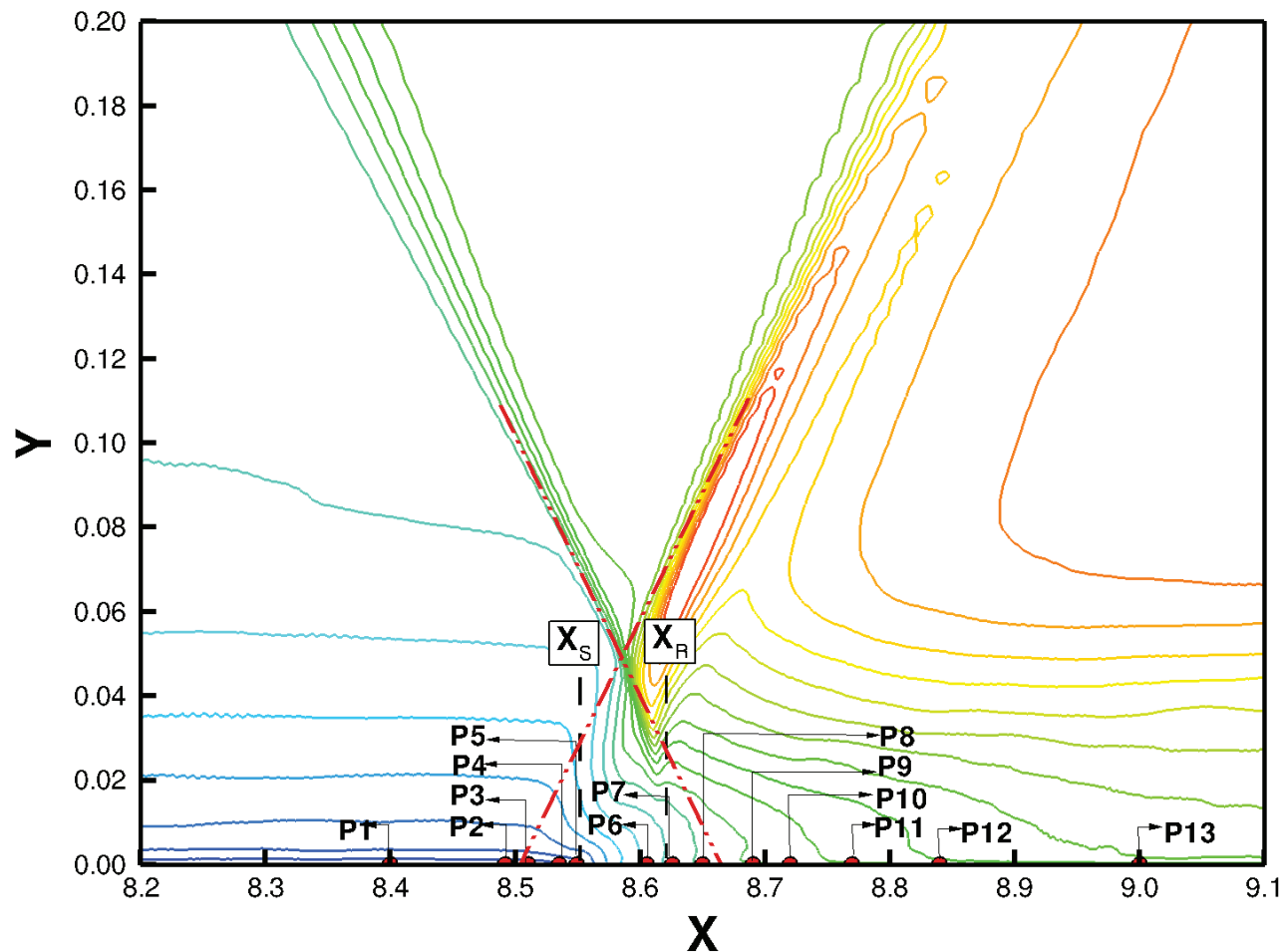


SHOCK INDUCED FLOW ALTERATION



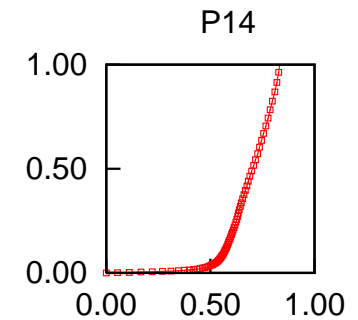
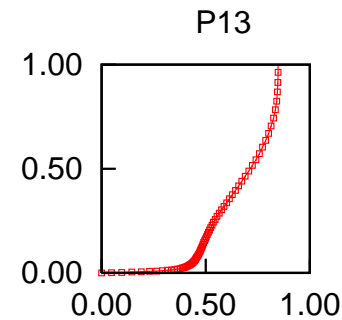
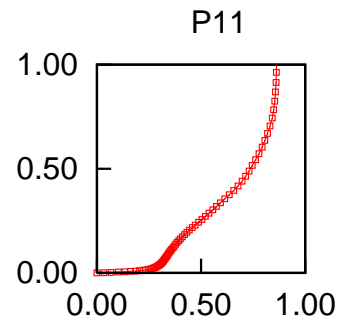
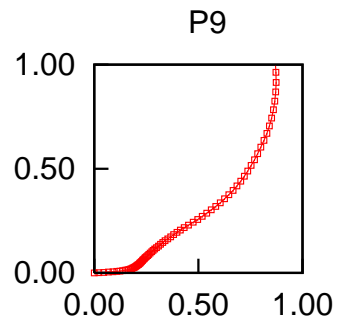
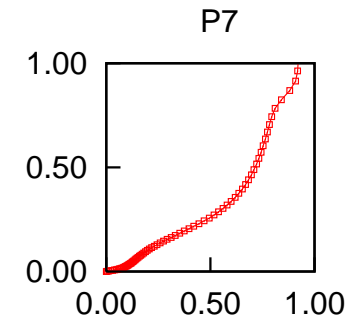
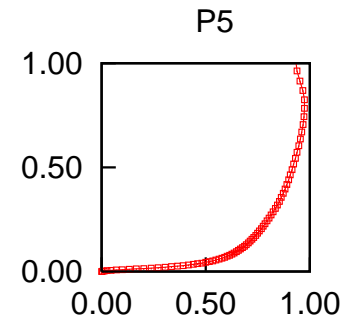
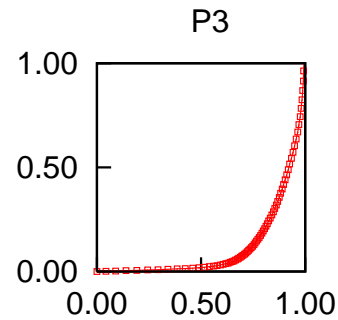
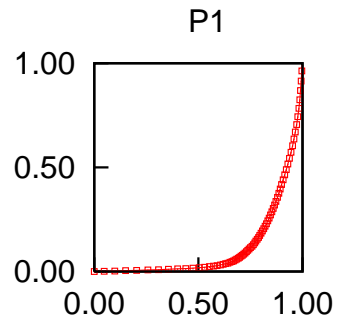
DIAGNOSTIC PLANES - POSITIONS

