



# Mathematical modelling for acoustic microstreaming produced by a gas bubble undergoing asymmetric oscillations

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An exact solution is developed for bubble-induced acoustic microstreaming in the case of a gas bubble undergoing asymmetric oscillations. The modelling is based on the decomposition of the solenoidal, first- and second-order, vorticity fields into poloidal and toroidal components. The result is valid for small-amplitude bubble oscillations without restriction on the size of the viscous boundary layer  $(2\nu/\omega)^{1/2}$  in comparison to the bubble radius. The non-spherical distortions of the bubble interface are decomposed over the set of orthonormal spherical harmonics  $Y_n^m(\theta, \phi)$  of degree  $n$  and order  $m$ . The present theory describes the steady flow produced by the non-spherical oscillations  $(n, \pm m)$  that occur at a frequency different from that of the spherical oscillation, as in the case of a parametrically excited surface oscillation. The three-dimensional aspect of the streaming pattern is revealed as well as the particular flow signatures associated with different asymmetric oscillations.

**Key words:** drops and bubbles

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## 1. Introduction

The high-frequency interfacial motion of ultrasound-driven gas bubbles can generate a steady flow in the surrounding fluid, called acoustic microstreaming. Interest in the bubble-induced streaming and the resulting stresses exerted on surrounding bodies is motivated by a variety of technological, chemical and biomedical applications. Oscillating bubbles close to or in contact with a wall can actuate the transport of particles within the

viscous boundary layer at solid surfaces, with applications in the removal of contamination particles and surface cleaning (Kim *et al.* 2009; Reuter *et al.* 2017), the amplification of chemical treatments (Mason 1999), the handwashing and cleaning of sensitive surfaces (Birkin, Offin & Leighton 2016), and the micromixing of fluids (Wang, Rallabandi & Hilgenfeldt 2013). Cavitation microstreaming is also a propelling source for small water-floating objects and bubble-driven microrobots (Dijkink *et al.* 2006; Ahmed *et al.* 2015). These artificial, acoustically driven microswimmers act as propulsion devices that can carry a payload, with a great potential for microfluidic applications and targeted drug delivery. The commonly used geometry for these microrobots includes a gas bubble trapped in the robot body cavity, whose oscillations create an axisymmetric flow that orients and propels the microrobot (Zhou, Dai & Jiao 2022). The orientation of the propeller can be controlled by inducing one or several holes on armoured bubbles (Bertin *et al.* 2015) by combining acoustic powering and magnetic steering (Aghakhani *et al.* 2020), or by designing gear-like bubble-based propellers in order to actuate rotational motion along closed trajectories (Mohanty *et al.* 2021). Biomedical applications based on bubble-induced flows include cell detachment (Ohl & Wolfrum 2003), the sorting and manipulation of biological materials (Volk *et al.* 2020), the lysis of vesicles (Marmottant, Biben & Hilgenfeldt 2008), and ultrasound-mediated targeted drug delivery (Lajoinie *et al.* 2016; Pereno *et al.* 2018). The ultrasound-mediated delivery of a drug is based on the action of oscillating microbubbles nearby biological barriers that increase their permeability and allow drug and genes to penetrate into individual cells without serious consequence for the cell viability (Fan *et al.* 2014). The temporary permeabilisation of biological barriers is caused by shear stresses exerted on cell tissues by the bubble-induced flows (Wu & Nyborg 2008), which are responsible for a ‘massage’ effect on cells and the creation of transient pores on the cell membrane. Even if no consensus exists on the exact mechanism responsible for cell poration and the required bubble activity (collapsing/inertial regime or stably oscillating regime), determining the bubble-induced flows and resulting shear stress is mandatory.

The first theoretical investigation of acoustic microstreaming was performed by Nyborg (1958). By investigating the near-boundary streaming induced by a compressible body (a gas bubble) resting on a surface, he showed how resonant bubbles produced a pronounced microstreaming in the surface vicinity. Davidson & Riley (1971) have considered the case of a spherical bubble oscillating laterally in an unbounded fluid. Their investigation covers a wide range of situations with respect to the orders of magnitude of two dimensionless parameters. The first,  $\epsilon = U/R_0\omega$ , is the ratio of the vibration amplitude of the velocity  $U$  occurring at the angular frequency  $\omega$  to the bubble radius  $R_0$ . The second parameter quantifies the ratio of the thickness of the Stokes layer to the bubble radius,  $\gamma = (2\nu/\omega)^{1/2}/R_0 = \delta_\nu/R_0$ , where  $\nu$  is the kinematic viscosity, and  $\delta_\nu$  is the thickness of the oscillatory shear layer. A great theoretical achievement of their work is the introduction of a matching approximation between the solution within the inner boundary layer and the one in the outer boundary, performed in the case of large bubbles ( $\gamma \ll 1$ ) driven at relatively low frequencies and with small amplitudes of lateral oscillations ( $\epsilon \ll 1$ ). This approximation has been used in later decades by several authors, adding the contribution of small radial oscillation (Longuet-Higgins 1998), of small-amplitude axisymmetric shape oscillations in the case of the  $n$ th distortion mode with  $n \gg 1$  (Maksimov 2007), and of any arbitrary combination of axisymmetric shape oscillations (Spelman & Lauga 2017). All the above-mentioned theoretical works are based on the matching of the inner/outer solution that assumes a small viscous penetration depth in comparison to the bubble radius. This assumption limits the findings to the case of large bubbles in low-viscosity fluids.

Recently, Doinikov *et al.* (2019*a*) have overcome these limitations by calculating exactly the second-order mean flow induced by all possible interactions between axisymmetric shape oscillations (including the spherical and translational ones).

Yet the similarity between all these theoretical derivations is to consider initially (at rest) spherical bubbles far from any boundary. While this scenario has been recovered experimentally by using levitating, acoustically trapped bubbles (Cleve *et al.* 2019), the majority of experimental work on acoustic microstreaming is performed on substrate-attached microbubbles. The positional stability of the bubble is therefore ensured, hence facilitating the capture of the interface dynamics as well as the surrounding fluid motion. Marmottant *et al.* (2006) resolved the acoustic streaming surrounding a wall-attached bubble experiencing spherical oscillations and a translational one occurring perpendicularly to the wall. Tho, Manasseh & Ooi (2007) performed an extensive study of streaming patterns surrounding a substrate-attached bubble from the top view. In addition to the cases of varying translational and/or oscillating motion of the bubble interface, the authors have also extended the analysis to the case of shape oscillations, without mentioning the triggered shape instability. Marin *et al.* (2015) revealed the three-dimensional nature of the acoustic streaming flow surrounding a wall-attached cylindrical bubble by using an astigmatism particle tracking velocimetry (APTV) technique. Using the same APTV technique, Bolanos-Jimenez *et al.* (2017) captured the three-dimensional axisymmetric, ‘fountain-like’ flow pattern surrounding a hemispherical bubble. Interestingly, the strength of the flow was used as a way of finding the bubble’s lowest resonant frequency. When summarizing the literature, it becomes obvious that experimental and theoretical works on bubbles experiencing asymmetric (i.e. non-axisymmetric) oscillations are scarce, while the ease of triggering asymmetric deformations is facilitated by the contact line dynamics and the breaking of the spherical symmetry. Usually, the complexity of the asymmetric oscillations is disregarded experimentally, where undetermined shape modes are sometimes reported (Saint-Michel & Garbin 2020). The landscape of emergence of specific spherical harmonics for high-amplitude-driven microbubbles was proposed by Fauconnier, Bera & Inserra (2020). The ease of triggering specific asymmetric modes near the minimum of the instability threshold, as well as the partitioning of the triggered modes within the instability region of existence for shape oscillations, was demonstrated. The only theoretical work discussing the emergence and triggering of asymmetric oscillations was performed by Maksimov (2020) in the case of a spherical bubble located in front of a wall. The splitting (partitioning) of the shape modes was recovered theoretically. Concerning the induced flows, a systematic study of the acoustic microstreaming surrounding a wall-attached bubble has been performed by Fauconnier *et al.* (2022). High-amplitude acoustic driving allowed the triggering of non-spherical shape oscillations, including asymmetric ones. The flow signatures were correlated to the bubble interface dynamics decomposed over the set of orthonormal spherical harmonics  $Y_n^m(\theta, \phi)$  of degree  $n$  and order  $m$ . The self-interaction of a given asymmetric shape oscillation results in various flower-like patterns whose numbers of lobes are associated with the degree  $n$  and order  $m$  of the triggered harmonics. Only top view observations were performed, and the three-dimensional nature of these asymmetric patterns has still to be determined.

The present paper provides the mathematical modelling of the second-order mean flow surrounding a bubble experiencing asymmetric oscillations at a frequency different from that of the spherical oscillations, so that the microstreaming comes from the interaction of the shape oscillation with itself (self-interaction). This case is relevant to parametrically excited shape oscillations. Section 2 describes the derivation of the

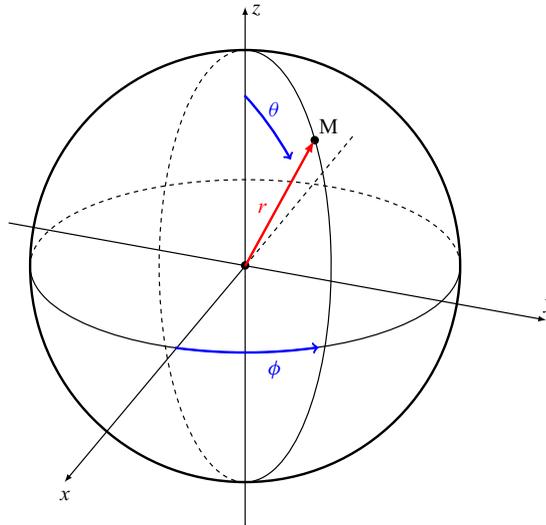


Figure 1. Coordinate system used in calculations.

second-order mean flow, with a particular focus on the decomposition of the solenoidal, first- and second-order, vorticity fields into poloidal and toroidal components. The derivation is valid for small-amplitude bubble oscillations with no restriction on the size of the viscous boundary layer  $\delta_v = (2\nu/\omega)^{1/2}$  in comparison to the bubble radius. This means that our theory is valid for any value of the liquid viscosity  $\nu$ , which in turn means that our theory is valid for any value of the ratio  $\delta_v/R_0$ , where  $R_0$  is the equilibrium bubble radius. We emphasise this fact because in many previous studies on acoustic streaming, the ratio  $\delta_v/R_0$  is assumed to be small, which means that the liquid viscosity is assumed to be very low and/or  $R_0$  to be big. Section 3 presents various numerical examples obtained by the proposed model, highlighting the three-dimensional nature of the streaming patterns, the reversal of the flow atop the bubble by means of the generation of an anti-fountain behaviour, and the possibility of creating flows with a strong azimuthal component when a travelling surface wave propagates at the interface of the bubble.

## 2. Theory

We consider a gas bubble surrounded by an infinite viscous incompressible liquid. We assume that the bubble, which is spherical at rest, undergoes asymmetric oscillations in response to an external acoustic excitation. Figure 1 shows a spherical coordinate system, originated at the equilibrium centre of the bubble, that is used in our calculations. Our derivation follows the conventional procedure for calculating acoustic streaming. We assume that the amplitudes of the bubble oscillation modes are small compared to the equilibrium bubble radius. This assumption allows us to linearise the equations of liquid motion (Navier–Stokes equations) and to find their solutions, assuming the amplitudes of the bubble oscillation modes to be given quantities. These solutions give us a first-order velocity field generated by the bubble in the liquid. Then the equations of liquid motion are written with accuracy up to terms of second order of smallness with respect to the first-order solutions and averaged over time. As a result, we obtain equations that describe the velocity field of acoustic streaming produced by the bubble.

2.1. First-order solutions

The surface of a bubble undergoing the oscillation modes  $(n, m)$  and  $(n, -m)$  can be represented by

$$r_s(\theta, \phi, t) = R_0 + e^{-i\omega t} s^{(n,m)} Y_n^m(\theta, \phi) + e^{-i\omega t} s^{(n,-m)} Y_n^{-m}(\theta, \phi), \quad (2.1)$$

where  $R_0$  is the bubble radius at rest,  $\omega$  is the angular frequency of the bubble oscillations,  $s^{(n,m)}$  and  $s^{(n,-m)}$  are the complex amplitudes of the modes  $(n, m)$  and  $(n, -m)$ , respectively, and  $Y_n^m(\theta, \phi)$  are spherical harmonics of degree  $n$  and order  $-n \leq m \leq n$ , which are defined by (D1) in Appendix D. Here, the azimuthal dependency as a complex exponential has been preferred to the cosine form (known as the real spherical harmonics) for the following reason. The cosine representation of the azimuthal part of the angular function implies an established, standing wave at the interface of the bubble. In order to allow for the most general case of two oppositely moving travelling waves at the interface of the bubble, the two components  $(n, \pm m)$  are considered. When the amplitudes of the two components are equal,  $s^{(n,m)} = s^{(n,-m)}$ , a stationary azimuthal wave is established. When they differ, a quasi-stationary wave exists that is composed of a partially stationary and a partially travelling component. In the general case, any three-dimensional bubble deformation can be decomposed over the set of orthonormal spherical harmonics, which means that several modes can coexist. The interaction of several modes oscillating at the same frequency (mixed-mode streaming) has been described as a dominant contribution to acoustic microstreaming in many situations; see, for example, Longuet-Higgins (1998) and Rallabandi, Wang & Hilgenfeldt (2014). However, the consideration of two interacting modes  $(n_1, m_1)$  and  $(n_2 \neq n_1, m_2 \neq m_1)$  will lead to serious mathematical complexity in calculating the resulting flow. According to the work of Fauconnier *et al.* (2022), the possibility of triggering a single, well-identified, asymmetric mode was demonstrated. The associated flow, resulting from the interaction of the triggered asymmetric mode with itself, was captured. It is therefore worth considering a single asymmetric mode interacting with itself for the description of the induced acoustic microstreaming, as in (2.1).

The values of  $s^{(n,\pm m)}$  and  $\omega$  are considered as known quantities. They are assumed to be measured experimentally and serve as input data in our study. We also assume that  $|s^{(n,\pm m)}|/R_0 \ll 1$ , which allows us to linearise the equations of liquid motion. The linearised equations of a viscous incompressible liquid are given by (Landau & Lifshitz 1987)

$$\nabla \cdot \mathbf{v}_1 = 0, \quad (2.2)$$

$$\frac{\partial \mathbf{v}_1}{\partial t} = -\frac{1}{\rho} \nabla p_1 + \nu \Delta \mathbf{v}_1, \quad (2.3)$$

where  $\mathbf{v}_1$  and  $p_1$  are the first-order liquid velocity and pressure, respectively,  $\rho$  is the constant liquid density,  $\nu = \eta/\rho$  is the kinematic liquid viscosity, and  $\eta$  is the dynamic liquid viscosity.

The first-order velocity field generated by modes  $(n, m)$  and  $(n, -m)$  can be written as

$$\mathbf{v}_1 = \mathbf{v}_1^{(n,m)} + \mathbf{v}_1^{(n,-m)}, \quad (2.4)$$

where  $\mathbf{v}_1^{(n,m)}$  and  $\mathbf{v}_1^{(n,-m)}$  are the first-order liquid velocities generated by the modes  $(n, m)$  and  $(n, -m)$ , respectively. Both  $\mathbf{v}_1^{(n,m)}$  and  $\mathbf{v}_1^{(n,-m)}$  obey (2.2) and (2.3).

The commonly used procedure to solve (2.2) and (2.3) consists in decomposing the first-order liquid velocity  $\mathbf{v}_1$  into the scalar  $\varphi$  and the vector  $\boldsymbol{\psi}$  velocity potentials using the Helmholtz decomposition  $\mathbf{v}_1 = \nabla \varphi + \nabla \times \boldsymbol{\psi}$ . In spherical coordinates associated with the basis set of vectors  $(\mathbf{e}_r, \mathbf{e}_\theta, \mathbf{e}_\phi)$ , the general forms of these potentials are

$\varphi = \varphi(r, \theta, \phi, t)$  and  $\boldsymbol{\psi} = \psi_r(r, \theta, \phi, t) \mathbf{e}_r + \psi_\theta(r, \theta, \phi, t) \mathbf{e}_\theta + \psi_\phi(r, \theta, \phi, t) \mathbf{e}_\phi$ . The Helmholtz decomposition is suitable for solving axisymmetric cases because the azimuthal invariance reduces the decomposition of the velocity field to only two unknowns,  $\varphi(r, \theta, \phi, t)$  and  $\psi_\phi(r, \theta, \phi, t)$  (Doinikov *et al.* 2019a). In the present problem, the general form of the scalar and vector potentials should be kept, leading to four unknown functions. Using the divergence-free property of the velocity field in (2.2), an alternative decomposition can be proposed to reduce the number of unknown functions, such as the poloidal–toroidal decomposition sometimes called the Mie representation of a vector field. Indeed, Mie (1908) was the first to introduce this decomposition in the investigation of Maxwell’s equations in a spherical geometry, after Lamb (1881), who introduced the toroidal part only in hydrodynamics. The application of the poloidal–toroidal decomposition of a solenoidal field concerns mainly terrestrial magnetism (Elsasser 1946; Bullard & Gellman 1954; Backus 1986). Chandrasekhar (1961) adapted this representation to treat a convective-flow stability problem in a spherical cavity. The validity of the poloidal–toroidal decomposition for any solenoidal fields has been demonstrated by Chadwick & Trowbridge (1967) in a bounded annular region, by Backus (1958) in a closed ball, and by Padmavati & Amaranath (2002) for unbounded regions. In the context of bubble physics, Prosperetti (1977) proposed this decomposition for the vorticity field induced by bubble non-spherical oscillations in order to determine the equations of motion of the bubble interface accounting for non-spherical perturbations in viscous fluids. Therefore, we follow the approach of Prosperetti (1977), and calculate the curl of both sides of (2.3), which results in

$$\frac{\partial \boldsymbol{\omega}_1^{(n,m)}}{\partial t} = \nu \Delta \boldsymbol{\omega}_1^{(n,m)}, \tag{2.5}$$

where  $\boldsymbol{\omega}_1^{(n,m)} = \nabla \times \mathbf{v}_1^{(n,m)}$  is called the vorticity of the velocity field  $\mathbf{v}_1^{(n,m)}$ . We then apply the poloidal–toroidal decomposition of the vorticity (Backus 1986)

$$\boldsymbol{\omega}_1^{(n,m)} = \mathbf{P}_1^{(n,m)} + \mathbf{T}_1^{(n,m)}, \tag{2.6}$$

where, in view of the equation of the bubble surface (2.1), the poloidal  $\mathbf{P}_1^{(n,m)}$  and toroidal  $\mathbf{T}_1^{(n,m)}$  fields are written by

$$\mathbf{P}_1^{(n,m)} = e^{-i\omega t} \nabla \times \nabla \times [\mathbf{e}_r P_{nm}(r) Y_n^m(\theta, \phi)], \tag{2.7}$$

$$\mathbf{T}_1^{(n,m)} = e^{-i\omega t} \nabla \times [\mathbf{e}_r T_{nm}(r) Y_n^m(\theta, \phi)], \tag{2.8}$$

with  $\mathbf{e}_r = \mathbf{r}/r$  being the unit radial vector.

Substitution of (2.6) into (2.5) yields

$$\frac{\partial \mathbf{P}_1^{(n,m)}}{\partial t} + \frac{\partial \mathbf{T}_1^{(n,m)}}{\partial t} = \nu \Delta \mathbf{P}_1^{(n,m)} + \nu \Delta \mathbf{T}_1^{(n,m)}. \tag{2.9}$$

In view of the orthogonality of the poloidal and toroidal fields, (2.9) can be split into two equations:

$$\frac{\partial \mathbf{P}_1^{(n,m)}}{\partial t} = \nu \Delta \mathbf{P}_1^{(n,m)}, \tag{2.10}$$

$$\frac{\partial \mathbf{T}_1^{(n,m)}}{\partial t} = \nu \Delta \mathbf{T}_1^{(n,m)}. \tag{2.11}$$

Substituting (2.7) and (2.8) into (2.10) and (2.11), and using the identity

$$\Delta [\mathbf{e}_r F(r) Y_n^m(\theta, \phi)] = \mathbf{e}_r Y_n^m(\theta, \phi) \left[ \frac{d^2 F(r)}{dr^2} - \frac{n(n+1)}{r^2} F(r) \right] + 2 \nabla \left[ \frac{F(r)}{r} Y_n^m(\theta, \phi) \right], \tag{2.12}$$

where  $F(r)$  is an arbitrary function, one obtains

$$-i\omega \nabla \times \nabla \times [\mathbf{e}_r P_{nm}(r) Y_n^m(\theta, \phi)] = \nu \nabla \times \nabla \times \left\{ \mathbf{e}_r Y_n^m(\theta, \phi) \left[ \frac{d^2 P_{nm}(r)}{dr^2} - \frac{n(n+1)}{r^2} P_{nm}(r) \right] \right\}, \tag{2.13}$$

$$-i\omega \nabla \times [\mathbf{e}_r T_{nm}(r) Y_n^m(\theta, \phi)] = \nu \nabla \times \left\{ \mathbf{e}_r Y_n^m(\theta, \phi) \left[ \frac{d^2 T_{nm}(r)}{dr^2} - \frac{n(n+1)}{r^2} T_{nm}(r) \right] \right\}. \tag{2.14}$$

It follows from (2.13) and (2.14) that  $P_{nm}(r)$  and  $T_{nm}(r)$  obey the equations

$$\left[ \frac{d^2}{dr^2} - \frac{n(n+1)}{r^2} + k_v^2 \right] P_{nm}(r) = 0, \tag{2.15}$$

$$\left[ \frac{d^2}{dr^2} - \frac{n(n+1)}{r^2} + k_v^2 \right] T_{nm}(r) = 0, \tag{2.16}$$

where  $k_v = (1+i)/\delta_v$  is the viscous wavenumber, and  $\delta_v = \sqrt{2\nu/\omega}$  is the viscous penetration depth.

It is easy to check that both (2.15) and (2.16) are transformed to the Riccati–Bessel equation (Abramowitz & Stegun 1972) by multiplying by  $r^2$ . Solutions to the above equation are given by  $k_v r z_n(k_v r)$ , where  $z_n$  is the spherical Bessel function of the first or second kind, or the spherical Hankel function of the first or second kind. Since we are looking for solutions in the form of an outgoing wave, we get

$$P_{nm}(r) = a_{nm} k_v r h_n^{(1)}(k_v r), \tag{2.17}$$

$$T_{nm}(r) = b_{nm} k_v r h_n^{(1)}(k_v r), \tag{2.18}$$

where  $a_{nm}$  and  $b_{nm}$  are constants, called the linear scattering coefficients, that are determined by boundary conditions at the bubble surface, and  $h_n^{(1)}$  is the spherical Hankel function of the first kind.

Substituting (2.7) and (2.8) into (2.6), and using (2.17) and (2.18), one obtains

$$\boldsymbol{\omega}_1^{(n,m)} = e^{-i\omega t} \left\{ \nabla \times \nabla \times [\mathbf{e}_r a_{nm} k_v r h_n^{(1)}(k_v r) Y_n^m(\theta, \phi)] + \nabla \times [\mathbf{e}_r b_{nm} k_v r h_n^{(1)}(k_v r) Y_n^m(\theta, \phi)] \right\}. \tag{2.19}$$

It follows from (2.19) that  $\mathbf{v}_1^{(n,m)}$  can be written as

$$\mathbf{v}_1^{(n,m)} = e^{-i\omega t} \left\{ \nabla \times [\mathbf{e}_r a_{nm} k_v r h_n^{(1)}(k_v r) Y_n^m(\theta, \phi)] + \mathbf{e}_r b_{nm} k_v r h_n^{(1)}(k_v r) Y_n^m(\theta, \phi) - \nabla \varphi \right\}, \tag{2.20}$$

where a scalar function  $\varphi$  is introduced in order to satisfy (2.2).

Substitution of (2.20) into (2.2) yields

$$\Delta\varphi = \nabla \cdot \left[ \mathbf{e}_r b_{nm} k_v r h_n^{(1)}(k_v r) Y_n^m(\theta, \phi) \right]. \quad (2.21)$$

Equation (2.21) is the inhomogeneous Laplace equation, which is also called Poisson's equation. Since we are looking for a solution for  $r > R_0$ , the solution to (2.21) can be represented by

$$\varphi(r, \theta, \phi) = c_{nm} r^{-(n+1)} Y_n^m(\theta, \phi) + \varphi_{nm}(r) Y_n^m(\theta, \phi), \quad (2.22)$$

where the first term on the right-hand side is the solution to the Laplace equation ( $\Delta\varphi = 0$ ),  $c_{nm}$  being a constant coefficient, and the second term is a particular solution to Poisson's equation (2.21),  $\varphi_{nm}(r)$  being a function to be found.

To find  $\varphi_{nm}(r)$ , we substitute (2.22) into (2.21), and calculate the right-hand side of (2.21). As a result, we obtain the equation

$$\begin{aligned} \left[ \frac{d^2}{dx^2} + \frac{2}{x} \frac{d}{dx} - \frac{n(n+1)}{x^2} \right] \varphi_{nm}(x) &= \frac{b_{nm}}{k_v} \left[ 3 h_n^{(1)}(x) + x h_n^{(1)'}(x) \right] \\ &= \frac{b_{nm}}{k_v} \left[ (n+3) h_n^{(1)}(x) - x h_{n+1}^{(1)}(x) \right], \end{aligned} \quad (2.23)$$

where  $x = k_v r$ , and the prime denotes the derivative with respect to an argument in brackets.

To solve (2.23), we use the identities (Abramowitz & Stegun 1972)

$$\frac{n}{x} h_n^{(1)}(x) - h_n^{(1)'}(x) = h_{n+1}^{(1)}(x), \quad (2.24)$$

$$\frac{n+1}{x} h_n^{(1)}(x) + h_n^{(1)'}(x) = h_{n-1}^{(1)}(x). \quad (2.25)$$

With the help of (2.24) and (2.25), we obtain

$$\left[ \frac{d^2}{dx^2} + \frac{2}{x} \frac{d}{dx} - \frac{n(n+1)}{x^2} \right] \left[ \alpha h_n^{(1)}(x) + \beta x h_{n+1}^{(1)}(x) \right] = (2\beta - \alpha) h_n^{(1)}(x) - \beta x h_{n+1}^{(1)}(x). \quad (2.26)$$

Comparison of (2.23) with (2.26) reveals that the solution to (2.23) is obtained by setting  $\alpha = -(n+1)b_{nm}/k_v$  and  $\beta = b_{nm}/k_v$ :

$$\varphi_{nm}(x) = \frac{b_{nm}}{k_v} \left[ x h_{n+1}^{(1)}(x) - (n+1) h_n^{(1)}(x) \right]. \quad (2.27)$$

It follows that the general solution to (2.21) is given by

$$\varphi(r, \theta, \phi) = \left\{ c_{nm} r^{-(n+1)} + \frac{b_{nm}}{k_v} \left[ k_v r h_{n+1}^{(1)}(k_v r) - (n+1) h_n^{(1)}(k_v r) \right] \right\} Y_n^m(\theta, \phi). \quad (2.28)$$

The coefficients  $a_{nm}$ ,  $b_{nm}$ ,  $c_{nm}$  are calculated in Appendix A. In the process of this calculation, the following boundary conditions at the bubble surface have been used: the condition that the normal component of the first-order liquid velocity is equal to the normal component of the bubble surface velocity, and the condition that the tangential stress generated by the liquid motion vanishes at the bubble surface because the gas viscosity is much lower than the liquid viscosity. By using the results obtained in Appendix A,  $\mathbf{v}_1^{(n,m)}$  is represented by

$$\mathbf{v}_1^{(n,m)} = v_{1r}^{(n,m)} \mathbf{e}_r + v_{1\theta}^{(n,m)} \mathbf{e}_\theta + v_{1\phi}^{(n,m)} \mathbf{e}_\phi, \tag{2.29}$$

$$v_{1r}^{(n,m)} = e^{-i\omega t} s^{(n,m)} V_n(r) Y_n^m(\theta, \phi), \tag{2.30}$$

$$v_{1\theta}^{(n,m)} = e^{-i\omega t} s^{(n,m)} W_n(r) \frac{\partial Y_n^m(\theta, \phi)}{\partial \theta}, \quad n \geq 1, \tag{2.31}$$

$$v_{1\phi}^{(n,m)} = e^{-i\omega t} s^{(n,m)} \frac{W_n(r)}{\sin \theta} \frac{\partial Y_n^m(\theta, \phi)}{\partial \phi}, \quad n, m \geq 1, \tag{2.32}$$

where the functions  $V_n(r)$  and  $W_n(r)$  are calculated by

$$V_n(r) = \frac{(n+1)\alpha_n}{r^{n+2}} + \frac{n(n+1)\beta_n h_n^{(1)}(k_v r)}{k_v r}, \tag{2.33}$$

$$W_n(r) = -\frac{\alpha_n}{r^{n+2}} + \frac{\beta_n}{k_v r} \left[ (n+1)h_n^{(1)}(k_v r) - k_v r h_{n+1}^{(1)}(k_v r) \right], \tag{2.34}$$

and the coefficients  $\alpha_n$  and  $\beta_n$  are given by

$$\alpha_n = \frac{i\omega R_0^{n+2} \left[ (2-n-n^2)h_n^{(1)}(\bar{x}) - \bar{x}^2 h_n^{(1)''}(\bar{x}) \right]}{(n+1) \left[ \bar{x}^2 h_n^{(1)''}(\bar{x}) - (n^2+3n+2)h_n^{(1)}(\bar{x}) \right]}, \quad n \geq 0, \tag{2.35}$$

$$\beta_n = \frac{2i(n+2)\bar{x}\omega}{(n+1) \left[ \bar{x}^2 h_n^{(1)''}(\bar{x}) - (n^2+3n+2)h_n^{(1)}(\bar{x}) \right]}, \quad n \geq 1, \tag{2.36}$$

where  $\bar{x} = k_v R_0$ . Note that (2.33)–(2.36) follow from (A8), (A9), (A22) and (A23) by setting  $c_{nm} = s^{(n,m)}\alpha_n$  and  $b_{nm} = s^{(n,m)}\beta_n$ .

The first-order velocity generated by the mode  $(n, -m)$  is obtained by replacing  $m$  with  $-m$  in (2.29)–(2.32):

$$\mathbf{v}_1^{(n,-m)} = v_{1r}^{(n,-m)} \mathbf{e}_r + v_{1\theta}^{(n,-m)} \mathbf{e}_\theta + v_{1\phi}^{(n,-m)} \mathbf{e}_\phi, \tag{2.37}$$

$$v_{1r}^{(n,-m)} = e^{-i\omega t} s^{(n,-m)} V_n(r) Y_n^{-m}(\theta, \phi), \tag{2.38}$$

$$v_{1\theta}^{(n,-m)} = e^{-i\omega t} s^{(n,-m)} W_n(r) \frac{\partial Y_n^{-m}(\theta, \phi)}{\partial \theta}, \quad n \geq 1, \tag{2.39}$$

$$v_{1\phi}^{(n,-m)} = e^{-i\omega t} s^{(n,-m)} \frac{W_n(r)}{\sin \theta} \frac{\partial Y_n^{-m}(\theta, \phi)}{\partial \phi}, \quad n, m \geq 1. \tag{2.40}$$

With the help of (D1) and (D3) from Appendix D, (2.38)–(2.40) are represented by

$$v_{1r}^{(n,-m)} = e^{-i\omega t} s^{(n,-m)} V_n(r) (-1)^m Y_n^{m*}(\theta, \phi), \tag{2.41}$$

$$v_{1\theta}^{(n,-m)} = e^{-i\omega t} s^{(n,-m)} W_n(r) (-1)^m \frac{\partial Y_n^{m*}(\theta, \phi)}{\partial \theta}, \quad n \geq 1, \tag{2.42}$$

$$v_{1\phi}^{(n,-m)} = e^{-i\omega t} s^{(n,-m)} \frac{W_n(r)}{\sin \theta} (-1)^m \frac{\partial Y_n^{m*}(\theta, \phi)}{\partial \phi}, \quad n, m \geq 1, \tag{2.43}$$

where the asterisk denotes the complex conjugate.

### 2.2. Solutions of the equations of acoustic streaming

The equations of acoustic streaming are given by (Doinikov *et al.* 2019a)

$$\nabla \cdot \mathbf{v}_E = 0, \tag{2.44}$$

$$\Delta \nabla \times \mathbf{v}_E = \frac{1}{\nu} \nabla \times \langle \mathbf{v}_1 \cdot \nabla \mathbf{v}_1 \rangle, \tag{2.45}$$

where  $\mathbf{v}_E$  is the Eulerian streaming velocity, i.e. the time-averaged second-order liquid velocity, and  $\langle \rangle$  means the time average.

Substitution of (2.4) into (2.45) yields

$$\begin{aligned} \Delta \nabla \times \mathbf{v}_E &= \frac{1}{\nu} \nabla \\ &\times \left\langle \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,m)} + \mathbf{v}_1^{(n,-m)} \cdot \nabla \mathbf{v}_1^{(n,-m)} + \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,-m)} + \mathbf{v}_1^{(n,-m)} \cdot \nabla \mathbf{v}_1^{(n,m)} \right\rangle. \end{aligned} \tag{2.46}$$

This equation can be divided into three equations:

$$\Delta \nabla \times \mathbf{v}_E^{(n,m)} = \frac{1}{\nu} \nabla \times \left\langle \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,m)} \right\rangle, \tag{2.47}$$

$$\Delta \nabla \times \mathbf{v}_E^{(n,-m)} = \frac{1}{\nu} \nabla \times \left\langle \mathbf{v}_1^{(n,-m)} \cdot \nabla \mathbf{v}_1^{(n,-m)} \right\rangle, \tag{2.48}$$

$$\Delta \nabla \times \mathbf{v}_E^{(\times)} = \frac{1}{\nu} \nabla \times \left\langle \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,-m)} + \mathbf{v}_1^{(n,-m)} \cdot \nabla \mathbf{v}_1^{(n,m)} \right\rangle, \tag{2.49}$$

where (2.47) describes the acoustic streaming generated by the mode  $(n, m)$  alone, (2.48) describes the acoustic streaming generated by the mode  $(n, -m)$  alone, and (2.49) describes the acoustic streaming due to the interaction of the above modes (streaming due to cross-terms).