- Streamwise location of $y - z$ planes in proximity of separation bubble



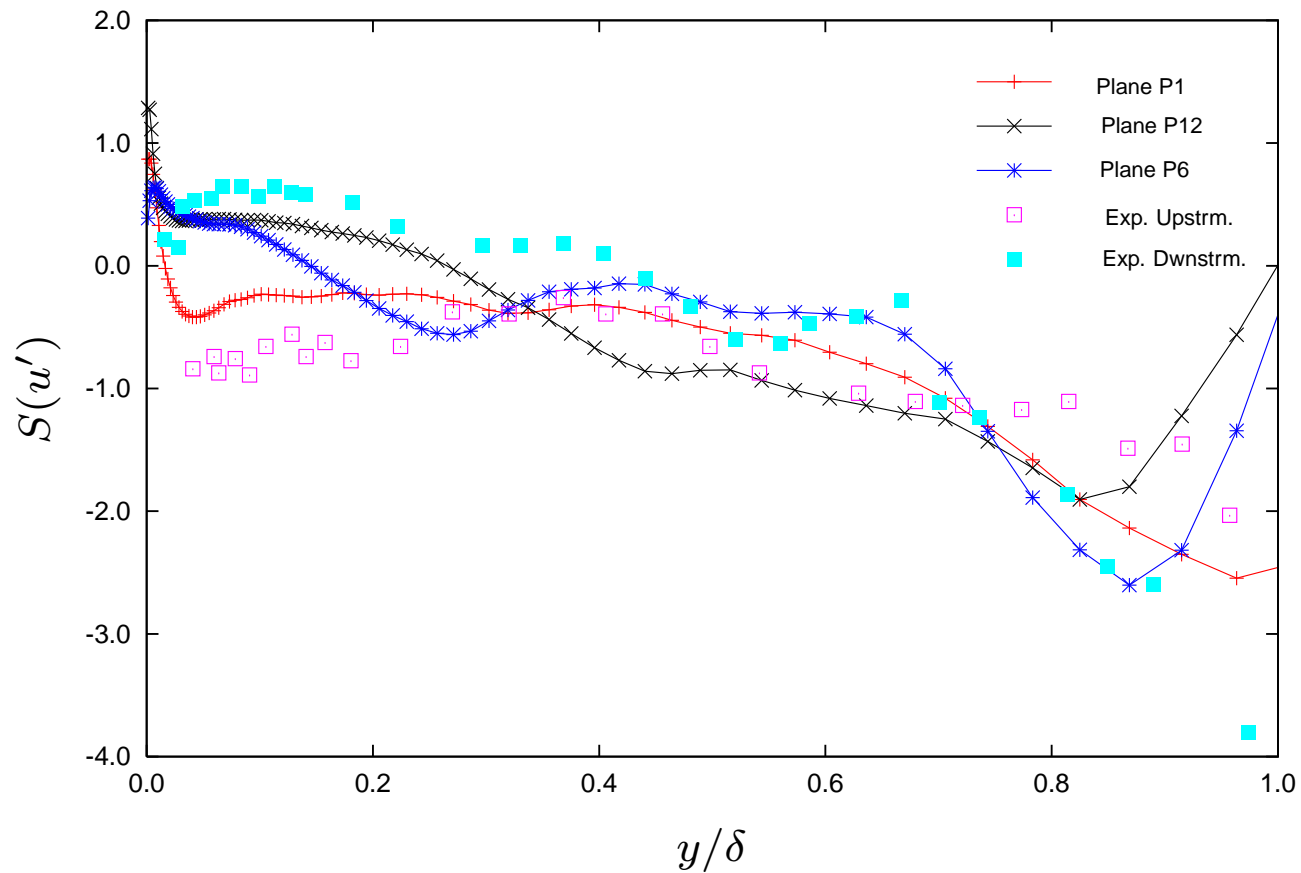
DIAGNOSTIC PLANES - POSITIONS

- Mean streamwise velocity profiles at diagnostic $y - z$ planes



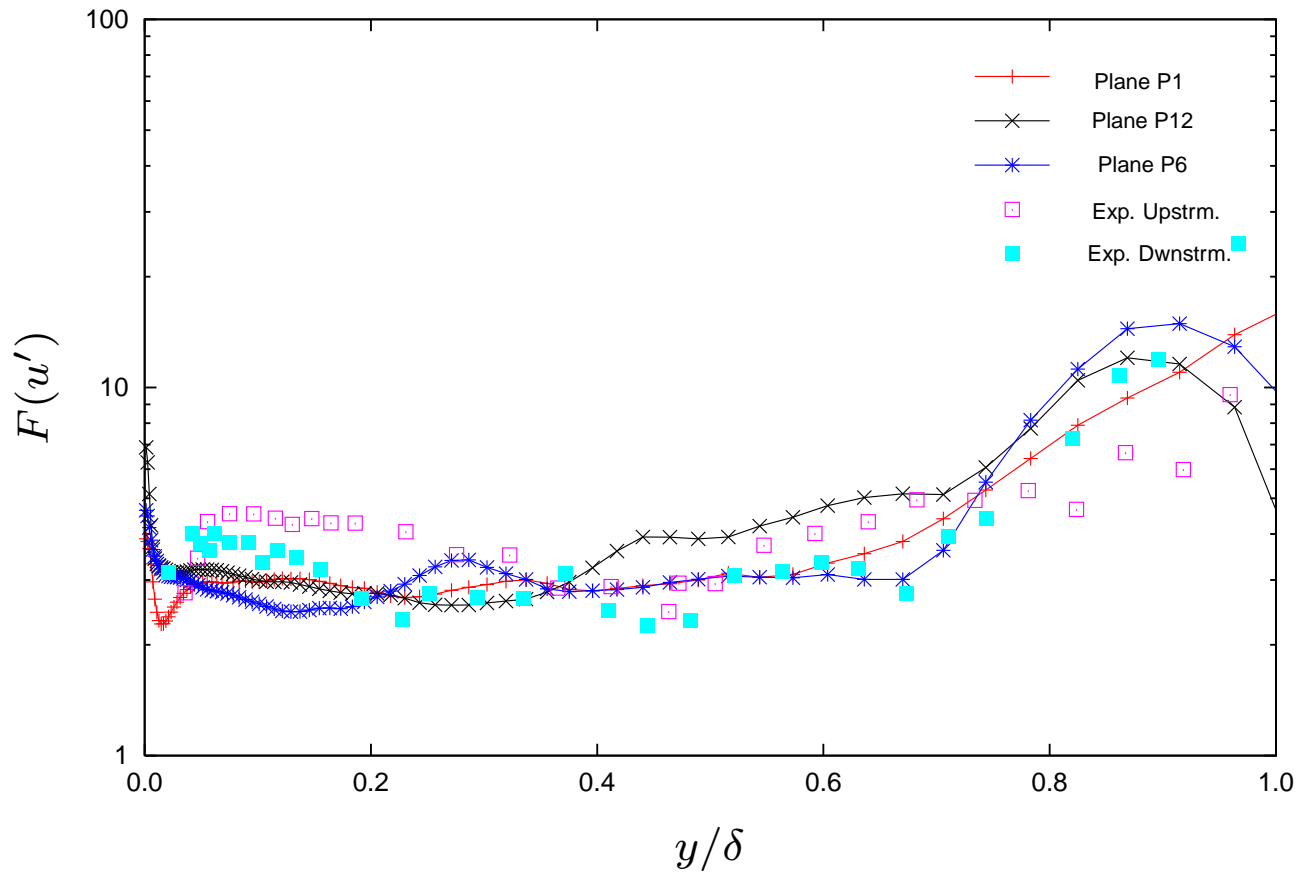
DISTRIBUTION OF SKEWNESS / FLATNESS

- Comparison of experimental (Deleuze, 1995) and simulation streamwise velocity skewness