Let us first consider (2.47). Since  $\nabla \times \mathbf{v}_E^{(n,m)}$  is a divergence-free vector field, it can be represented by a poloidal-toroidal decomposition (Backus 1986)

$$\begin{aligned} \nabla \times \mathbf{v}_E^{(n,m)} &= \nabla \times \nabla \times \left[ \mathbf{e}_r \sum_{k=1}^{\infty} \sum_{l=-k}^k P_{kl}^{(n,m)}(r) Y_k^l(\theta, \phi) \right] \\ &+ \nabla \times \left[ \mathbf{e}_r \sum_{k=1}^{\infty} \sum_{l=-k}^k T_{kl}^{(n,m)}(r) Y_k^l(\theta, \phi) \right] \\ &= \sum_{k=1}^{\infty} \sum_{l=-k}^k \left\{ \mathbf{e}_r \frac{k(k+1) P_{kl}^{(n,m)}(r)}{r^2} Y_k^l(\theta, \phi) \right. \\ &+ \frac{P_{kl}^{(n,m)'}(r)}{r} \left[ \mathbf{e}_\theta \frac{\partial Y_k^l(\theta, \phi)}{\partial \theta} + \frac{\mathbf{e}_\phi}{\sin \theta} \frac{\partial Y_k^l(\theta, \phi)}{\partial \phi} \right] \\ &+ \left. \frac{T_{kl}^{(n,m)}(r)}{r} \left[ \frac{\mathbf{e}_\theta}{\sin \theta} \frac{\partial Y_k^l(\theta, \phi)}{\partial \phi} - \mathbf{e}_\phi \frac{\partial Y_k^l(\theta, \phi)}{\partial \theta} \right] \right\}. \end{aligned} \tag{2.50}$$

Recall that the prime in the superscript denotes the derivative with respect to an argument in brackets. Substitution of (2.50) into (2.47) and the calculation of  $\Delta \nabla \times \mathbf{v}_E^{(n,m)}$  yield

$$\begin{aligned}
 \Delta \nabla \times \mathbf{v}_E^{(n,m)} &= \sum_{k=1}^{\infty} \sum_{l=-k}^k \left\{ \mathbf{e}_r \frac{k(k+1)}{r^2} \left[ P_{kl}^{(n,m)''}(r) - \frac{k(k+1) P_{kl}^{(n,m)}(r)}{r^2} \right] Y_k^l(\theta, \phi) \right. \\
 &+ \frac{1}{r} \left[ P_{kl}^{(n,m)'''}(r) - \frac{k(k+1) P_{kl}^{(n,m)'}(r)}{r^2} + \frac{2k(k+1) P_{kl}^{(n,m)}(r)}{r^3} \right] \\
 &\times \left[ \mathbf{e}_\theta \frac{\partial Y_k^l(\theta, \phi)}{\partial \theta} + \frac{\mathbf{e}_\phi}{\sin \theta} \frac{\partial Y_k^l(\theta, \phi)}{\partial \phi} \right] \\
 &+ \frac{1}{r} \left[ T_{kl}^{(n,m)''}(r) - \frac{k(k+1) T_{kl}^{(n,m)}(r)}{r^2} \right] \left[ \frac{\mathbf{e}_\theta}{\sin \theta} \frac{\partial Y_k^l(\theta, \phi)}{\partial \phi} - \mathbf{e}_\phi \frac{\partial Y_k^l(\theta, \phi)}{\partial \theta} \right] \left. \right\} \\
 &= \frac{1}{v} \nabla \times \left\langle \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,m)} \right\rangle. \tag{2.51}
 \end{aligned}$$

Equating the  $r$ -components of both sides of (2.51), one obtains

$$\begin{aligned}
 &\sum_{k=1}^{\infty} \sum_{l=-k}^k \frac{k(k+1)}{r^2} \left[ P_{kl}^{(n,m)''}(r) - \frac{k(k+1) P_{kl}^{(n,m)}(r)}{r^2} \right] Y_k^l(\theta, \phi) \\
 &= \frac{1}{v} \mathbf{e}_r \cdot \left[ \nabla \times \left\langle \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,m)} \right\rangle \right]. \tag{2.52}
 \end{aligned}$$

Calculating the curl of both sides of (2.51) and taking the  $r$ -component, one finds

$$\begin{aligned}
 &\sum_{k=1}^{\infty} \sum_{l=-k}^k \frac{k(k+1)}{r^2} \left[ T_{kl}^{(n,m)''}(r) - \frac{k(k+1) T_{kl}^{(n,m)}(r)}{r^2} \right] Y_k^l(\theta, \phi) \\
 &= \frac{1}{v} \mathbf{e}_r \cdot \left[ \nabla \times \nabla \times \left\langle \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,m)} \right\rangle \right]. \tag{2.53}
 \end{aligned}$$

Equations (2.52) and (2.53) make it possible to calculate  $P_{kl}^{(n,m)}(r)$  and  $T_{kl}^{(n,m)}(r)$ , and hence  $\mathbf{v}_E^{(n,m)}$ . In view of the cumbersome nature of these calculations, they are performed in Appendix B. As a result, we obtain the components of the Eulerian streaming velocity in the following form:

$$v_{Er}^{(n,m)}(r, \theta) = \frac{1}{2\sqrt{\pi}} \sum_{k=1}^{\infty} \sqrt{2k+1} \left[ T_{k0}^{(n,m)}(r) + \Phi_{k0}^{(n,m)'}(r) \right] P_k(\cos \theta), \tag{2.54}$$

$$v_{E\theta}^{(n,m)}(r, \theta) = \frac{1}{2\sqrt{\pi} r} \sum_{k=1}^{\infty} \sqrt{2k+1} \Phi_{k0}^{(n,m)}(r) P_k^1(\cos \theta), \tag{2.55}$$

$$v_{E\phi}^{(n,m)}(r, \theta) = -\frac{1}{2\sqrt{\pi} r} \sum_{k=1}^{\infty} \sqrt{2k+1} P_{k0}^{(n,m)}(r) P_k^1(\cos \theta), \tag{2.56}$$

where  $P_k$  is the Legendre polynomial of degree  $k$ ,  $P_k^1$  is the associated Legendre polynomial of first order and degree  $k$ , and the functions  $P_{k0}^{(n,m)}(r)$ ,  $T_{k0}^{(n,m)}(r)$ ,  $\Phi_{k0}^{(n,m)}(r)$ ,  $\Phi_{k0}^{(n,m)'}(r)$  are calculated by (B18), (B24), (B33) and (B45).

In the process of the calculation of  $\mathbf{v}_E^{(n,m)}$  in Appendix B, we also calculate the Stokes drift velocity  $\mathbf{v}_S^{(n,m)}$  (Longuet-Higgins 1998), whose components are given by

$$v_{Sr}^{(n,m)}(r, \theta) = \frac{|s^{(n,m)}|^2}{4\sqrt{\pi} \omega} \sum_{k=1}^{\infty} \sqrt{2k+1} A_{k0}^{nmnm} \times \operatorname{Re} \left\{ i V_n^*(r) \left[ \frac{2n(n+1) - k(k+1)}{2r} W_n(r) - V_n'(r) \right] \right\} P_k(\cos \theta), \tag{2.57}$$

$$v_{S\theta}^{(n,m)}(r, \theta) = \frac{|s^{(n,m)}|^2}{8\sqrt{\pi} \omega} \operatorname{Re} \left\{ i V_n^*(r) \left[ \frac{W_n(r)}{r} - W_n'(r) \right] \right\} \sum_{k=1}^{\infty} \sqrt{2k+1} A_{k0}^{nmnm} P_k^1(\cos \theta), \tag{2.58}$$

$$v_{S\phi}^{(n,m)}(r, \theta) = \sum_{k=1}^{\infty} E_k^{(n,m)}(r) P_k^1(\cos \theta), \tag{2.59}$$

where  $\operatorname{Re}$  means ‘the real part of’, the coefficients  $A_{k0}^{nmnm}$  are calculated by (D20), and the function  $E_k^{(n,m)}$  is defined by (B63). Note that (2.57) and (2.58) follow from (B54) and (B56) using  $f_{nm}(r) = s^{(n,m)} V_n(r)$  and  $g_{nm}(r) = s^{(n,m)} W_n(r)$ .

Knowing  $\mathbf{v}_E^{(n,m)}$  and  $\mathbf{v}_S^{(n,m)}$ , we can calculate the Lagrangian streaming velocity produced by the mode  $(n, m)$ , which is defined by  $\mathbf{v}_L^{(n,m)} = \mathbf{v}_E^{(n,m)} + \mathbf{v}_S^{(n,m)}$ .

Due to symmetry, solutions to (2.48) are expressed in terms of the solutions to (2.47) as follows:

$$v_{Lr}^{(n,-m)}(r, \theta) = \frac{|s^{(n,-m)}|^2}{|s^{(n,m)}|^2} v_{Lr}^{(n,m)}(r, \pi - \theta), \tag{2.60}$$

$$v_{L\theta}^{(n,-m)}(r, \theta) = -\frac{|s^{(n,-m)}|^2}{|s^{(n,m)}|^2} v_{L\theta}^{(n,m)}(r, \pi - \theta), \tag{2.61}$$

$$v_{L\phi}^{(n,-m)}(r, \theta) = -\frac{|s^{(n,-m)}|^2}{|s^{(n,m)}|^2} v_{L\phi}^{(n,m)}(r, \pi - \theta). \tag{2.62}$$

To solve (2.49), by analogy with the solution of (2.47),  $\nabla \times \mathbf{v}_E^{(\times)}$  is represented by a poloidal–toroidal decomposition,

$$\begin{aligned} \nabla \times \mathbf{v}_E^{(\times)} &= \operatorname{Re} \left\{ \nabla \times \nabla \times \left[ \mathbf{e}_r \sum_{k=1}^{\infty} \sum_{l=-k}^k P_{kl}^{(\times)}(r) Y_k^l(\theta, \phi) \right] \right. \\ &\quad \left. + \nabla \times \left[ \mathbf{e}_r \sum_{k=1}^{\infty} \sum_{l=-k}^k T_{kl}^{(\times)}(r) Y_k^l(\theta, \phi) \right] \right\} \\ &= \operatorname{Re} \sum_{k=1}^{\infty} \sum_{l=-k}^k \left\{ \mathbf{e}_r \frac{k(k+1) P_{kl}^{(\times)}(r)}{r^2} Y_k^l(\theta, \phi) \right. \\ &\quad \left. + \frac{P_{kl}^{(\times)'}(r)}{r} \left[ \mathbf{e}_\theta \frac{\partial Y_k^l(\theta, \phi)}{\partial \theta} + \frac{\mathbf{e}_\phi}{\sin \theta} \frac{\partial Y_k^l(\theta, \phi)}{\partial \phi} \right] \right. \\ &\quad \left. + \frac{T_{kl}^{(\times)}(r)}{r} \left[ \frac{\mathbf{e}_\theta}{\sin \theta} \frac{\partial Y_k^l(\theta, \phi)}{\partial \phi} - \mathbf{e}_\phi \frac{\partial Y_k^l(\theta, \phi)}{\partial \theta} \right] \right\}, \tag{2.63} \end{aligned}$$

where the functions  $P_{kl}^{(\times)}(r)$  and  $T_{kl}^{(\times)}(r)$ , by analogy with (2.52) and (2.53), obey the equations

$$\begin{aligned} \operatorname{Re} \sum_{k=1}^{\infty} \sum_{l=-k}^k \frac{k(k+1)}{r^2} \left[ P_{kl}^{(\times)''}(r) - \frac{k(k+1)P_{kl}^{(\times)}(r)}{r^2} \right] Y_k^l(\theta, \phi) \\ = \frac{1}{\nu} \mathbf{e}_r \cdot \left[ \nabla \times \left\langle \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,-m)} + \mathbf{v}_1^{(n,-m)} \cdot \nabla \mathbf{v}_1^{(n,m)} \right\rangle \right], \end{aligned} \quad (2.64)$$

$$\begin{aligned} \operatorname{Re} \sum_{k=1}^{\infty} \sum_{l=-k}^k \frac{k(k+1)}{r^2} \left[ T_{kl}^{(\times)''}(r) - \frac{k(k+1)T_{kl}^{(\times)}(r)}{r^2} \right] Y_k^l(\theta, \phi) \\ = \frac{1}{\nu} \mathbf{e}_r \cdot \left[ \nabla \times \nabla \times \left\langle \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,-m)} + \mathbf{v}_1^{(n,-m)} \cdot \nabla \mathbf{v}_1^{(n,m)} \right\rangle \right]. \end{aligned} \quad (2.65)$$

Equations (2.64) and (2.65) are solved in Appendix C. As a result, we obtain the components of  $\mathbf{v}_E^{(\times)}$  in the form

$$v_{Er}^{(\times)}(r, \theta, \phi) = \operatorname{Re} \sum_{k=1}^{\infty} \sum_{l=-k}^k \left[ T_{kl}^{(\times)}(r) + \Phi_{kl}^{(\times)'}(r) \right] Y_k^l(\theta, \phi), \quad (2.66)$$

$$\begin{aligned} v_{E\theta}^{(\times)}(r, \theta, \phi) = \operatorname{Re} \sum_{k=1}^{\infty} \sum_{l=-k}^k \frac{\Phi_{kl}^{(\times)}(r)}{2r} \\ \times \left[ \sqrt{k(k+1) - l(l+1)} Y_k^{l+1}(\theta, \phi) e^{-i\phi} - \sqrt{k(k+1) - l(l-1)} Y_k^{l-1}(\theta, \phi) e^{i\phi} \right], \end{aligned} \quad (2.67)$$

$$\begin{aligned} v_{E\phi}^{(\times)}(r, \theta, \phi) = -\operatorname{Re} \sum_{k=1}^{\infty} \sum_{l=-k}^k \frac{i l \Phi_{kl}^{(\times)}(r) e^{i\phi}}{r} \sqrt{\frac{(2k+1)(k-l)!}{(k+l)!}} \\ \times \sum_{s=1}^{[(k-l+2)/2]} \sqrt{\frac{(2k-4s+3)(k+l-2s)!}{(k-l-2s+2)!}} Y_{k-2s+1}^{l-1}(\theta, \phi), \end{aligned} \quad (2.68)$$

where the functions  $T_{kl}^{(\times)}(r)$ ,  $\Phi_{kl}^{(\times)}(r)$  and  $\Phi_{kl}^{(\times)'}(r)$  are calculated by (C13), (C22) and (C33).

The components of the Stokes drift velocity produced by the interaction of the modes  $(n, m)$  and  $(n, -m)$  are given by

$$v_{Sr}^{(\times)}(r, \theta, \phi) = \operatorname{Re} \sum_{k=1}^{\infty} S_k^{(\times)}(r) \sum_{l=-k}^k D_{kl}^{nmnm} Y_k^l(\theta, \phi), \quad (2.69)$$

$$\begin{aligned} v_{S\theta}^{(\times)}(r, \theta, \phi) = \frac{1}{2} \operatorname{Re} \left\{ U_{nm}(r) \times \sum_{k=1}^{\infty} \sum_{l=-k}^k D_{kl}^{nmnm} \left[ \sqrt{k(k+1) - l(l+1)} Y_k^{l+1}(\theta, \phi) e^{-i\phi} \right. \right. \\ \left. \left. - \sqrt{k(k+1) - l(l-1)} Y_k^{l-1}(\theta, \phi) e^{i\phi} \right] \right\}, \end{aligned} \quad (2.70)$$

$$v_{S\phi}^{(\times)}(r, \theta, \phi) = -\text{Re} \left\{ i U_{nm}(r) e^{i\phi} \sum_{k=1}^{\infty} \sum_{l=-k}^k l \sqrt{\frac{(2k+1)(k-l)!}{(k+l)!}} D_{kl}^{nmnm} \right. \\ \left. \times \sum_{s=1}^{[(k-l+2)/2]} \sqrt{\frac{(2k-4s+3)(k+l-2s)!}{(k-l-2s+2)!}} Y_{k-2s+1}^{l-1}(\theta, \phi) \right\}, \quad (2.71)$$

where the coefficients  $D_{kl}^{nmnm}$  are calculated by (D27), and the functions  $S_k^{(\times)}(r)$  and  $U_{nm}(r)$  are defined by (C43) and (C44).

Knowing  $v_E^{(\times)}$  and  $v_S^{(\times)}$ , we can calculate the corresponding Lagrangian streaming velocity:  $v_L^{(\times)} = v_E^{(\times)} + v_S^{(\times)}$ .

Finally, summing the three components of the acoustic streaming, we get the total flow:

$$v_L^{(total)}(r, \theta, \phi) = v_L^{(n,m)}(r, \theta) + v_L^{(n,-m)}(r, \theta) + v_L^{(\times)}(r, \theta, \phi). \quad (2.72)$$

In the process of the calculations described in this section, we have applied the boundary conditions for the acoustic streaming at the bubble surface that assume that the normal velocity and the tangential stress produced by the Lagrangian streaming vanish at the equilibrium bubble surface.

It is worth noting that we do not provide expressions for the first- and second-order pressures because they are not used in the calculation of acoustic streaming. The above pressures are needed, for example, for the calculation of the acoustic radiation force on the bubble. However, this problem is beyond the scope of our paper. It requires individual consideration somewhere else because, in particular, the calculation of the second-order pressure is not a trivial mathematical problem.

### 3. Results and discussion

#### 3.1. Three classes of spherical harmonics

Let us first consider how the asymmetric shape deformations are described mathematically. In the general case, the shape of a deformed three-dimensional body can always be decomposed over the set of orthonormal spherical harmonics  $Y_n^m(\theta, \phi)$  of degree  $n$  and order  $m$ . These two indexes are related to the spatial evolution of the spherical harmonics along the spherical angular coordinates, the colatitude  $\theta \in [0, \pi]$  and the longitude  $\phi \in [0, 2\pi]$ . For a given degree  $n$ , three classes of spherical harmonics are usually considered: the zonal harmonics when  $m = 0 < n$ , the tesseral harmonics when  $0 < m < n$ , and the sectoral harmonics when  $m = n$ . The three classes of spherical harmonics are represented in figure 2 for degree  $n = 5$ .

In figure 2(a), the bubble undergoes the zonal harmonic  $Y_5^0$ . The bubble interface is axisymmetric, the bubble contour looks spherical from the top view, and the shape from the side view is a Legendre polynomial ( $m = 0$ ). Figure 2(b) illustrates the case of the tesseral harmonic  $Y_5^3$ . The bubble interface is complex to describe at first, as angular deviations from the sphere appear along both the elevation and azimuthal directions. A closer look reveals that the bubble interface possesses  $n - m = 2$  nodal lines along the elevation (see figure 2(b), side view), and  $m = 3$  meridian nodal lines (see figure 2(b), top view). Along the azimuthal direction, and equivalently along the elevation, two successive extrema are out of phase from both side of the nodal lines. Figure 2(c) displays a bubble experiencing the sectoral harmonic  $Y_5^5$ . The top view contour of a sectoral harmonic of

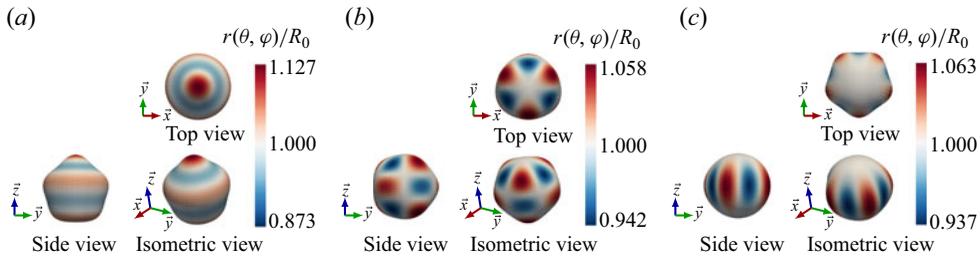


Figure 2. Numerical shape deformations of a bubble experiencing (a) the zonal harmonic  $Y_5^0$ , (b) the tesseral harmonic  $Y_5^3$ , and (c) the sectoral harmonic  $Y_5^5$ . Every isometric view of the spherical harmonics is displayed in top (upper) and side (lower) views.

degree  $n$  corresponds to an  $n$ -lobe deformation and is easily recognisable. The side view of a sectoral harmonic is close to the spherical shape. In fact, the side view contour resembles a bell-shape function, with a higher amplitude at the equator  $\theta = \pi/2$ , and a decreasing oscillation amplitude when reaching the poles. It is worth mentioning that the so-called top and side views are ruled experimentally by the existence of a preferential direction for the triggering of a given shape oscillation at the bubble interface. For instance, in the case of a substrate-attached deformable body, the normal to the substrate is always the preferential direction for the triggering of asymmetric oscillations, as observed in Fauconnier *et al.* (2022) for wall-attached bubbles, and in Chang *et al.* (2015) for sessile drops.

In the present derivation of the bubble-induced microstreaming, only self-interacting asymmetric oscillations are considered. We recall here that the main mechanism for generating shape oscillations at the bubble interface is the Faraday instability occurring at the subharmonic of the driving frequency. Therefore, interactions of shape oscillations with the radial (spherical) oscillations of the bubble cannot lead to fluid mean flows, as the radial mode oscillates at the driving frequency. In addition, near the instability threshold of a given shape oscillation, we also assume that a single instability is triggered without considering the energy transfer to secondary shape oscillations, as theoretically discussed by Shaw (2006) and experimentally observed by Guédra *et al.* (2016). An analysis of the intermodal interactions and their impact on the microstreaming pattern is performed in Regnault *et al.* (2021). The analysis of self-interacting axisymmetric modes is well-known theoretically (Inserra *et al.* 2020a) and has been observed from a side view in a plane containing the bubble symmetry  $z$  axis using acoustically trapped bubbles, being far from any boundary (Cleve *et al.* 2019). The case of self-interacting asymmetric oscillations was considered by Fauconnier *et al.* (2022). The authors investigated experimentally the top view microstreaming flow induced by a wall-attached bubble experiencing various asymmetric oscillations. The predominant shape oscillations were selected using a spectral analysis of the displacement of the bubble interface, and the modal content of the bubble could safely be associated with the observed fluid pattern. For some experimental cases, the secondary excited shape oscillations were so weak that the microstreaming pattern could be confidently related to the self-interaction of the main triggered surface oscillation. Such patterns resulting from self-interacting asymmetric oscillations are reproduced in figure 3 (adapted from Fauconnier *et al.* 2022). Figure 3(a) shows the top view microstreaming pattern induced by the self-interacting zonal harmonic  $Y_4^0$ . The pattern is exclusively radial, since the oscillating bubble interface exhibits no azimuthal dependence (figure 2a, top view). Figure 3(b) represents the top view microstreaming pattern induced by the self-interacting tesseral harmonic  $Y_4^2$ . The pattern is characterised by  $4m = 8$  lobes, arranged by pairs around the  $z$  axis orthogonal to the image, each pair being located

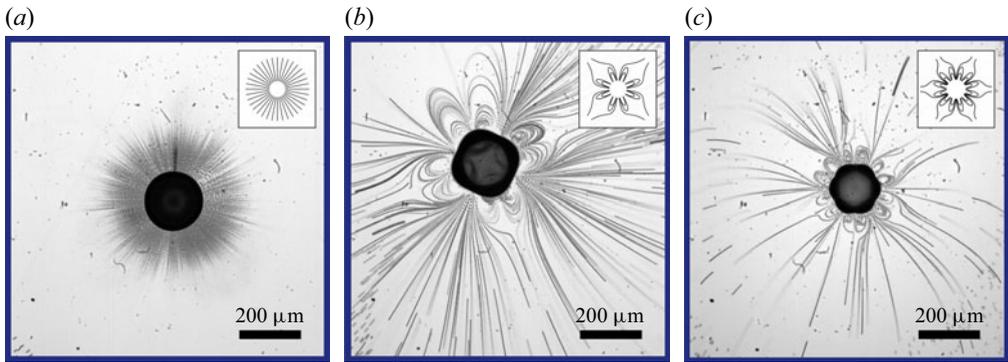


Figure 3. Microstreaming patterns associated with the three classes of spherical harmonics, i.e. (a) zonal, (b) tesseral and (c) sectoral, experienced by a wall-attached bubble and observed with microscope in a top view configuration. Images are reproduced from Fauconnier *et al.* (2022).

between two displacement nodes of the bubble interface (the location of the four meridian lines is clearly visible through the light shades inside the bubble). Figure 3(c) shows the top view microstreaming pattern induced by the self-interacting sectoral harmonic  $Y_3^3$ . The microstreaming pattern displays  $4m = 12$  lobes that are also arranged in pairs. Because sectoral modes are devoid of nodal parallels and exhibit an azimuthal shape that corresponds to the  $\cos(m\phi)$  function along the equator,  $2m = 6$  extrema of displacements are observed on the bubble interface. Therefore, two vortices are expected between two successive nodal meridians, leading to the observed 12-lobe pattern.

For all these experimental microstreaming patterns, the top view configuration avoids the analysis of the full three-dimensional signature of fluid flows induced by asymmetric oscillations, as the seeded particles tracking the fluid motion can escape from the focal plane of observation. The dependence in elevation for the above-mentioned pattern is therefore not ensured and can only be guessed using physical arguments. The three-dimensional nature of the fluid flow was investigated by Marin *et al.* (2015) and Bolanos-Jimenez *et al.* (2017) using an APTV technique. However, the analysis was performed on a wall-attached bubble exhibiting an axisymmetric flow around the perpendicular to the wall. In the following, we illustrate the three-dimensional nature of the flow surrounding asymmetric bubbles using the present modelling.

### 3.2. Signature for axisymmetric, zonal ( $m = 0$ ) harmonics

Axisymmetric shape oscillations are the widely investigated cases because of the ease of triggering them in various experimental configurations. The lack of the dependence of the zonal harmonics in the azimuthal direction significantly facilitates their mathematical analysis, as already discussed in the Introduction. Therefore, we first analyse the case of a zonal (axisymmetric) harmonic, namely the case  $n = 3$ ,  $m = 0$ . The bubble equilibrium radius is set to  $73.8 \mu\text{m}$ , as in the experimental case (figure 3c) displaying a shape oscillation of degree  $n = 3$ . This value is close to the resonant radius of the  $n$ th shape oscillation, as derived by Lamb (1916):

$$R_{res}^n = \sqrt[3]{\frac{(n-1)(n+1)(n+2)\sigma}{\rho\omega_d^2/4}}, \quad (2.73)$$

where  $\sigma$  is the surface tension,  $\rho$  is the liquid density, and  $\omega_d = 2\pi f_d$  is the angular frequency of acoustic driving. The value of  $\omega_d$  differs from the frequency of the shape

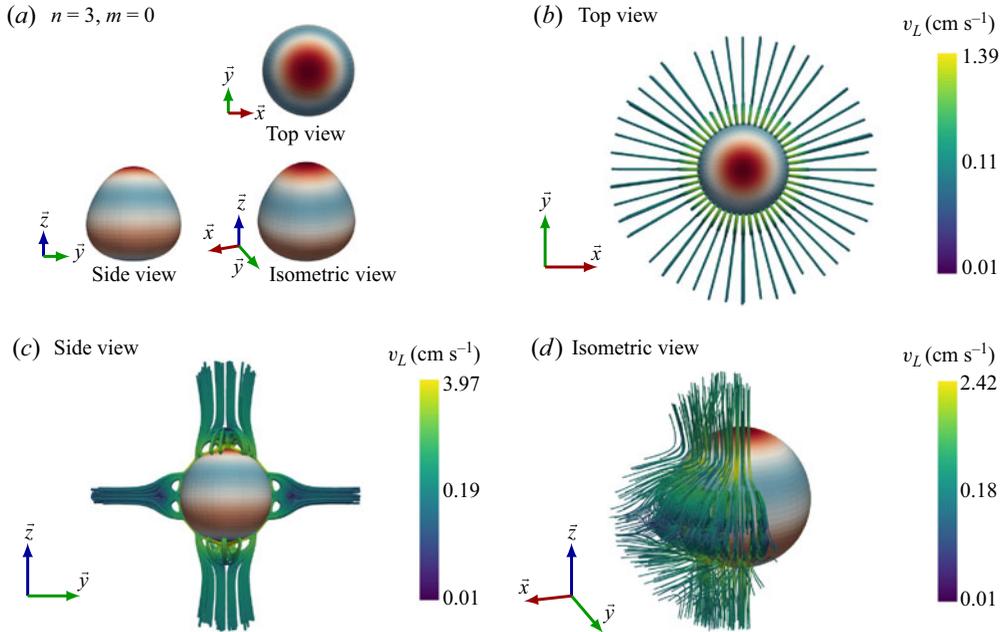


Figure 4. Presentation of the microstreaming pattern observed for a bubble (equilibrium radius  $73.8\ \mu\text{m}$ ) exhibiting zonal oscillations on the mode ( $n = 3, m = 0$ ): (a) numerical contours of the bubble interface in the top, side and three-dimensional views; (b) top, (c) side and (d) isometric views of the resulting flow.

oscillation when the surface deformation is induced by a parametric instability. It should hence be noted that in all the following numerical simulations of microstreaming induced by a shape oscillation, the angular frequency  $\omega$  used in the theoretical derivation is assumed equal to half the driving frequency: here,  $\omega = \omega_d/2$ .

For the axisymmetric shape oscillations of degree  $n = 3$ , the resonant radius is  $R_{res}^n = 65.9\ \mu\text{m}$  for an air bubble in water with  $\rho = 1000\ \text{kg m}^{-3}$ ,  $\sigma = 0.0727\ \text{N m}^{-1}$  at  $f_d = 30.5\ \text{kHz}$ . The value of the frequency corresponds to the experimental driving frequency in Fauconnier *et al.* (2022). We recall that the resonant radius (2.73) is theoretically independent of order  $m$  of the spherical harmonics. The amplitudes of the two modes  $s^{(n,\pm m)}$  are set equal to  $15\ \mu\text{m}$  ( $|s^{(n,\pm m)}|/R_0 \sim 0.2$ ), so that the case of a stationary surface oscillation is investigated. It is worth mentioning that we have chosen the value of the oscillation amplitude that corresponds approximately to measured amplitudes of asymmetric oscillations in Fauconnier *et al.* (2022). This value leads to a not very small value of the dimensionless parameter  $|s^{(n,\pm m)}|/R_0$ , which, however, in practice is small enough to ensure the convergence of the first-order solutions (see § 2.1). What is more, from the point of view of the qualitative behaviour of acoustic streaming, the value of the oscillation amplitude is of no importance in our simulations because mathematically the streaming velocity is directly proportional to the oscillation amplitude squared. Hence a change in the oscillation amplitude does not change, qualitatively, the obtained results. Numerical simulations are performed for an asymmetric deformation oscillating at half the driving frequency, i.e. for  $f = 15.25\ \text{kHz}$ , as the shape oscillations are supposed to be triggered by the Faraday parametric instability. The dimensionless thickness of the viscous boundary layer is therefore  $\gamma = \delta_v/R_0 \sim 0.06 \ll 1$ .

The bubble interface and the resulting microstreaming are presented in figure 4. This display will be used in all investigated numerical cases of standing-wave patterns.

Figure 4(a) shows the deformation of the bubble interface on the axisymmetric mode  $Y_3^0$ , with a display similar to that in figure 2 (top, side and three-dimensional views). Keeping the same orientation of the Cartesian frame, figures 4(b)–4(d) present the microstreaming pattern derived from the Lagrangian velocity field. The streamlines have been obtained using the library *pyvista* from Python programming. The top and side views of the microstreaming are obtained by calculating the streamlines in a narrow area (in depth) along the whole equator (for the top view, figure 4(b) or along a whole meridian (side view, figure 4(c)). The procedure is as follows. The considered equator/meridian is segmented in 48 particle clouds, termed as source, homogeneously distributed along the perimeter. A source particle cloud is located at the radial distance  $1.01 R_0$  from the centre of the bubble, for a given angular position  $(\theta, \phi)$ . Each source contains 10 particles. The streamlines are generated by using each particle as a starting location. For the sake of readability, the three-dimensional streamlines are computed in figure 4(d) only inside a constrained range of the longitude  $\phi$  of the three-dimensional space surrounding the bubble, and by calculating 400 streamlines in the investigated region. Note that because of these different numerical calculations for the streamlines, the velocity range displayed in the colour bars may differ from one view to another. The derived streamlines are in full agreement with the theoretical predictions (Doinikov *et al.* 2019a) and experimental observations (Cleve *et al.* 2019; Fauconnier *et al.* 2022) of the microstreaming induced by an axisymmetric oscillation. The side view exhibits a cross-like shape with small recirculation loops in the vicinity of the bubble interface. It is worth mentioning that while theoretically all streamlines are closed vortical trajectories, some of the vortices are so extended spatially that they appear as straight lines in figure 4(c). In fact, these streamlines will close at a large distance from the centre of the bubble. Increasing the number of calculated streamlines would fill the region between the two orthogonal branches of the cross-like shape in figure 4(c), for instance. Due to the absence of azimuthal dependence, the streamlines from the top view are purely radial. Note that the small recirculation loops along the meridian are not observed because of the cutting of the microstreaming field along the equator. This situation is similar to that encountered when looking at a streaming field in the focal plane of a microscope (figure 2a). The rotational direction of the flow can be perceived from a close look at the streamlines in the side and three-dimensional views: it is known that the fluid particles are propelled away from the anti-nodes (where the streamlines start) and attracted back to the nodes of displacement of the bubble interface (where the streamlines finish). This fact will be very useful in the following to discern the three-dimensional pattern of the flow, in the case of asymmetric modes.

### 3.3. Signature for various asymmetric modes with the same degree $n$

For the same bubble equilibrium radius and mode amplitudes, figures 5–7 show the resulting microstreaming patterns for the class of tesseral ( $Y_3^1$ , figure 5, and  $Y_3^2$ , figure 6) and sectoral ( $Y_3^3$ , figure 7) harmonics of the same degree  $n = 3$ .