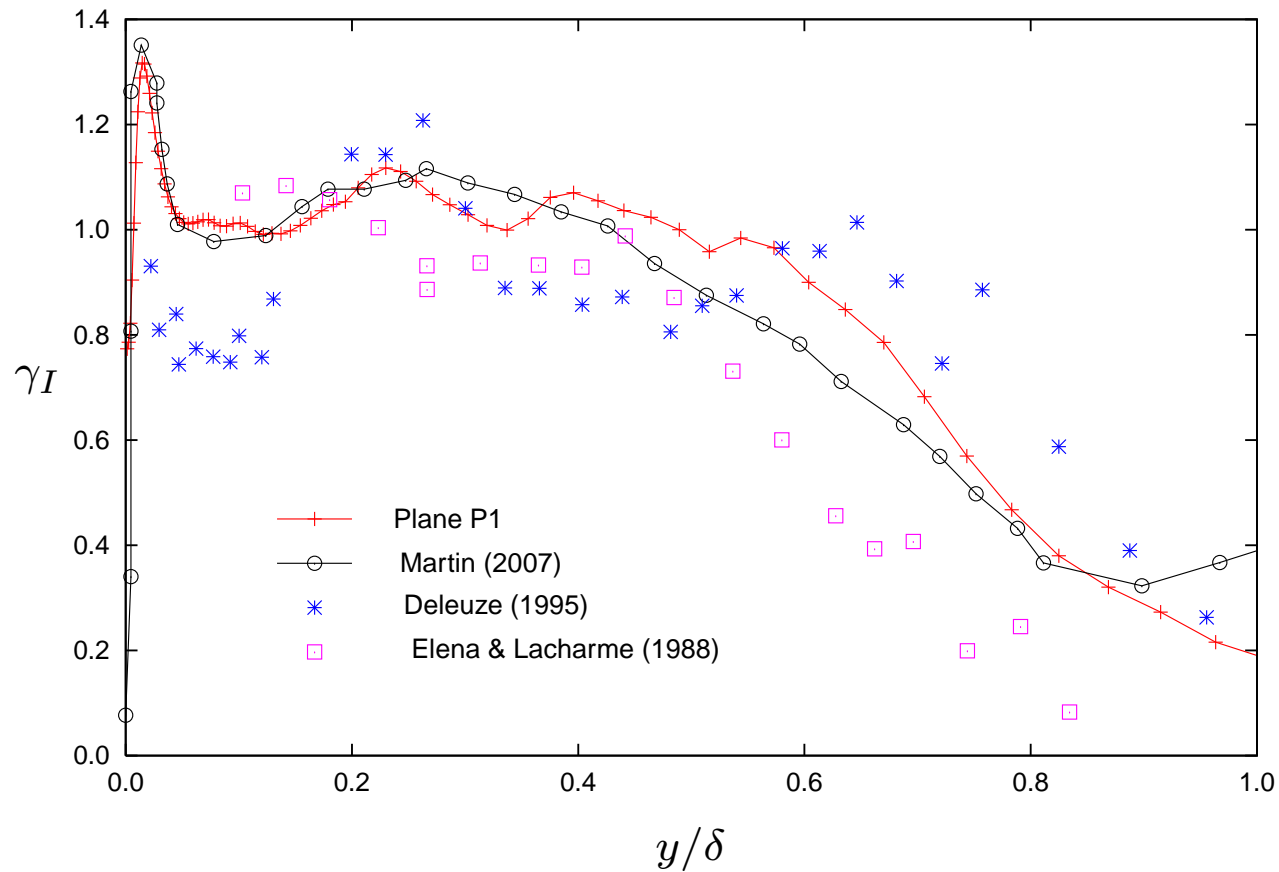
DISTRIBUTION OF SKEWNESS / FLATNESS

- Comparison of experimental (Deleuze, 1995) and simulation streamwise velocity flatness