The tesseral mode  $Y_3^1$  possesses  $m = 1$  meridian nodal lines (figure 5a, top view) and  $n - m = 2$  nodal parallels (figure 5a, side view). From the top view configuration, the bubble contour exhibits two nodes and two anti-nodes of displacement. The resulting top view pattern is characterised by a cross shape (figure 5b), similar to the quadrupole pattern generated by a solid-body translation oscillation without shape deformation (Longuet-Higgins 1998; Doinikov *et al.* 2019b). The main difference with this axisymmetric quadrupole pattern lies in the out-of-plane component of the velocity field, as streamlines go away from the equatorial plane and from a closed loop that reaches the nearest displacement node on the bubble interface. The closeness of this top view asymmetric

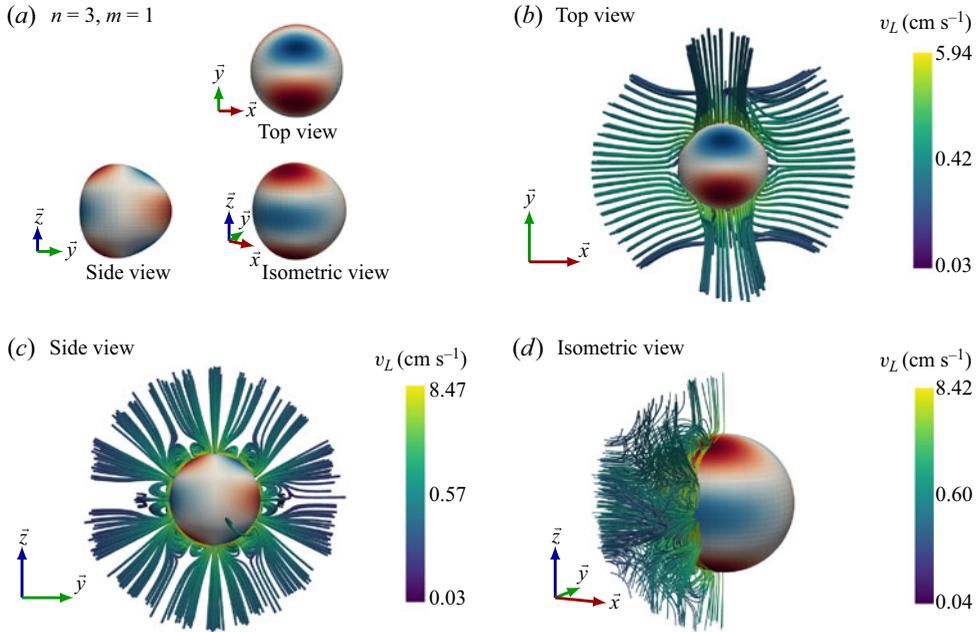


Figure 5. Presentation of the microstreaming pattern observed for a bubble (equilibrium radius  $73.8\ \mu\text{m}$ ) exhibiting tesseral oscillations on the mode ( $n = 3, m = 1$ ): (a) numerical contours of the bubble interface in the top, side and three-dimensional views; (b) top, (c) side and (d) isometric views of the resulting flow.

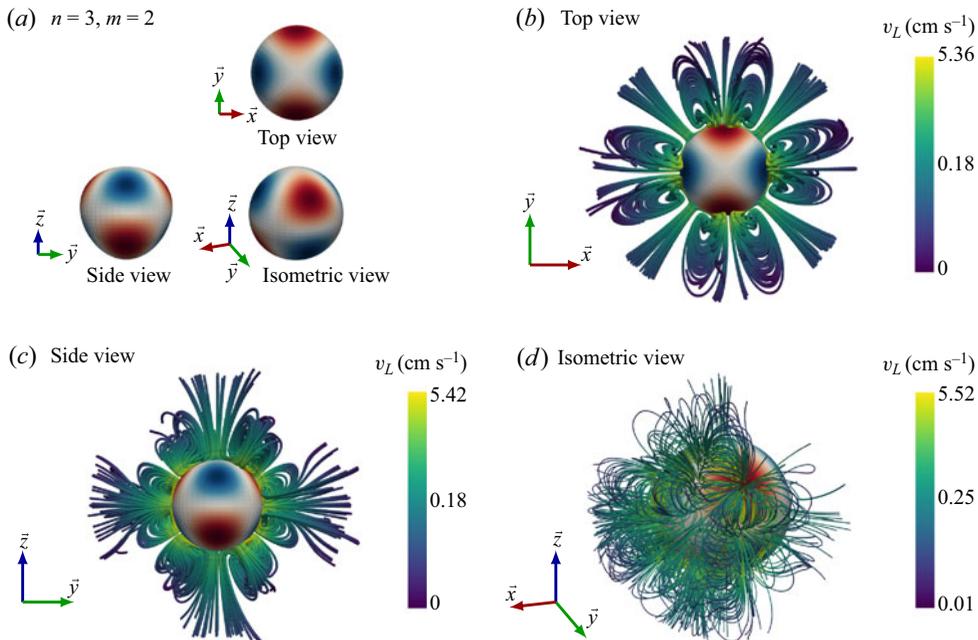


Figure 6. Presentation of the microstreaming pattern observed for a bubble (equilibrium radius  $73.8\ \mu\text{m}$ ) exhibiting tesseral oscillations on the mode ( $n = 3, m = 2$ ): (a) numerical contours of the bubble interface in the top, side and three-dimensional views; (b) top, (c) side and (d) isometric views of the resulting flow.

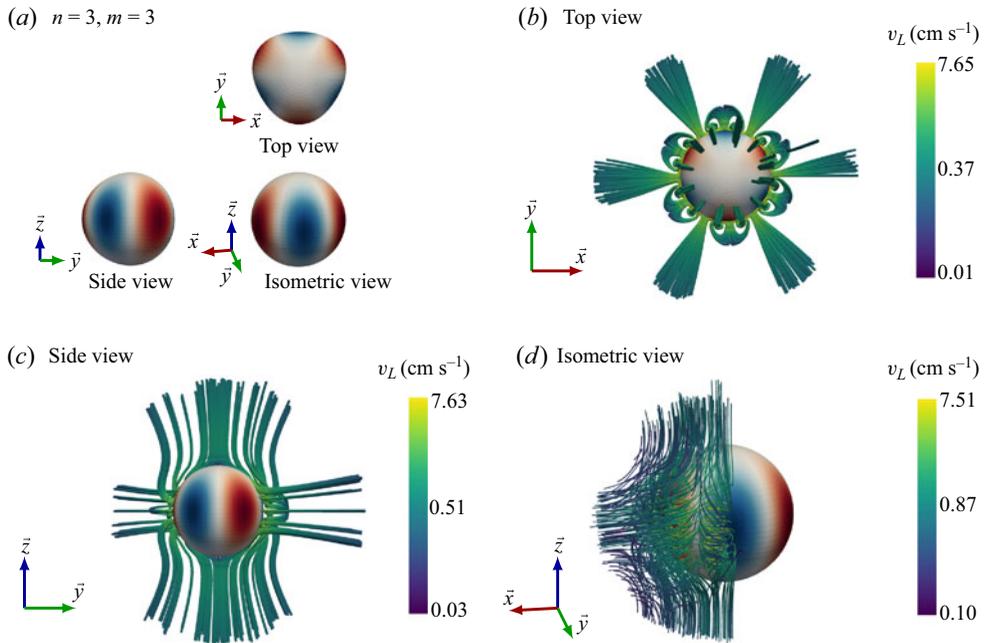


Figure 7. Presentation of the microstreaming pattern observed for a bubble (equilibrium radius  $73.8 \mu\text{m}$ ) exhibiting sectoral oscillations on the mode  $(n=3, m=3)$ : (a) numerical contours of the bubble interface in the top, side and three-dimensional views; (b) top, (c) side and (d) isometric views of the resulting flow.

pattern to the translation-induced quadrupole shape confirms the importance of capturing both the acoustic (high-frequency) dynamics of the bubble interface and the fluid flow, in order to avoid misinterpretation of the physical origin of the streaming pattern. In particular, from the top view, the tesseral  $m=1$  harmonic, whatever the degree  $n$ , always exhibits an up-and-down oscillation around the  $x$  axis that resembles the translational oscillation of the bubble along the  $y$  axis. From the side view, the bubble interface displays six extrema of displacement. It results in a recognisable 12-lobe flow pattern (figure 5c), where the lobes are arranged in pairs and are oriented from the extremum of the bubble interface towards the nearest displacement node. Combining these two views, and the fact that the fluid particles move from the anti-node towards the nearest displacement node on the bubble interface, the isometric view of the pattern can be guessed in figure 5(d).

The tesseral mode  $Y_3^2$  possesses  $m=2$  meridian nodal lines (figure 6a, top view) and  $n-m=1$  nodal parallels (figure 6a, side view). From the top view configuration, the bubble contour exhibits four nodes and four anti-nodes of displacement. Note that because the nodal parallel is located on the equator of the bubble interface, the so-called top view nodes and anti-nodes are located out of the equatorial plane. The resulting top view pattern (figure 6b) is characterised by a lobe-type pattern with  $4m=8$  recirculation loops arranged in pairs. The overall structure of the top view streaming is in good agreement with the experimental top view pattern displayed in figure 3(b) for another tesseral oscillation whose order also equals  $m=2$ . The microstreaming pattern from the side view (figure 6c) is harder to interpret as the bubble interface displays four extrema of displacement whose location is dependent on the orientation of the bubble around the  $z$  axis. Here, eight lobes are arranged in pairs and are superimposed on a cross-type pattern. A closer look at the pairs of lobes located at the poles ( $\theta=0$  and  $\theta=\pi$ ) reveals that the recirculation

loops are in fact split into two loops. This artefact is due to the slicing of the streamlines along the plane containing meridians. In fact, the isometric view (figure 6d) indicates how the streamlines start from the displacement anti-node located in the upper right corner in figure 6(d), and reach the nearest displacement nodes that form a triangular shape surrounding this anti-node. It results in a seemingly axisymmetric vortex around the normal at the bubble interface passing through the displacement anti-node.

The results for an asymmetric bubble experiencing sectoral oscillations on the mode  $Y_3^3$  are shown in figure 7. Being devoid of nodal parallels, the maximal longitudinal displacement occurs at the equatorial plane, where the bubble interface exhibits as many azimuthal lobes as the modal degree  $n$  to which it belongs. The amplitude of the oscillation displacement at a given acoustic phase decreases along the line going from the equator to the poles of the bubble. For  $n = 3$ , it results in  $2n = 6$  extrema for the displacement of the interface along the equator (figure 7a), an azimuthal shape that is easily recognisable from the top view observation. From the side view, the bubble contour is almost spherical, with an outgrowth located at the equator. Due to the (relative) simplicity of the bubble deformation along the elevation and the azimuthal direction, the resulting microstreaming pattern is easy to analyse from the top, side, and even isometric view. The top view is characterised by a  $4n = 12$ -lobe flower-like pattern, where the lobes are arranged in pairs around all extrema of the bubble interface displacement. This pattern is in good qualitative agreement with the experimental microstreaming pattern shown in figure 3(c), both for the number of recirculation loops and for the spatial extension of the vortices. The side view resembles a cross-like shape (figure 7c), typical of a quadrupole pattern. This pattern is the analogue of the top view streaming resulting from the tesseral mode  $m = 1$  (figure 5b) when switching from the top to the side view observation. Indeed, sectoral oscillations from the side view exhibit an out-of-phase motion along a meridian from one side of the bubble to the opposite one around the  $z$  axis, so that the oscillation seems like that of a solid-body translation oscillation. Because the sectoral harmonic  $Y_3^3$  possesses only meridian nodal lines, the vortices observed from the top view configuration spread with a decreasing amplitude towards the poles of the bubble (figure 7d).

The numerical streaming patterns obtained for the self-interacting tesseral (figure 6) or sectoral (figure 7) oscillations are found to be in good agreement with the patterns (figure 3) obtained by Fauconnier *et al.* (2022). Unlike the experimental observations of the latter, the present theory considers neither the presence of a wall in the bubble vicinity, nor the tethering of the bubble on a surface. It was shown in Fauconnier *et al.* (2020) that the contact angle between the bubble interface and the substrate lies in the range  $40^\circ$ – $60^\circ$ , with no dependence on the bubble equilibrium radius. It is also indicated that the contact angle remains the same after the activation of the ultrasound driving sequence. For this range of contact angle values, the bubble tethering does not influence strongly the dynamics of the oscillation, and the majority of the existing asymmetric oscillations for a given degree  $n$  are triggered. Concerning the resulting acoustic microstreaming, it is known that the mathematical modelling of the flow surrounding a free bubble, being far from any boundary, can be in fairly good agreement with the experimental flows in the form of a large-scale streaming induced by a substrate-attached bubble (Marmottant & Hilgenfeldt 2003). Here, in the case of asymmetric oscillations, the vortices with the highest velocity magnitude are confined in the close vicinity of the bubble interface (figure 7b) and extend much less than the large-scale quadrupole-like streaming. It can then be inferred that the influence of the bubble tethering on the resulting flow can be less pronounced in comparison to the case of an axisymmetric flow. In addition, it should be mentioned that our theory does not consider the effect of buoyancy, which may

cause the deviation of experimental streamlines from theoretical Lagrangian streamlines. This fact should be taken into account when comparing experimental results with our theory.

### 3.4. Extension to other spherical harmonics of any degree $n$

The previously investigated case of the microstreaming induced by the three classes of spherical harmonics for the same degree  $n = 3$  can help us in predicting the pattern for any asymmetric modes, whatever the degree  $n$  and order  $m$ . The simplest case concerns bubbles exhibiting zonal oscillations  $Y_n^0$ , for which theoretical predictions exist (Inserra *et al.* 2020a). Due to the absence of azimuthal dependence for the bubble displacement, the top view pattern of a zonal-induced microstreaming is unique and consists in a purely radial flow. Due to the axisymmetry of the zonal harmonics, slicing the three-dimensional microstreaming pattern in a plane containing the  $z$  axis always provides the same pattern, which consists of a large-scale cross pattern with small recirculation zones in the vicinity of the bubble interface. This general signature is identical whatever the degree  $n$  of the investigated zonal harmonics. Only the number of small vortices in the vicinity of the bubble interface increases as the degree  $n$  increases.

In general, a bubble exhibiting an asymmetric oscillation on a tesseral harmonic of order  $m$ , whatever the degree  $n$ , will exhibit the same top view patterns as shown in figure 5 when  $m = 1$ , or figure 6 when  $m = 2$ . Indeed, these patterns are uniquely linked to the number of meridian nodal lines, which equals  $m$ . For tesseral harmonics with higher order  $m$ , top view streaming will be characterised by a lobe-type pattern with  $4m$  lobes arranged in pairs. This top view signature of the pattern resulting from a self-interacting tesseral mode is similar to the shape obtained from another self-interacting spherical harmonics (obtained from a side or top view). This means that without knowing the bubble equilibrium radius and hence the degree  $n$  ruled by (2.73), the identification of the triggered mode at the bubble interface cannot be inferred when viewing the resulting streaming pattern. The analysis from the side view only is even more complicated, as the orientation of the focal plane around the  $z$  axis significantly affects the conformation of the captured flow.

The prediction of the microstreaming pattern induced by the class of sectoral harmonics is far easier to infer in comparison to the tesseral harmonics. All the sectoral harmonics  $m = n$  possess the same spatial conformation for the bubble displacement, with a maximal longitudinal displacement occurring at the equatorial plane. Along the equator, as many azimuthal lobes as the modal degree  $n$  to which they belong exist. The bubble displacement at the poles always tends to zero, so that the side view microstreaming pattern always resembles a cross-like shape, whatever the degree  $n$  of the sectoral oscillations. This is evidenced in figure 8, where the top and side view patterns resulting from self-interacting sectoral oscillations from  $n = 2$  to  $n = 5$  are shown. Here, the bubble equilibrium radii are chosen so that they correspond to the resonant radius of a given degree  $n$ :  $R_{res}^2 = 46 \mu\text{m}$  ( $\gamma = \delta_v/R_0 \sim 0.1$ ),  $R_{res}^3 = 68 \mu\text{m}$  ( $\gamma = \delta_v/R_0 \sim 0.06$ ),  $R_{res}^4 = 90 \mu\text{m}$  ( $\gamma = \delta_v/R_0 \sim 0.05$ ) and  $R_{res}^5 = 110 \mu\text{m}$  ( $\gamma = \delta_v/R_0 \sim 0.04$ ). The amplitudes of the two modes  $s^{(n,\pm n)}$  are set equal to  $15 \mu\text{m}$ , resulting in a stationary sectoral oscillation. The top view microstreaming is characterised by a lobe-type pattern where the lobes are arranged in pairs, and their number equals twice the number of extrema of the bubble displacement along the equator. Therefore, a  $4n$ -lobe shape is expected from the top view, as shown in figure 8. This signature is in full agreement with experimental observations of top view microstreaming patterns induced by sectoral oscillation for various degrees  $n$  in Fauconnier *et al.* (2022).

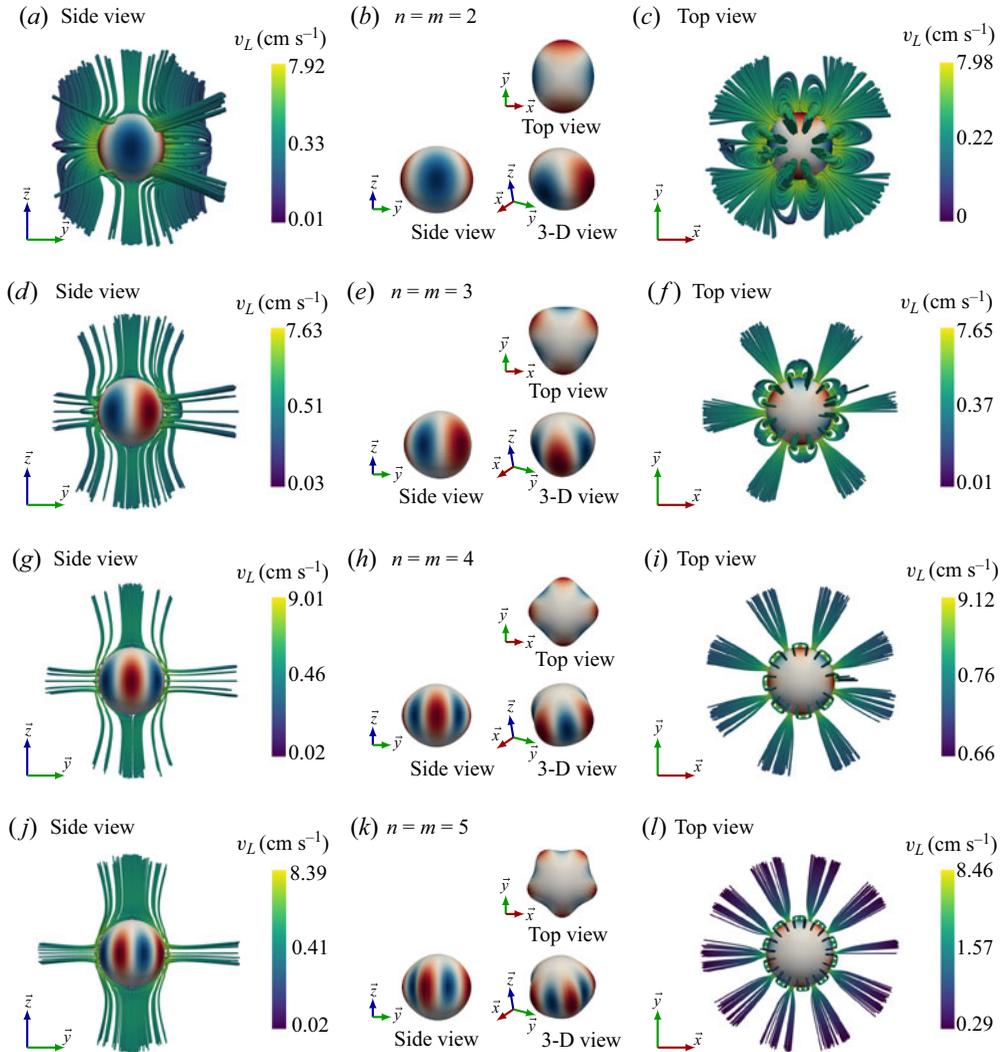


Figure 8. Presentation of the microstreaming pattern observed for various sectoral oscillations, with the degree  $n$  ranging from 2 to 5. Every line corresponds to a given degree  $n$ . (a,d,g,j) The projected side view microstreaming pattern. (b,e,h,k) The deformation of the bubble interface exhibiting the sectoral oscillation. (c,f,i,l) The top view microstreaming pattern.

### 3.5. Influence of the thickness of the viscous boundary layer on the streaming pattern

The acoustic microstreaming is driven by the streaming inside the oscillatory boundary layer around the bubble, while nonlinear second-order effects of the hydrodynamic equations are responsible for extending the streaming field much further than the viscous boundary layer. This explains why Elder (1959) reported different types of streaming patterns whose appearance depended mostly on the bubble surface velocity and the fluid viscosity. For a given bubble equilibrium radius and driving frequency, the influence of the thickness of the viscous boundary layer was investigated for varying values of the liquid viscosity in Doinikov *et al.* (2019a) and Inserra *et al.* (2020b) in the case of axisymmetric shape oscillations. For the translational oscillation of a solid body, Li *et al.* (2023) reveal changes in the structure of the streaming pattern for varying

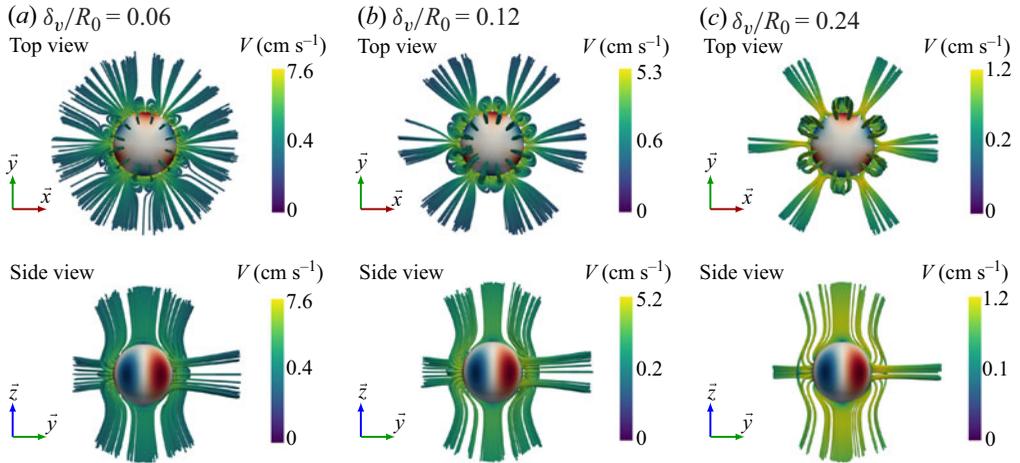


Figure 9. Evolution of the microstreaming pattern for the sectoral oscillation  $n = m = 3$  for varying values of the dimensionless thickness of the viscous boundary layer. The liquid dynamic viscosities and resulting dimensionless thickness of the viscous boundary layer are (a)  $\eta = 10^{-6}$  Pa s,  $\gamma = 0.06$ ; (b)  $\eta = 4 \times 10^{-6}$  Pa s,  $\gamma = 0.12$ , and (c)  $\eta = 16 \times 10^{-6}$  Pa s,  $\gamma = 0.24$ . Only the top and side views are displayed.

driving frequencies while keeping the body size and the liquid viscosity constant. Here, we investigate the influence of the value of the dimensionless thickness of the viscous boundary layer on the microstreaming pattern. We have previously considered the case (figure 7) of a sectoral oscillation  $n = m = 3$  at frequency  $f = 15.25$  kHz for a bubble with equilibrium radius  $73.8 \mu\text{m}$  in water (dynamic viscosity  $\eta = 10^{-6}$  Pa s). It corresponds to the dimensionless thickness of the viscous boundary layer  $\gamma = \delta_v/R_0 \sim 0.06$ . In order to modify the thickness of the viscous boundary layer  $\delta_v$ , the liquid viscosity is varied while keeping the bubble equilibrium radius and the oscillation frequency constant, so that the triggered shape oscillation given by (2.73) remains unchanged. For the same parameters as in figure 7, figure 9 presents the microstreaming patterns when the liquid viscosity is varied from  $\eta = 10^{-6}$  Pa s ( $\gamma = 0.06$ , figure 9a) to  $\eta = 4 \times 10^{-6}$  Pa s ( $\gamma = 0.12$ , figure 9b) and  $\eta = 16 \times 10^{-6}$  Pa s ( $\gamma = 0.24$ , figure 9c).

When the size of the viscous boundary layer is varied by four times, the overall structure of the streaming pattern remains unchanged: the top view is characterised by a 12-lobe flower-like pattern, and the side view looks like a cross (quadrupolar) shape. When the ratio  $\gamma = \delta_v/R_0$  is increased, the magnitude of the maximum streaming velocity decreases, while the size of the small vortices visible in the top view increases slightly. More pronounced modifications of the microstreaming pattern can be expected for large values of the dimensionless parameter  $\gamma$ , but such values would correspond to unrealistic experimental conditions (too large kinematic viscosity or a bubble size or driving frequency no longer matching (2.73)).

### 3.6. Sign reversal of the flow at the bubble zenith

Substrate-attached microbubbles are commonly used as microactuators for the trapping and manipulation of small particles or biological bodies in their vicinity. The hydrodynamic flow field generated by the bubble oscillation can rotate single microparticles within microchannels (Ahmed *et al.* 2016), precisely manipulate millimetric fish eggs (Lee *et al.* 2012), or manipulate and rupture vesicles (Marmottant *et al.* 2008). In most microfluidic applications, a substrate-attached microbubble experiences a combination of spherical and translational oscillations, at the origin of a

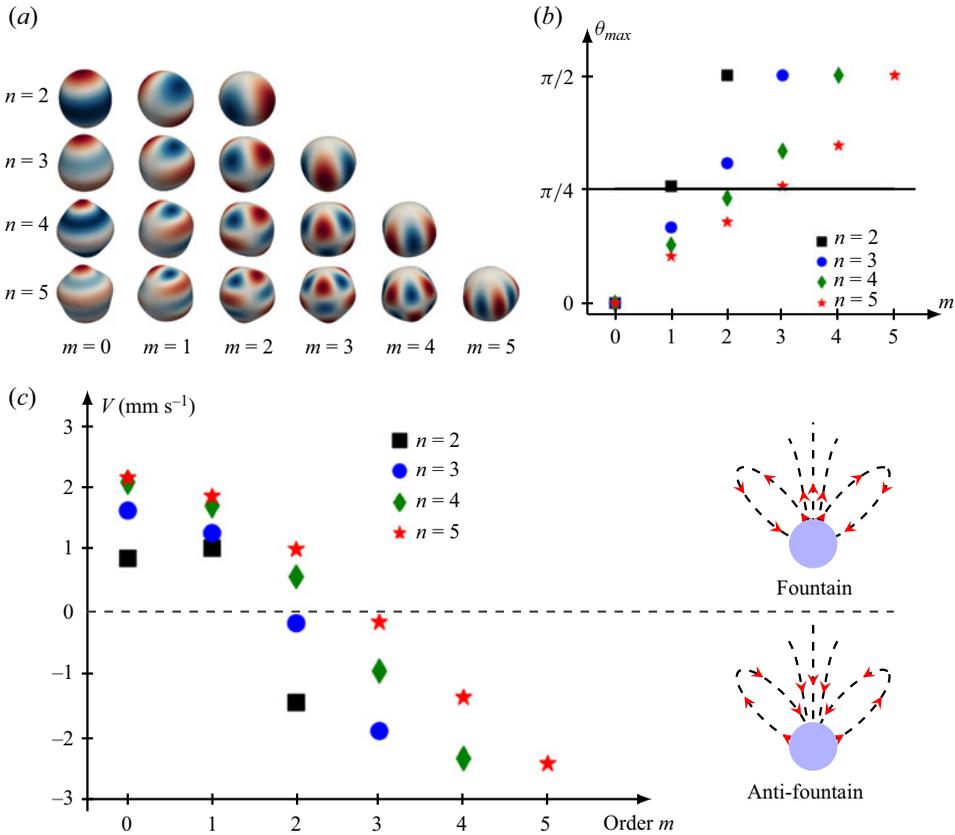


Figure 10. Investigation of the orientation of the flow at the zenith of the bubble ( $\theta = 0$ ). (a) Three-dimensional view of the bubble interface oscillating on asymmetric modes with  $n \in [2, 5]$ . (b) Evolution of the value of the colatitude  $\theta_{max}$  at which the displacement of the bubble interface is maximum, as a function of the order  $m$  for various degrees  $n$ . (c) Evolution of the amplitude of the radial velocity at the zenith ( $\theta = 0$ ) of the bubble, at the distance  $r = 3R_0$  as a function of the order  $m$  for various degrees  $n$ . A positive value corresponds to the fountain-like streaming, while a negative value is typical of the anti-fountain behaviour.

large-scale microstreaming pattern constituted of two symmetric vortices (in the plane of observation, from a side view) atop the bubble. When particles are injected near the oscillating bubble, they are expelled from the top bubble interface and move along a closed loop back to the substrate. This motion is often called fountain-like streaming, as the fluid particles are expelled from the bubble interface to the surrounding medium at the zenith ( $\theta = 0$ ) of the bubble. A similar fountain behaviour is obtained when axisymmetric modes are triggered at the bubble interface, because the zenith of the bubble interface is always a displacement anti-node, whatever the degree  $n$  of the zonal harmonics (see the first column of figure 10a). In the case of wall-bounded semi-cylindrical bubbles, Wang *et al.* (2013) and Rallabandi *et al.* (2014) have observed an inversion of the flow direction atop the bubble, identifying an anti-fountain behaviour of the vortices near the pole. This flow inversion was shown to result from the interaction between the radial oscillation and an axisymmetric shape oscillation (mixed-mode streaming). When asymmetric modes are triggered, the location of the maximum displacement on the bubble interface evolves as the order  $m$  increases, tending to a maximum at the equator of the bubble in the case of a sectoral mode. Figure 10(a) illustrates the three-dimensional bubble shapes for various degrees  $n$  ranging from 2 to 5. In addition, the value of the colatitude  $\theta_{max}$  at which

the location of the maximum displacement on the bubble interface occurs, whatever the value of the azimuthal angle  $\phi$ , is shown in [figure 10\(b\)](#). When the order  $m$  is smaller than  $(n + 1)/2$ ,  $\theta_{max}$  ranges from 0 to  $\pi/4$ , and the maximum displacement at the bubble interface is located in the upper part of the bubble, between the zenith and the bisector  $\theta_{max} = \pi/4$ . For higher values of  $m$ ,  $\theta_{max}$  gets closer to  $\pi/2$ , and the maximum displacement tends to the equatorial plane.

For the investigated asymmetric modes, the direction of the resulting microstreaming has been evaluated atop the bubble, at the radial distance  $r = 3R_0$  and for  $\theta = 0$ . [Figure 10\(c\)](#) shows the amplitude of the radial component of the Lagrangian velocity at this location. A sign reversal of the velocity amplitude occurs when the order  $m$  reaches  $(n + 1)/2$ , in agreement with the evolution of the colatitude  $\theta_{max}$ . In the case of zonal oscillations, the fluid particles are expelled (positive radial component of the velocity) from the zenith of the bubble, resulting in a fountain-like behaviour. In the case of sectoral oscillations, the analysis of the deformation of the bubble interface reveals that the maximum displacement occurs at the equator, while the zenith ( $\theta = 0$ ) of the bubble becomes a displacement node. The fluid particles are therefore expelled from the equator and are attracted from the zenith of the bubble to the bubble interface. This results in an anti-fountain behaviour, which has not been observed experimentally so far in the case of self-interacting mode streaming. It is worth noting that the observation of the flow direction atop the bubble indirectly provides information on the triggered shape oscillation, as the direction of the flow is correlated to the order  $m$  of the asymmetric oscillation. If the bubble equilibrium radius is known, then the degree  $n$  of the shape oscillations is obtained from the Lamb spectrum (2.73), and the range of possible triggered order  $m$  can be deduced from the observation of a fountain or anti-fountain flow.

### 3.7. The case of travelling surface waves

Up to now, only the stationary shape oscillations were considered, meaning that the amplitudes of the two modes  $s^{(n, \pm m)}$  were equal. A slight change in the amplitude of the surface perturbation propagating in one direction along the azimuthal angle  $\phi$  in comparison to the one propagating in the opposite direction will result in a quasi-stationary surface wave. Such a bubble will experience a rotating asymmetric surface wave, whose angular velocity will depend on the difference in the two amplitudes of modes  $(n, \pm m)$ . This has already been reported once in the literature by Mekki-Berrada, Thibault & Marmottant (2016), who measured a constant angular velocity of approximately 0.5 revolutions per second for every modal degree  $n$ , in the case of bubbles flattened between two elastic walls. The underlying cause for the triggering of a rotating shape oscillation so far remains unknown.