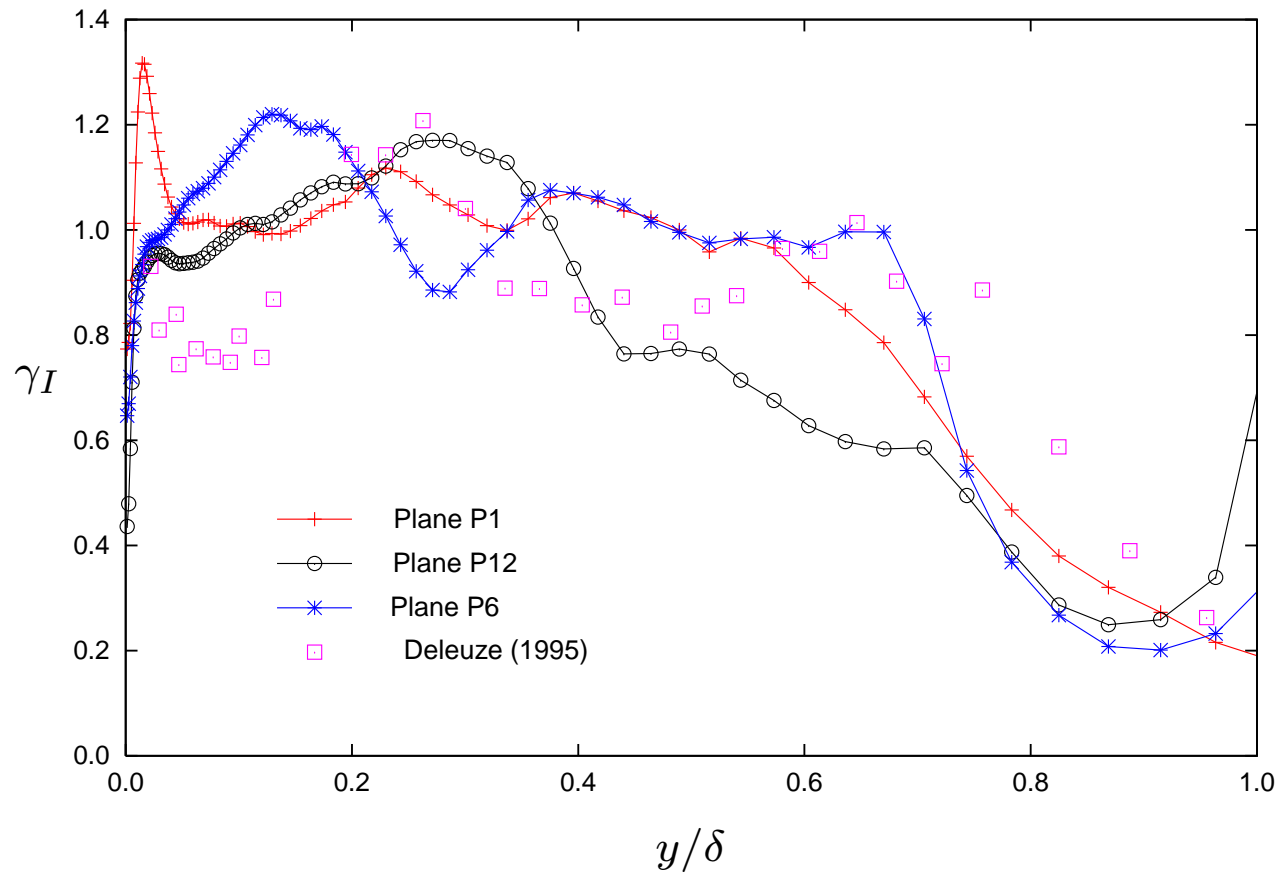
INTERMITTENCY DISTRIBUTION

- Comparison of experimental and simulation intermittency data upstream of shock interaction zone



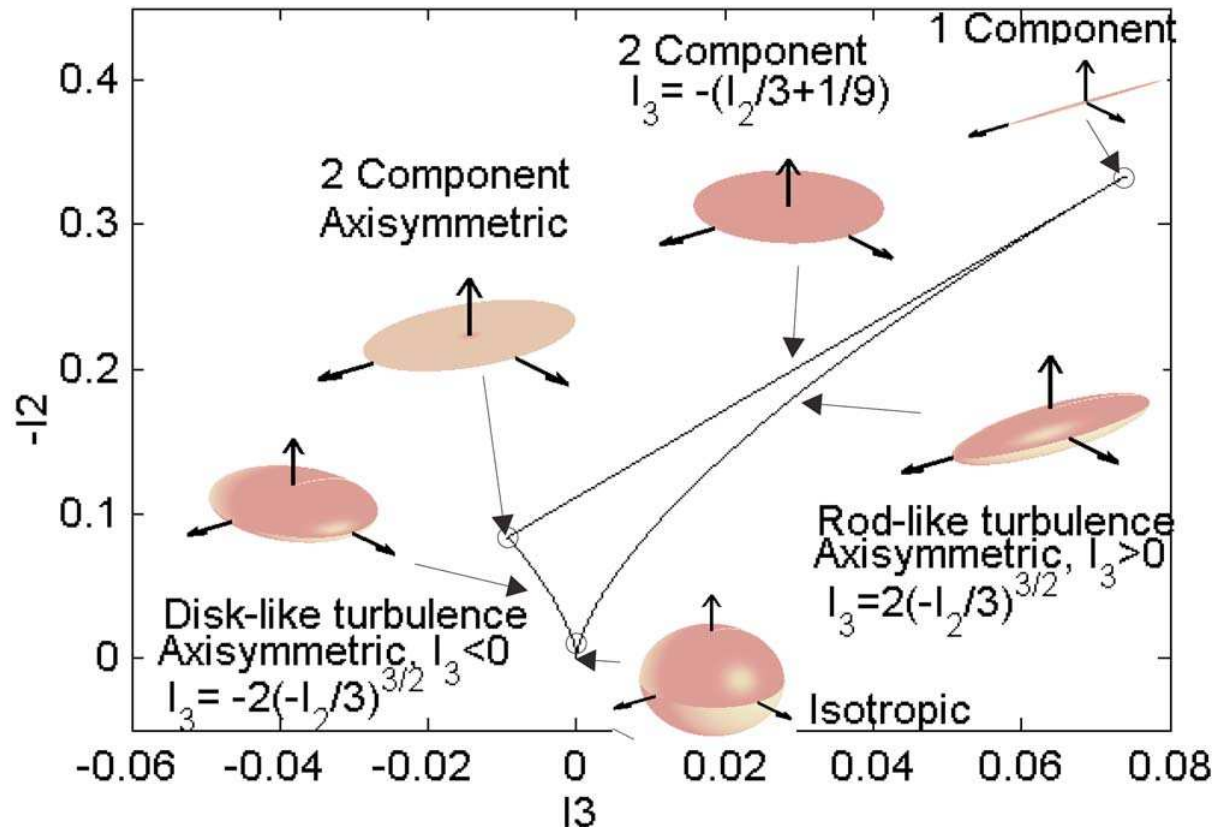
INTERMITTENCY DISTRIBUTION

- Intermittency function at various streamwise locations



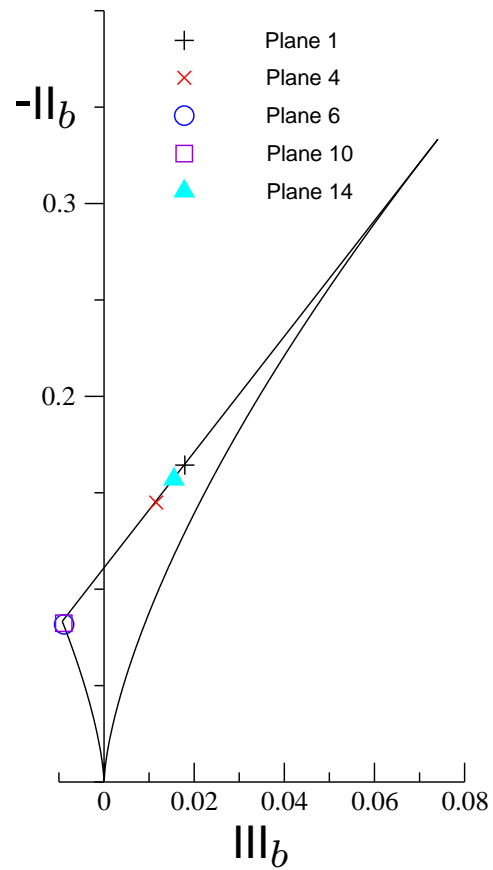
ANISOTROPY INVARIANT MAP

- Structural description of turbulence (Simonsen & Krogstad, Phys. Fluids, 2005)

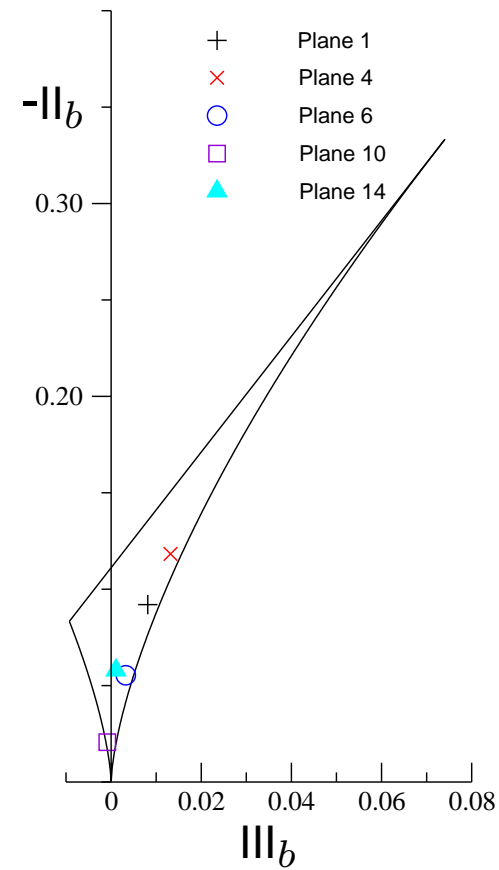


ANISOTROPY INVARIANT MAP

● Invariant mapping of turbulent stress anisotropy at fixed y/δ



$y/\delta = 0.0027$



$y/\delta = 0.047$

TURBULENT STRESSES IN INTERACTION ZONE

- Relationship between density-weighted (Favre) and the Reynolds averaged velocity second moments

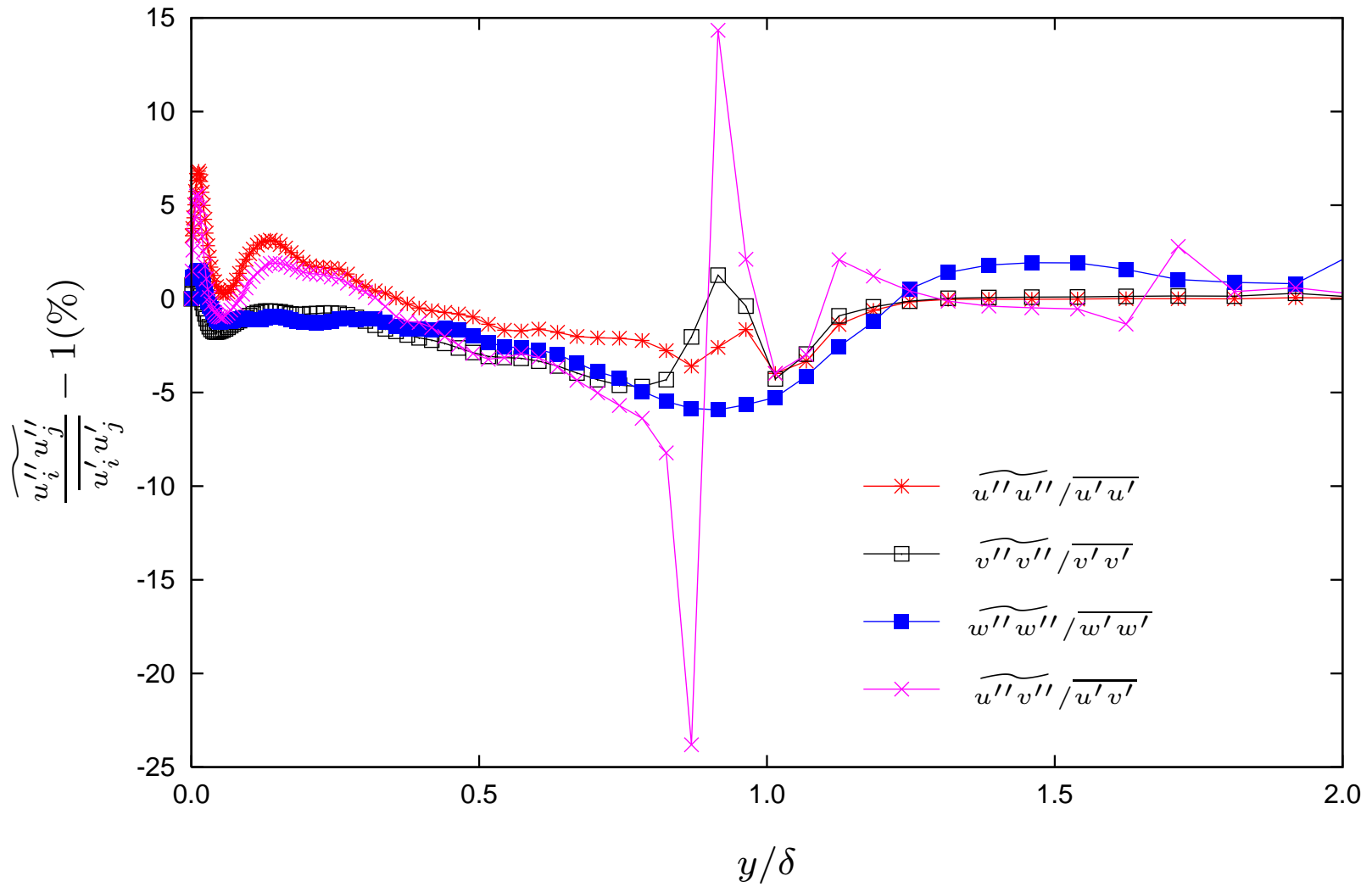
$$\widetilde{u''_i u''_j} = \overline{u'_i u'_j} + \frac{\overline{\rho' u'_i u'_j}}{\bar{\rho}} - \frac{(\overline{\rho' u'_i})(\overline{\rho' u'_j})}{\bar{\rho}^2},$$

$$\widetilde{u''_i \phi''} = \overline{u'_i \phi'} + \frac{\overline{\rho' u'_i \phi'}}{\bar{\rho}} - \frac{(\overline{\rho' u'_i})(\overline{\rho' \phi'})}{\bar{\rho}^2},$$