The case of travelling surface waves is investigated in [figure 11](#), for different ratios of the amplitudes of the two propagating modes  $(n, \pm m)$ . The case of the sectoral oscillation  $n = m = 3$  is investigated, for which the microstreaming pattern obtained in the case of a stationary wave is presented in [figure 7](#). Only the top and isometric views of the streaming pattern are displayed in [figure 11](#), and the amplitude of the  $(n, m)$  wave is kept equal to 15  $\mu\text{m}$ . When the amplitude of the  $(n, -m)$  wave is modified to 14.9  $\mu\text{m}$ , i.e. when  $s^{(n, -m)}/s^{(n, m)} = 0.99$ , streamlines are curved along the azimuthal direction ([figure 11\(a\)](#), top view) and the maximum amplitude of the Lagrangian velocity reaches 8.3  $\text{cm s}^{-1}$ . From [figure 7](#), it is worth noting that the maximum amplitude of the Lagrangian velocity reaches 7.65  $\text{cm s}^{-1}$  in the case of a stationary wave, i.e. when  $s^{(n, -m)}/s^{(n, m)} = 1$ . The increase in difference between the amplitudes of the two counter-propagating surface waves results in a stronger azimuthal component of the velocity field. The amplitude of

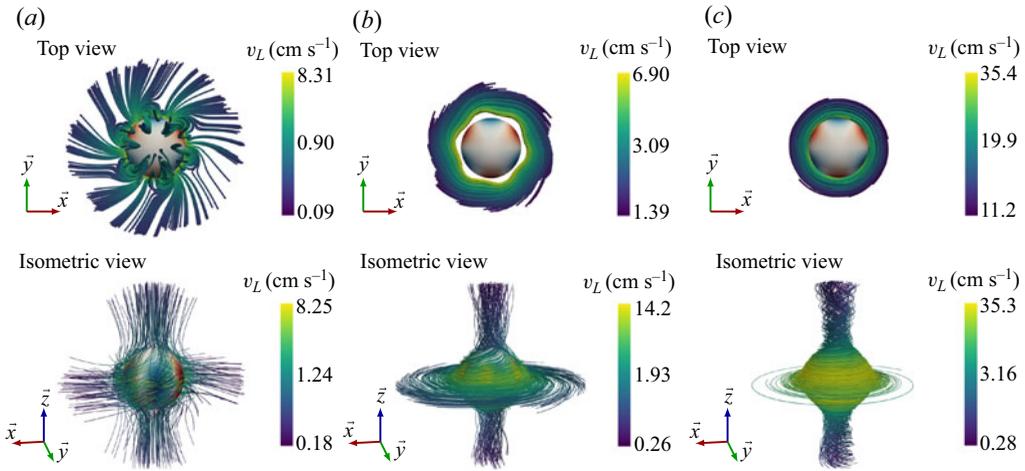


Figure 11. Evolution of the microstreaming pattern in the case of a quasi-stationary wave, for the sectoral oscillation  $n = m = 3$ . Three ratios of the amplitudes of the two modes  $s^{(n,-m)}/s^{(n,m)}$  are investigated for (a)  $s^{(n,-m)}/s^{(n,m)} = 0.99$ , (b)  $s^{(n,-m)}/s^{(n,m)} = 0.93$  and (c)  $s^{(n,-m)}/s^{(n,m)} = 0.66$ . Only the top and isometric views are displayed.

the streaming flow can increase by a factor of 2 (figure 11b) when  $s^{(n,-m)}/s^{(n,m)} = 0.93$ , or a factor of 4 (figure 11c) when  $s^{(n,-m)}/s^{(n,m)} = 0.66$ , in comparison to the stationary case.

The morphology of the swirling flow can be explained as follows. When the amplitudes  $s^{(n,\pm m)}$  of a given shape oscillation are set equal, a standing shape oscillation is formed on the bubble interface. This means that displacement anti-nodes (starting points of the streamlines) and nodes (end points of the streamlines) remain at the same location with time. The resulting flow is constituted of vortical lines that are spatially stationary. When the amplitudes  $s^{(n,\pm m)}$  of the two components of a shape oscillation differ, a quasi-propagating wave is triggered in a preferential direction on the bubble interface. ‘Quasi-propagating’ refers to the coexistence of a purely standing wave at the bubble interface and a purely propagating wave. Hence the locations of the displacement nodes and anti-nodes constantly move along the bubble interface with time. This prevents the spatial stationarity of the flow, so a convective-like flow is generated around the bubble. This flow follows the direction of propagation of the propagative surface wave, and is characterised by a strong azimuthal component of the flow velocity and a large-scale extension at the equator. However, why this flow is stronger in amplitude in comparison to the one induced by the standing wave alone is difficult to explain. Nevertheless, these results highlight the possibility to drastically enhance the streaming efficiency around bubbles if the bubble rotation can be controlled.

#### 4. Conclusion

We present for the first time a theoretical modelling of acoustic microstreaming induced by a bubble experiencing asymmetric oscillations. The modelling is based on the decomposition of the first- and second-order vorticity field into the poloidal and toroidal fields, allowing the exact analytical derivation of the Lagrangian streaming induced by the bubble. This derivation is valid whatever the bubble size and the liquid viscosity, without any limitation on the thickness of the viscous boundary layer at the bubble interface. By representing the shape of the bubble interface in terms of the set of

the orthonormal spherical harmonics, the signatures of the microstreaming patterns are investigated as a function of different classes of triggered spherical harmonics (zonal, tesseral or sectoral oscillations). Keeping in mind that the streamlines start from the displacement anti-node at the bubble interface, and close at the displacement nodes, the three-dimensional asymmetric patterns are shown to be easily predicted once the asymmetric shape deformation of the bubble is known. For a given class of spherical harmonics of degree  $n$ , it is shown that the sign reversal in the flow orientation atop the bubble is obtained when the order  $m$  evolves between 0 and  $n$ : zonal harmonics result in the fountain-like streaming, while the anti-fountain flow occurs in the case of sectoral oscillations. In between, the flow reverses for a typical value of the order  $m$  that helps in the identification of the triggered asymmetric mode by means of the indirect observation of the flow orientation. The case of travelling surface waves along the bubble interface reveals the possibility of a drastic enhancement of the streaming strength. This observation highlights the interest in the controlling of oscillations of rotating bubbles for practical use.

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### Appendix A. Calculation of $a_{nm}$ , $b_{nm}$ and $c_{nm}$

To find  $a_{nm}$ ,  $b_{nm}$  and  $c_{nm}$ , we apply boundary conditions at the bubble surface.

The first boundary condition requires that the normal component of  $\mathbf{v}_1^{(n,m)}$  at  $r = R_0$  be equal to the respective normal component of the bubble surface velocity. This condition is written as

$$v_{1r}^{(n,m)} \Big|_{r=R_0} = \frac{dr_s^{(n,m)}}{dt} = -i\omega s^{(n,m)} e^{-i\omega t} Y_n^m(\theta, \phi), \tag{A1}$$

where  $v_{1r}^{(n,m)}$  is the normal component of  $\mathbf{v}_1^{(n,m)}$ , and  $r_s^{(n,m)}$  is given by the second term of (2.1).

The second boundary condition assumes slippage on the bubble surface, which means that the tangential stress generated by the liquid motion should be zero on the bubble surface. This condition is written as

$$\sigma_{r\theta} = \eta \left( \frac{1}{r} \frac{\partial v_{1r}^{(n,m)}}{\partial \theta} + \frac{\partial v_{1\theta}^{(n,m)}}{\partial r} - \frac{v_{1\theta}^{(n,m)}}{r} \right) = 0 \quad \text{at } r = R_0, \tag{A2}$$

$$\sigma_{r\phi} = \eta \left( \frac{\partial v_{1\phi}^{(n,m)}}{\partial r} + \frac{1}{r \sin \theta} \frac{\partial v_{1r}^{(n,m)}}{\partial \phi} - \frac{v_{1\phi}^{(n,m)}}{r} \right) = 0 \quad \text{at } r = R_0, \tag{A3}$$

where  $\sigma_{r\theta}$  and  $\sigma_{r\phi}$  are the tangential components of the liquid stress in spherical coordinates (Landau & Lifshitz 1987). It should be mentioned that in the case when there are impurities and surfactants on the bubble surface, and in the case of a contrast agent bubble having a shell, the boundary condition of slippage should be replaced by the no-slip boundary condition, i.e. by the condition of adhesion of liquid particles to the bubble surface. In the case of a bubble with a shell, the behaviour of the shell material should also be taken into consideration. In view of its complexity, this case requires a separate study. The general algorithm of calculations remains the same, but all constants related to the boundary conditions at the bubble surface should be recalculated.

Substitution of (2.28) into (2.20) yields

$$\mathbf{v}_1^{(n,m)} = v_{1r}^{(n,m)} \mathbf{e}_r + v_{1\theta}^{(n,m)} \mathbf{e}_\theta + v_{1\phi}^{(n,m)} \mathbf{e}_\phi, \tag{A4}$$

$$v_{1r}^{(n,m)} = e^{-i\omega t} f_{nm}(r) Y_n^m(\theta, \phi), \tag{A5}$$

$$v_{1\theta}^{(n,m)} = e^{-i\omega t} \left[ \frac{a_{nm} k_v h_n^{(1)}(k_v r)}{\sin \theta} \frac{\partial Y_n^m(\theta, \phi)}{\partial \phi} + g_{nm}(r) \frac{\partial Y_n^m(\theta, \phi)}{\partial \theta} \right], \tag{A6}$$

$$v_{1\phi}^{(n,m)} = e^{-i\omega t} \left[ -a_{nm} k_v h_n^{(1)}(k_v r) \frac{\partial Y_n^m(\theta, \phi)}{\partial \theta} + \frac{g_{nm}(r)}{\sin \theta} \frac{\partial Y_n^m(\theta, \phi)}{\partial \phi} \right], \tag{A7}$$

where  $f_{nm}(r)$  and  $g_{nm}(r)$  are given by

$$f_{nm}(r) = \frac{(n+1) c_{nm}}{r^{n+2}} + \frac{n(n+1) b_{nm} h_n^{(1)}(k_v r)}{k_v r}, \tag{A8}$$

$$g_{nm}(r) = -\frac{c_{nm}}{r^{n+2}} + \frac{b_{nm}}{k_v r} \left[ (n+1) h_n^{(1)}(k_v r) - k_v r h_{n+1}^{(1)}(k_v r) \right]. \tag{A9}$$

Substituting (A5) and (A8) into (A1), one obtains

$$c_{nm} + \frac{n R_0^{n+2} h_n^{(1)}(\bar{x})}{\bar{x}} b_{nm} = -\frac{i\omega R_0^{n+2} s^{(n,m)}}{n+1}, \tag{A10}$$

where  $\bar{x} = k_v R_0$ .

Substitution of (A5)–(A7) into (A2) and (A3) yields

$$a_{nm} k_v \left[ \bar{x} h_n^{(1)'}(\bar{x}) - h_n^{(1)}(\bar{x}) \right] \frac{1}{\sin \theta} \frac{\partial Y_n^m(\theta, \phi)}{\partial \phi} + \left[ f_{nm}(R_0) - g_{nm}(R_0) + R_0 g'_{nm}(R_0) \right] \frac{\partial Y_n^m(\theta, \phi)}{\partial \theta} = 0, \tag{A11}$$

$$a_{nm} k_v \left[ h_n^{(1)}(\bar{x}) - \bar{x} h_n^{(1)'}(\bar{x}) \right] \frac{\partial Y_n^m(\theta, \phi)}{\partial \theta} + \left[ f_{nm}(R_0) - g_{nm}(R_0) + R_0 g'_{nm}(R_0) \right] \frac{1}{\sin \theta} \frac{\partial Y_n^m(\theta, \phi)}{\partial \phi} = 0, \tag{A12}$$

where

$$g'_{nm}(r) = \frac{(n+2) c_{nm}}{r^{n+3}} + \frac{b_{nm}}{k_v r^2} \left\{ (n+1) \left[ k_v r h_n^{(1)'}(k_v r) - h_n^{(1)}(k_v r) \right] - (k_v r)^2 h_{n+1}^{(1)'}(k_v r) \right\}. \tag{A13}$$

Multiplying (A11) by  $(\sin^{-1} \theta) \partial Y_n^m(\theta, \phi) / \partial \phi$  and subtracting (A12) multiplied by  $\partial Y_n^m(\theta, \phi) / \partial \theta$ , one obtains

$$a_{nm} \left[ \bar{x} h_n^{(1)'}(\bar{x}) - h_n^{(1)}(\bar{x}) \right] \left\{ \left[ \frac{1}{\sin \theta} \frac{\partial Y_n^m(\theta, \phi)}{\partial \phi} \right]^2 + \left[ \frac{\partial Y_n^m(\theta, \phi)}{\partial \theta} \right]^2 \right\} = 0. \tag{A14}$$

It follows from (A14) that

$$a_{nm} = 0. \tag{A15}$$

Accordingly, (A6) and (A7) take the form

$$v_{1\theta}^{(n,m)} = e^{-i\omega t} g_{nm}(r) \frac{\partial Y_n^m(\theta, \phi)}{\partial \theta}, \tag{A16}$$

$$v_{1\phi}^{(n,m)} = e^{-i\omega t} \frac{g_{nm}(r)}{\sin \theta} \frac{\partial Y_n^m(\theta, \phi)}{\partial \phi}. \tag{A17}$$

Multiplying (A11) by  $\partial Y_n^m(\theta, \phi)/\partial\theta$  and adding to (A12) multiplied by  $(\sin^{-1}\theta)\partial Y_n^m(\theta, \phi)/\partial\phi$ , one obtains

$$[f_{nm}(R_0) - g_{nm}(R_0) + R_0 g'_{nm}(R_0)] \left\{ \left[ \frac{\partial Y_n^m(\theta, \phi)}{\partial\theta} \right]^2 + \left[ \frac{1}{\sin\theta} \frac{\partial Y_n^m(\theta, \phi)}{\partial\phi} \right]^2 \right\} = 0. \tag{A18}$$

It follows from (A18) that

$$f_{nm}(R_0) - g_{nm}(R_0) + R_0 g'_{nm}(R_0) = 0. \tag{A19}$$

Substituting (A8) and (A9) into (A19) and using the identity

$$h_{n+1}^{(1)}(x) = \frac{n}{x} h_n^{(1)}(x) - h_n^{(1)'}(x), \tag{A20}$$

one obtains

$$\frac{2(n+2)}{R_0^{n+2}} c_{nm} + \frac{b_{nm}}{\bar{x}} \left[ (n^2 + n - 2) h_n^{(1)}(\bar{x}) + \bar{x}^2 h_n^{(1)''}(\bar{x}) \right] = 0. \tag{A21}$$

Combining (A10) and (A21), one finds

$$c_{nm} = s^{(n,m)} \frac{i\omega R_0^{n+2} \left[ (2 - n - n^2) h_n^{(1)}(\bar{x}) - \bar{x}^2 h_n^{(1)''}(\bar{x}) \right]}{(n+1) \left[ \bar{x}^2 h_n^{(1)''}(\bar{x}) - (n^2 + 3n + 2) h_n^{(1)}(\bar{x}) \right]}, \tag{A22}$$

$$b_{nm} = s^{(n,m)} \frac{2i(n+2)\bar{x}\omega}{(n+1) \left[ \bar{x}^2 h_n^{(1)''}(\bar{x}) - (n^2 + 3n + 2) h_n^{(1)}(\bar{x}) \right]}, \quad n \geq 1. \tag{A23}$$

### Appendix B. Solving the equations of acoustic streaming for the mode $(n, m)$

To solve (2.52) and (2.53), we first need to calculate their right-hand sides.

The calculation of  $\mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,m)}$  yields

$$\begin{aligned} \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,m)} &= \left( v_{1r}^{(n,m)} \frac{\partial}{\partial r} + \frac{v_{1\theta}^{(n,m)}}{r} \frac{\partial}{\partial\theta} + \frac{v_{1\phi}^{(n,m)}}{r \sin\theta} \frac{\partial}{\partial\phi} \right) \left( v_{1r}^{(n,m)} \mathbf{e}_r + v_{1\theta}^{(n,m)} \mathbf{e}_\theta + v_{1\phi}^{(n,m)} \mathbf{e}_\phi \right) \\ &= \mathbf{e}_r \left( v_{1r}^{(n,m)} \frac{\partial v_{1r}^{(n,m)}}{\partial r} + \frac{v_{1\theta}^{(n,m)}}{r} \frac{\partial v_{1r}^{(n,m)}}{\partial\theta} + \frac{v_{1\phi}^{(n,m)}}{r \sin\theta} \frac{\partial v_{1r}^{(n,m)}}{\partial\phi} - \frac{\left( v_{1\theta}^{(n,m)} \right)^2 + \left( v_{1\phi}^{(n,m)} \right)^2}{r} \right) \\ &+ \mathbf{e}_\theta \left( v_{1r}^{(n,m)} \frac{\partial v_{1\theta}^{(n,m)}}{\partial r} + \frac{v_{1\theta}^{(n,m)}}{r} \frac{\partial v_{1\theta}^{(n,m)}}{\partial\theta} + \frac{v_{1\phi}^{(n,m)}}{r \sin\theta} \frac{\partial v_{1\theta}^{(n,m)}}{\partial\phi} + \frac{v_{1r}^{(n,m)} v_{1\theta}^{(n,m)}}{r} - \frac{\cos\theta}{r \sin\theta} \left( v_{1\phi}^{(n,m)} \right)^2 \right) \\ &+ \mathbf{e}_\phi \left( v_{1r}^{(n,m)} \frac{\partial v_{1\phi}^{(n,m)}}{\partial r} + \frac{v_{1\theta}^{(n,m)}}{r} \frac{\partial v_{1\phi}^{(n,m)}}{\partial\theta} + \frac{v_{1\phi}^{(n,m)}}{r \sin\theta} \frac{\partial v_{1\phi}^{(n,m)}}{\partial\phi} + \frac{v_{1r}^{(n,m)} v_{1\phi}^{(n,m)}}{r} + \frac{\cos\theta}{r \sin\theta} v_{1\theta}^{(n,m)} v_{1\phi}^{(n,m)} \right). \end{aligned} \tag{B1}$$

Substituting (A5), (A16) and (A17) into (B1), and averaging it over time, one obtains

$$\begin{aligned} & \langle \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,m)} \rangle \\ &= \frac{1}{2} \text{Re} \left\{ \mathbf{e}_r \left[ f'_{nm} f_{nm}^* Y_n^m Y_n^{m*} + \frac{(f_{nm} - g_{nm}) g_{nm}^*}{r} \left( \frac{\partial Y_n^m}{\partial \theta} \frac{\partial Y_n^{m*}}{\partial \theta} + \frac{1}{\sin^2 \theta} \frac{\partial Y_n^m}{\partial \phi} \frac{\partial Y_n^{m*}}{\partial \phi} \right) \right] \right. \\ &+ \mathbf{e}_\theta \left[ f_{nm}^* \left( g'_{nm} + \frac{g_{nm}}{r} \right) Y_n^{m*} \frac{\partial Y_n^m}{\partial \theta} + \frac{|g_{nm}|^2}{r} \left( \frac{\partial Y_n^{m*}}{\partial \theta} \frac{\partial^2 Y_n^m}{\partial \theta^2} + \frac{1}{\sin^2 \theta} \frac{\partial Y_n^{m*}}{\partial \phi} \frac{\partial^2 Y_n^m}{\partial \theta \partial \phi} \right. \right. \\ &- \left. \left. \frac{\cos \theta}{\sin^3 \theta} \frac{\partial Y_n^{m*}}{\partial \phi} \frac{\partial Y_n^m}{\partial \phi} \right) \right] + \frac{\mathbf{e}_\phi}{\sin \theta} \left[ f_{nm}^* \left( g'_{nm} + \frac{g_{nm}}{r} \right) Y_n^{m*} \frac{\partial Y_n^m}{\partial \phi} \right. \\ &+ \left. \left. \frac{|g_{nm}|^2}{r} \left( \frac{\partial Y_n^{m*}}{\partial \theta} \frac{\partial^2 Y_n^m}{\partial \theta \partial \phi} + \frac{1}{\sin^2 \theta} \frac{\partial Y_n^{m*}}{\partial \phi} \frac{\partial^2 Y_n^m}{\partial \phi^2} \right) \right] \right\}. \end{aligned} \tag{B2}$$

For simplicity, we drop the arguments of the functions in (B2).