- Favre and Reynolds averaged anisotropy tensors

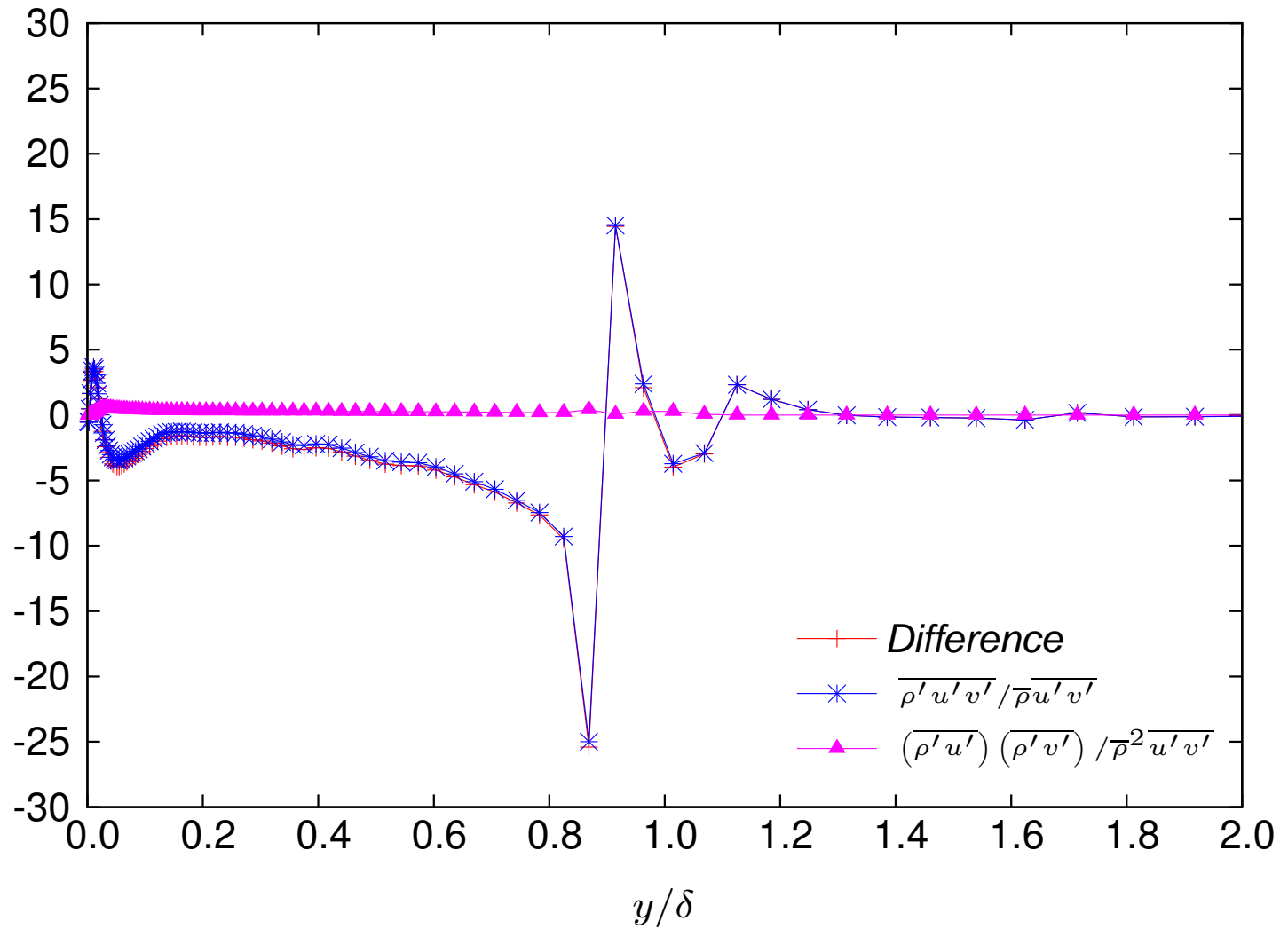
$$\tilde{b}_{ij} = \frac{\widetilde{u''_i u''_j}}{\widetilde{u''_i u''_i}} - \frac{\delta_{ij}}{3} \quad \text{and} \quad \bar{b}_{ij} = \frac{\overline{u'_i u'_j}}{\overline{u'_i u'_i}} - \frac{\delta_{ij}}{3}.$$

TURBULENT STRESSES IN INTERACTION ZONE



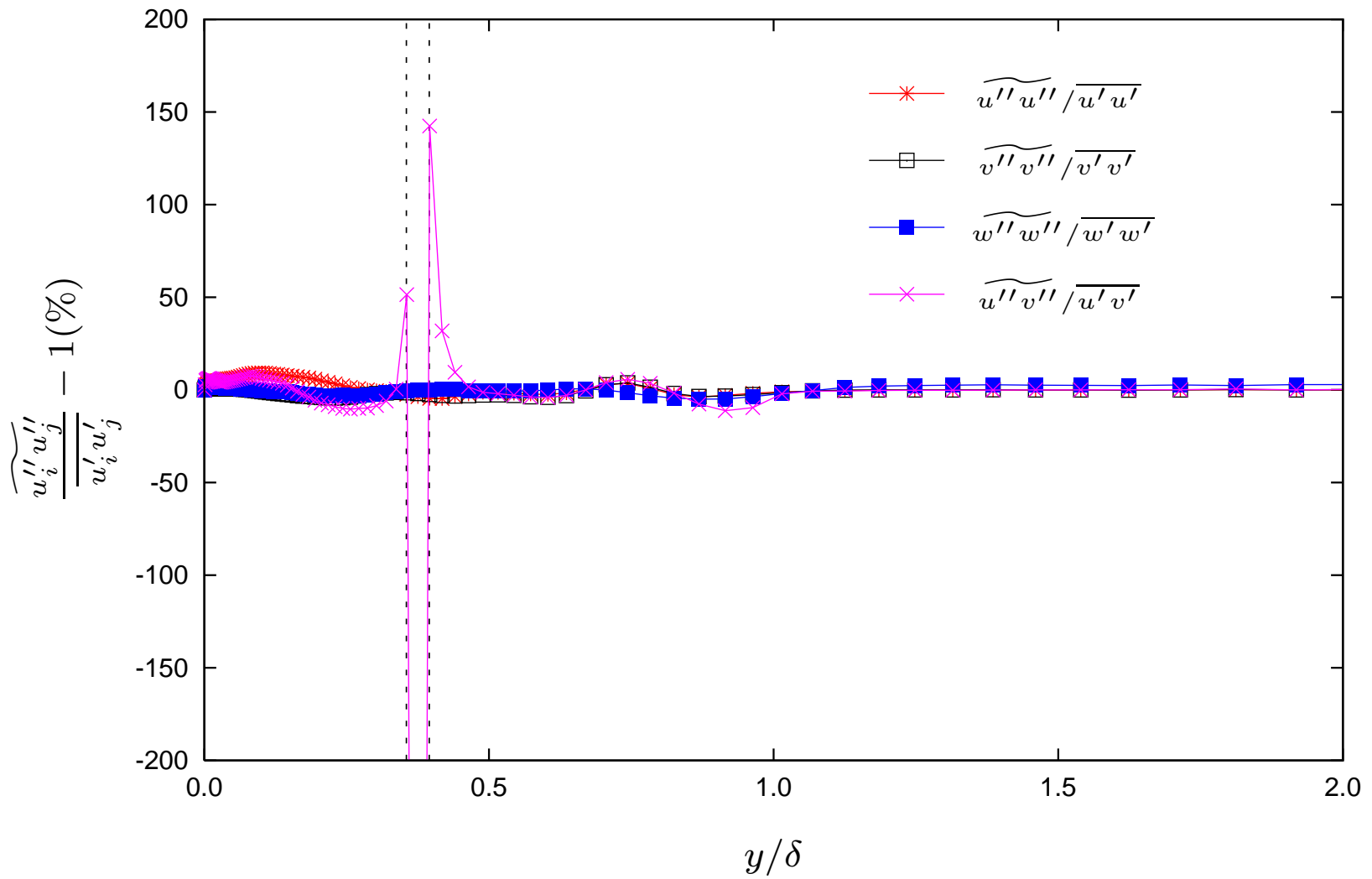
Plane P4

TURBULENT STRESSES IN INTERACTION ZONE



Plane P4

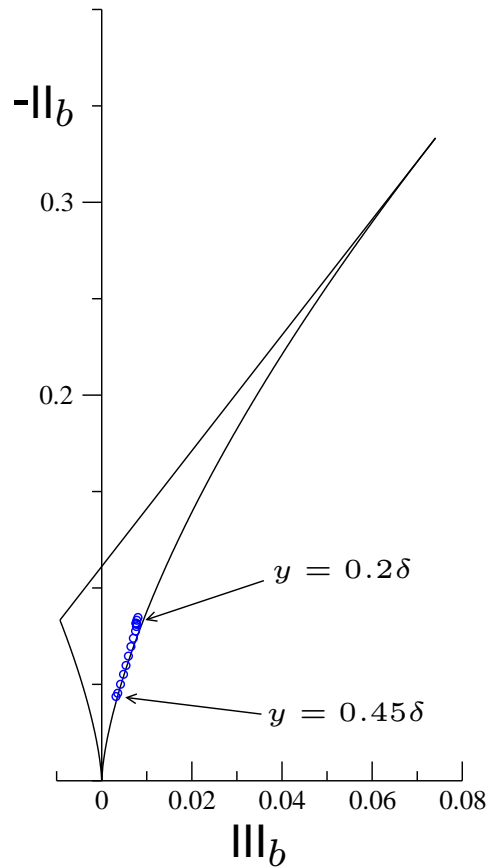
TURBULENT STRESSES IN INTERACTION ZONE



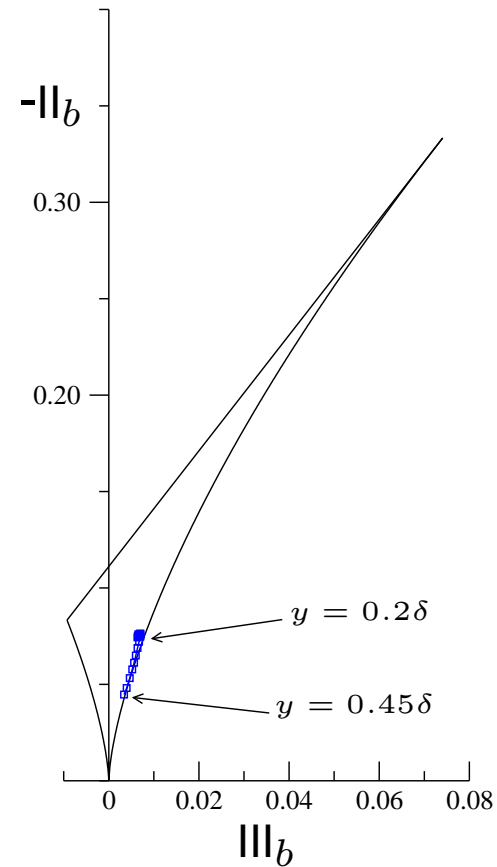
Plane P6

TURBULENT STRESSES IN INTERACTION ZONE

● Anisotropy invariant maps at Plane P6



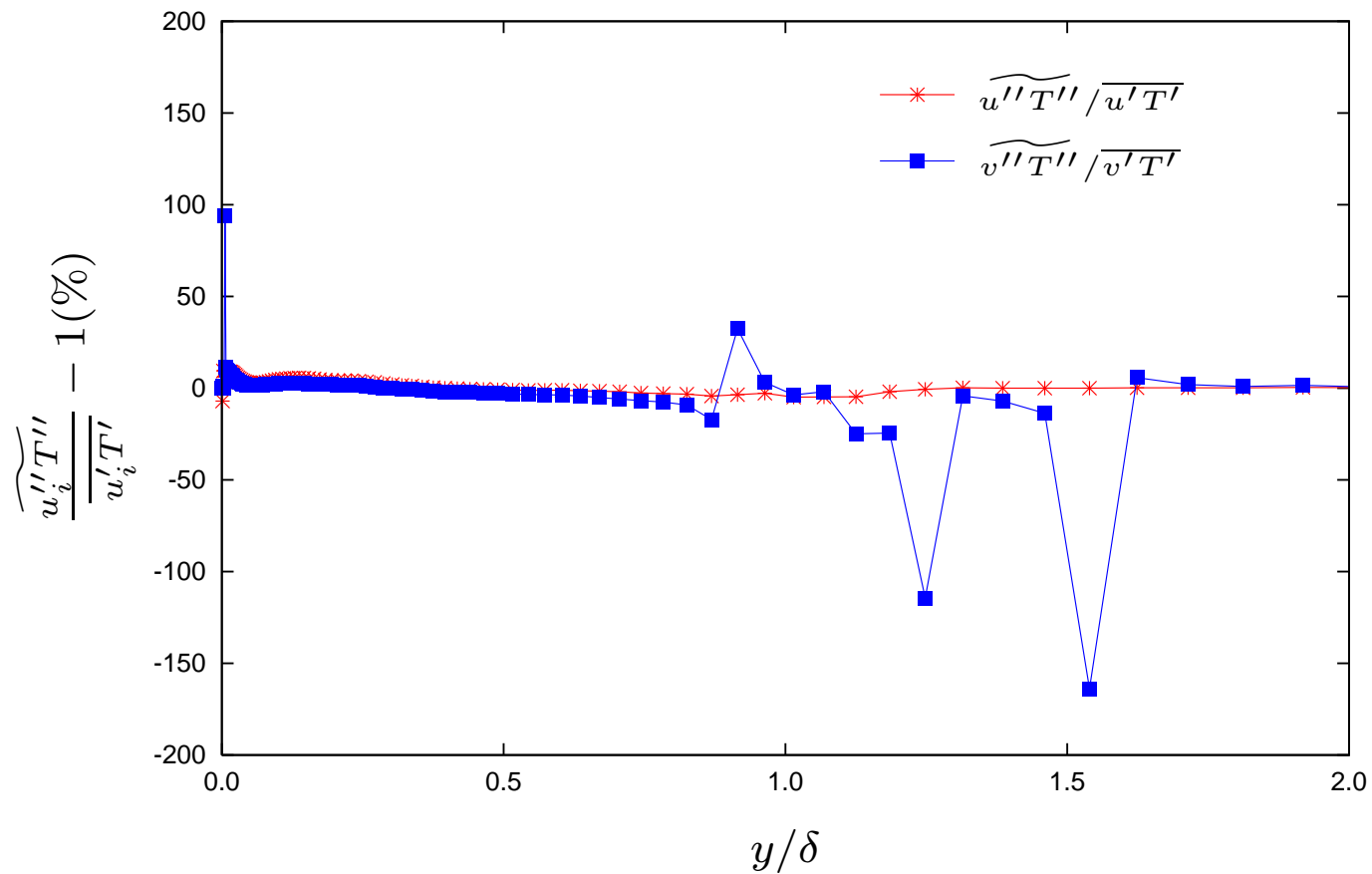
Favre average



Reynolds average

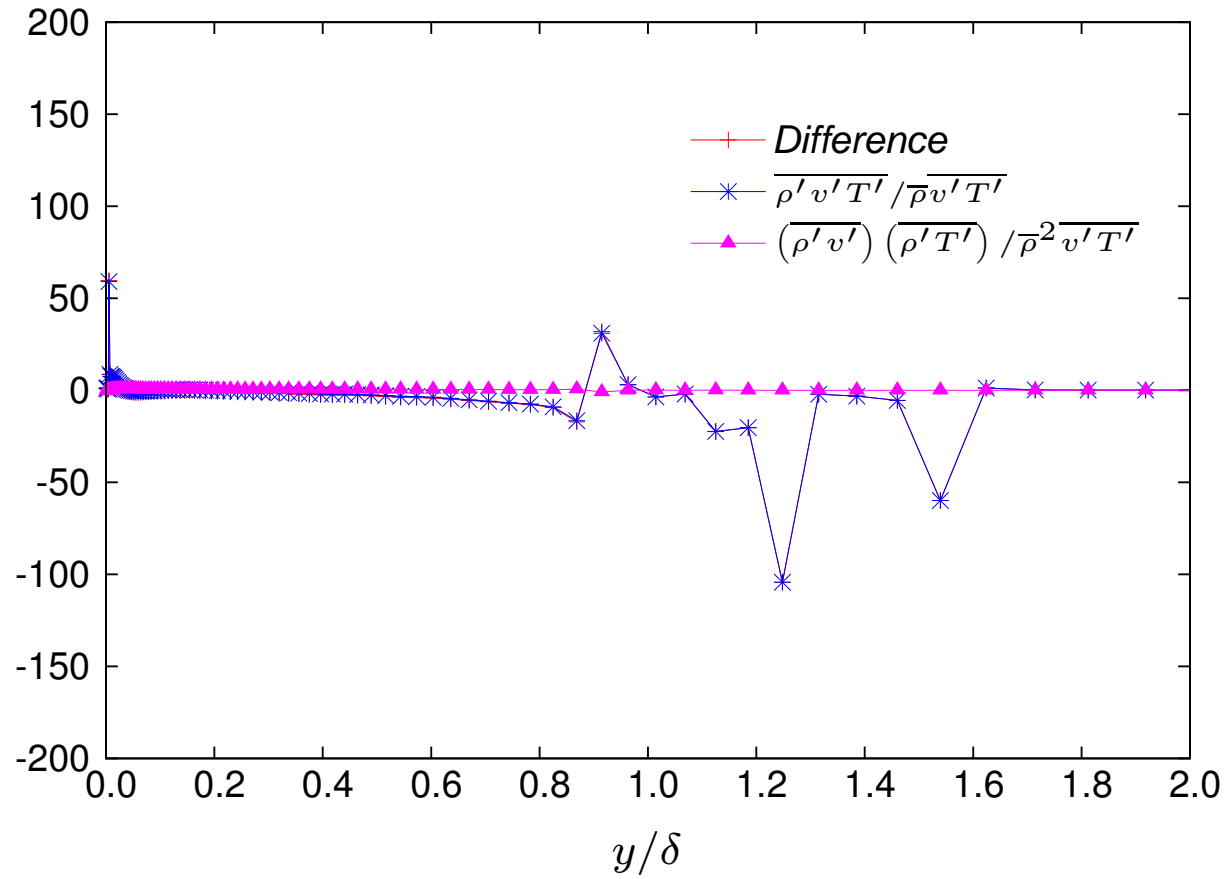
HEAT FLUX RELATIONSHIP

● Normalized turbulent heat fluxes



Plane P4

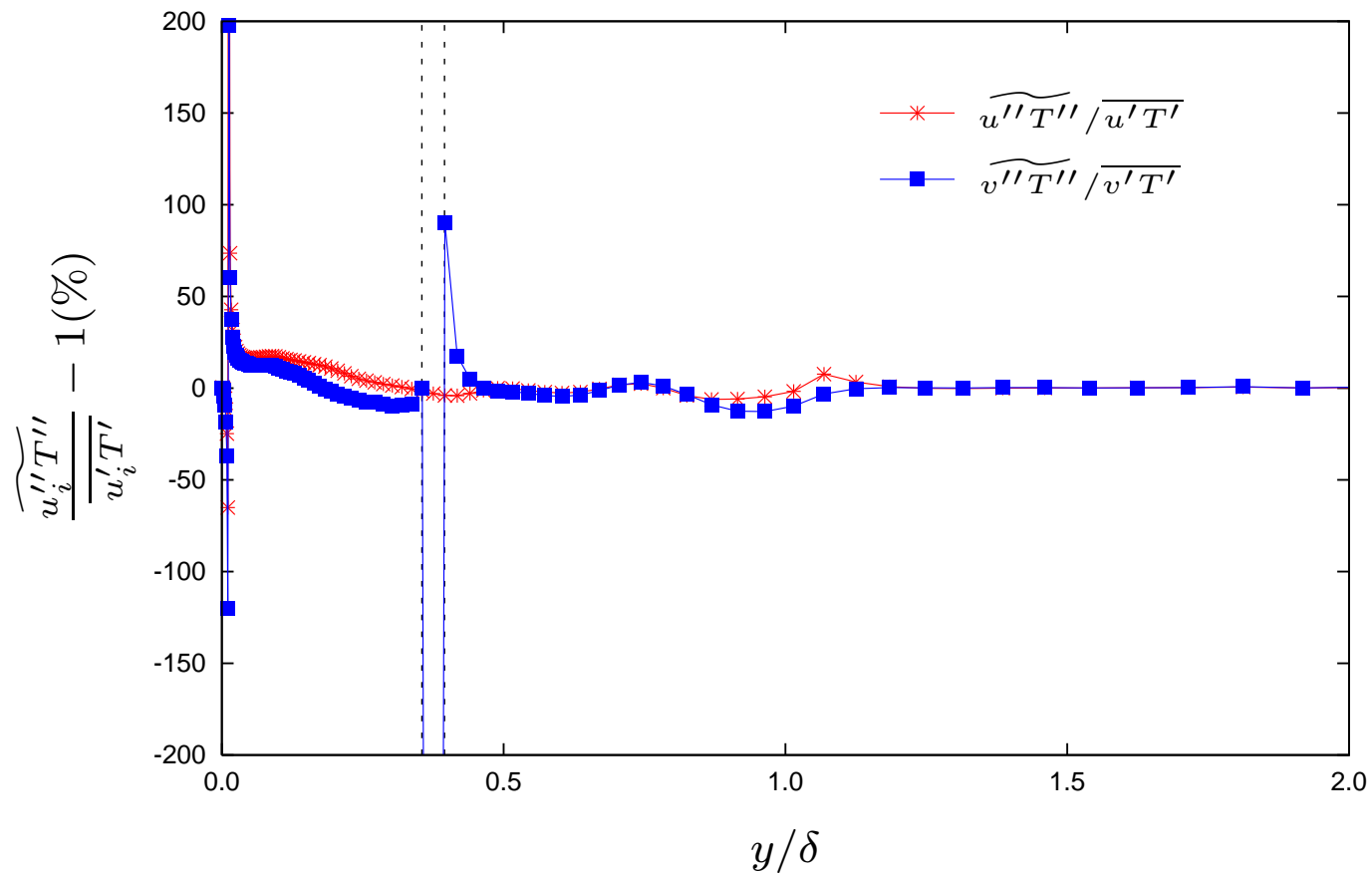
HEAT FLUX RELATIONSHIP



Plane P4

HEAT FLUX RELATIONSHIP

● Normalized turbulent heat fluxes



Plane P6

SUMMARIZING COMMENTS

- Shock impingement induces small separation zone with BL
- Turbulent shear stress distribution significantly affected by shock
 - Anisotropy map less sensitive to distortion
- Key element in model development is turbulent correlation relaxation from shock distortion