The calculation of  $\nabla \times \langle \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,m)} \rangle$ , after some rearrangements, results in

$$\begin{aligned} \nabla \times \langle \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,m)} \rangle &= \frac{1}{2} \text{Re} \left\{ \mathbf{e}_r \frac{f_{nm}^* (g_{nm} + r g'_{nm})}{r^2 \sin \theta} \left( \frac{\partial Y_n^m}{\partial \phi} \frac{\partial Y_n^{m*}}{\partial \theta} - \frac{\partial Y_n^{m*}}{\partial \phi} \frac{\partial Y_n^m}{\partial \theta} \right) \right. \\ &- \frac{(f_{nm}^* g_{nm} + r f_{nm}^* g'_{nm})'}{r} \left( \frac{\mathbf{e}_\theta}{\sin \theta} Y_n^{m*} \frac{\partial Y_n^m}{\partial \phi} - \mathbf{e}_\phi Y_n^{m*} \frac{\partial Y_n^m}{\partial \theta} \right) \\ &+ \frac{f_{nm} f_{nm}^* + f_{nm}^* f'_{nm}}{2r} \left[ \frac{\mathbf{e}_\theta}{\sin \theta} \frac{\partial}{\partial \phi} (Y_n^m Y_n^{m*}) - \mathbf{e}_\phi \frac{\partial}{\partial \theta} (Y_n^m Y_n^{m*}) \right] \\ &+ \frac{1}{2r} \left[ \frac{f_{nm} g_{nm}^* + f_{nm}^* g_{nm} - 2g_{nm} g_{nm}^*}{r} - (g_{nm} g_{nm}^*)' \right] \\ &\times \left[ \frac{\mathbf{e}_\theta}{\sin \theta} \frac{\partial}{\partial \phi} \left( \frac{\partial Y_n^m}{\partial \theta} \frac{\partial Y_n^{m*}}{\partial \theta} + \frac{1}{\sin^2 \theta} \frac{\partial Y_n^m}{\partial \phi} \frac{\partial Y_n^{m*}}{\partial \phi} \right) \right. \\ &- \left. \mathbf{e}_\phi \frac{\partial}{\partial \theta} \left( \frac{\partial Y_n^m}{\partial \theta} \frac{\partial Y_n^{m*}}{\partial \theta} + \frac{1}{\sin^2 \theta} \frac{\partial Y_n^m}{\partial \phi} \frac{\partial Y_n^{m*}}{\partial \phi} \right) \right] \right\}. \end{aligned} \tag{B3}$$

Comparison of (2.52) and (B3) leads to

$$\begin{aligned} & \sum_{k=1}^{\infty} \sum_{l=-k}^k k(k+1) \left[ P_{kl}^{(n,m)''} (r) - \frac{k(k+1) P_{kl}^{(n,m)} (r)}{r^2} \right] Y_k^l (\theta, \phi) \\ &= \frac{1}{2\nu} \text{Re} \left\{ \frac{f_{nm}^* (g_{nm} + r g'_{nm})}{\sin \theta} \left( \frac{\partial Y_n^m}{\partial \phi} \frac{\partial Y_n^{m*}}{\partial \theta} - \frac{\partial Y_n^{m*}}{\partial \phi} \frac{\partial Y_n^m}{\partial \theta} \right) \right\}. \end{aligned} \tag{B4}$$

With the help of (D8) and (D21), the right-hand side of (B4) is transformed so that (B4) takes the form

$$\begin{aligned} & \sum_{k=1}^{\infty} \sum_{l=-k}^k k(k+1) \left[ P_{kl}^{(n,m)''} (r) - \frac{k(k+1) P_{kl}^{(n,m)} (r)}{r^2} \right] Y_k^l (\theta, \phi) \\ &= \frac{1}{2\nu} \text{Re} \sum_{k=1}^{\infty} \sum_{l=-k}^k i m f_{nm}^* (g_{nm} + r g'_{nm}) \times \left[ n C_{(n+1)m} \left( B_{kl}^{(n+1)mnm} + B_{kl}^{nm(n+1)m} \right) \right. \\ &- \left. (n+1) C_{nm} \left( B_{kl}^{(n-1)mnm} + B_{kl}^{nm(n-1)m} \right) \right] Y_k^l (\theta, \phi), \end{aligned} \tag{B5}$$

where  $C_{nm}$  and  $B_{kl}^{n_1 m_1 n_2 m_2}$  are constants that are calculated by (D11) and (D22), respectively. In fact, (B5) involves only terms with  $l = 0$ , as  $m_1 = m_2 B_{kl}^{n_1 m_1 n_2 m_2} = 0$  for  $l \neq 0$ . This fact is in agreement with the right-hand side of (B4), which is independent of  $\phi$ .

Keeping only non-zero terms, one obtains from (B5),

$$P_{k0}^{(n,m)''}(r) - \frac{k(k+1)}{r^2} P_{k0}^{(n,m)}(r) = F_k^{(n,m)}(r), \tag{B6}$$

$$F_k^{(n,m)}(r) = \frac{m}{2k(k+1)v} \operatorname{Re} \left\{ i f_{nm}^*(r) [g_{nm}(r) + r g'_{nm}(r)] \right\} \\ \times \left[ n C_{(n+1)m} \left( B_{k0}^{(n+1)nmn} + B_{k0}^{nm(n+1)m} \right) - (n+1) C_{nm} \left( B_{k0}^{(n-1)nmn} + B_{k0}^{nm(n-1)m} \right) \right]. \tag{B7}$$

The calculation of the  $r$ -component of  $\nabla \times \nabla \times \langle \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,m)} \rangle$  gives

$$\mathbf{e}_r \cdot \left[ \nabla \times \nabla \times \langle \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,m)} \rangle \right] = \operatorname{Re} \left\{ \frac{f_{nm} f_{nm}^* + f_{nm}^* f'_{nm}}{4r^2} L^2 [Y_n^m Y_n^{m*}] \right. \\ \left. + \frac{f_{nm} g_{nm}^* + f_{nm}^* g_{nm} - 2g_{nm} g_{nm}^* - r (g_{nm} g_{nm}^*)'}{4r^3} L^2 \left[ \frac{\partial Y_n^m}{\partial \theta} \frac{\partial Y_n^{m*}}{\partial \theta} + \frac{m^2 Y_n^m Y_n^{m*}}{\sin^2 \theta} \right] \right. \\ \left. + \frac{(f_{nm}^* g_{nm} + r f_{nm}^* g'_{nm})'}{2r^2} \left[ \frac{\partial Y_n^m}{\partial \theta} \frac{\partial Y_n^{m*}}{\partial \theta} + \frac{m^2 Y_n^m Y_n^{m*}}{\sin^2 \theta} - n(n+1) Y_n^m Y_n^{m*} \right] \right\}, \tag{B8}$$

where  $L^2$  stands for the square of the orbital angular momentum operator (Varshalovich, Moskalev & Khersonskii 1988),

$$L^2 = -\frac{1}{\sin \theta} \frac{\partial}{\partial \theta} \sin \theta \frac{\partial}{\partial \theta} - \frac{1}{\sin^2 \theta} \frac{\partial^2}{\partial \phi^2}. \tag{B9}$$

By using (D5), it can be shown that the following identity holds:

$$-\frac{1}{2} L^2 [Y_n^m Y_n^{m*}] = \frac{\partial Y_n^m}{\partial \theta} \frac{\partial Y_n^{m*}}{\partial \theta} + \frac{m^2 Y_n^m Y_n^{m*}}{\sin^2 \theta} - n(n+1) Y_n^m Y_n^{m*}. \tag{B10}$$

Substitution of (B10) into (B8) yields

$$\mathbf{e}_r \cdot \left[ \nabla \times \nabla \times \langle \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,m)} \rangle \right] \\ = \frac{1}{8r^3} \operatorname{Re} \left\{ L^4 [Y_n^m Y_n^{m*}] \left[ 2g_{nm} g_{nm}^* - f_{nm} g_{nm}^* - f_{nm}^* g_{nm} + r (g_{nm} g_{nm}^*)' \right] \right. \\ \left. + 2L^2 [Y_n^m Y_n^{m*}] \left\{ r \left[ f_{nm} f_{nm}^* + f_{nm}^* f'_{nm} - (f_{nm}^* g_{nm} + r f_{nm}^* g'_{nm})' \right] \right. \right. \\ \left. \left. + n(n+1) \left[ f_{nm} g_{nm}^* + f_{nm}^* g_{nm} - 2g_{nm} g_{nm}^* - r (g_{nm} g_{nm}^*)' \right] \right\} \right\}. \tag{B11}$$

By using (D17) and the identity  $L^2 Y_k^l = k(k+1)Y_k^l$ , one obtains

$$\begin{aligned} \mathbf{e}_r \cdot \left[ \nabla \times \nabla \times \left\langle \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,m)} \right\rangle \right] &= \frac{1}{8r^3} \operatorname{Re} \sum_{k=1}^{\infty} \sum_{l=-k}^k k(k+1) A_{kl}^{nmnm} Y_k^l(\theta, \phi) \\ &\times \left\{ 2r \left[ f_{nm} f_{nm}' + f_{nm}^* f_{nm}' - (f_{nm}^* g_{nm} + r f_{nm}^* g_{nm}') \right] \right. \\ &\left. + [k(k+1) - 2n(n+1)] \left[ 2g_{nm} g_{nm}^* - f_{nm} g_{nm}^* - f_{nm}^* g_{nm} + r (g_{nm} g_{nm}^*)' \right] \right\}, \end{aligned} \tag{B12}$$

where the constant coefficients  $A_{kl}^{nmnm}$  are calculated by (D20). In fact, (B12) involves only terms with  $l = 0$  as  $A_{kl}^{nmnm} = 0$  for  $l \neq 0$ .

Comparing (2.53) with (B12), and keeping only non-zero terms, one obtains

$$\begin{aligned} T_{k0}^{(n,m)''}(r) - \frac{k(k+1)}{r^2} T_{k0}^{(n,m)}(r) &= G_k^{(n,m)}(r), \tag{B13} \\ G_k^{(n,m)}(r) &= \frac{A_{k0}^{nmnm}}{4\nu r} \operatorname{Re} \left\{ r f_{nm}^*(r) \left[ 2f_{nm}'(r) - 2g_{nm}'(r) - r g_{nm}''(r) \right] \right. \\ &\quad \left. - r f_{nm}'(r) \left[ g_{nm}(r) + r g_{nm}'(r) \right] \right. \\ &\quad \left. + [k(k+1) - 2n(n+1)] g_{nm}^*(r) \left[ g_{nm}(r) + r g_{nm}'(r) - f_{nm}(r) \right] \right\}. \end{aligned} \tag{B14}$$

The derivatives that appear in (B14) are calculated by

$$f_{nm}'(r) = -\frac{(n+1)(n+2)c_{nm}}{r^{n+3}} + \frac{n(n+1)b_{nm}}{k_v r^2} \left[ (n-1)h_n^{(1)}(k_v r) - k_v r h_{n+1}^{(1)}(k_v r) \right], \tag{B15}$$

$$g_{nm}'(r) = \frac{(n+2)c_{nm}}{r^{n+3}} + \frac{b_{nm}}{k_v r^2} \left\{ \left[ n^2 - 1 - (k_v r)^2 \right] h_n^{(1)}(k_v r) + k_v r h_{n+1}^{(1)}(k_v r) \right\}, \tag{B16}$$

$$\begin{aligned} g_{nm}''(r) &= -\frac{(n+2)(n+3)c_{nm}}{r^{n+4}} + \frac{b_{nm}}{k_v r^3} \left\{ 2(1-n^2)h_n^{(1)}(k_v r) \right. \\ &\quad \left. + k_v r \left[ n^2 - 1 - (k_v r)^2 \right] h_n^{(1)'}(k_v r) - k_v r h_{n+1}^{(1)}(k_v r) + (k_v r)^2 h_{n+1}^{(1)'}(k_v r) \right\}. \end{aligned} \tag{B17}$$

Equations (B6) and (B13) are solved by the method of variation of parameters (Boyce & DiPrima 2001). According to this method, a solution to (B6) is given by

$$P_{k0}^{(n,m)}(r) = r^{k+1} C_{1k}^{(n,m)}(r) + r^{-k} C_{2k}^{(n,m)}(r), \tag{B18}$$

where  $C_{1k}^{(n,m)}(r)$  and  $C_{2k}^{(n,m)}(r)$  obey the equations

$$r^{k+1} C_{1k}^{(n,m)'}(r) + r^{-k} C_{2k}^{(n,m)'}(r) = 0, \tag{B19}$$

$$(k+1)r^k C_{1k}^{(n,m)'}(r) - k r^{-k-1} C_{2k}^{(n,m)'}(r) = F_k^{(n,m)}(r). \tag{B20}$$

Solving (B19) and (B20) gives

$$C_{1k}^{(n,m)}(r) = \bar{C}_{1k}^{(n,m)} + \frac{1}{2k+1} \int_{R_0}^r s^{-k} F_k^{(n,m)}(s) ds, \tag{B21}$$

$$C_{2k}^{(n,m)}(r) = \bar{C}_{2k}^{(n,m)} - \frac{1}{2k+1} \int_{R_0}^r s^{k+1} F_k^{(n,m)}(s) ds, \tag{B22}$$

where  $\bar{C}_{1k}^{(n,m)}$  and  $\bar{C}_{2k}^{(n,m)}$  are constants. From the condition that the acoustic streaming vanishes at infinity, one finds

$$\bar{C}_{1k}^{(n,m)} = -\frac{1}{2k+1} \int_{R_0}^{\infty} s^{-k} F_k^{(n,m)}(s) ds, \tag{B23}$$

while  $\bar{C}_{2k}^{(n,m)}$  is calculated by boundary conditions at the bubble surface; see below.

Equation (B13) is similar to (B6), so its solution can be written by analogy,

$$T_{k0}^{(n,m)}(r) = r^{k+1} C_{3k}^{(n,m)}(r) + r^{-k} C_{4k}^{(n,m)}(r), \tag{B24}$$

$$C_{3k}^{(n,m)}(r) = \bar{C}_{3k}^{(n,m)} + \frac{1}{2k+1} \int_{R_0}^r s^{-k} G_k^{(n,m)}(s) ds, \tag{B25}$$

$$C_{4k}^{(n,m)}(r) = \bar{C}_{4k}^{(n,m)} - \frac{1}{2k+1} \int_{R_0}^r s^{k+1} G_k^{(n,m)}(s) ds, \tag{B26}$$

$$\bar{C}_{3k}^{(n,m)} = -\frac{1}{2k+1} \int_{R_0}^{\infty} s^{-k} G_k^{(n,m)}(s) ds, \tag{B27}$$

where  $\bar{C}_{4k}^{(n,m)}$  is a constant to be calculated by boundary conditions at the bubble surface; see below.

Continuing the calculation of  $\mathbf{v}_E^{(n,m)}$ , one obtains from (2.50),

$$\begin{aligned} \mathbf{v}_E^{(n,m)} = \nabla \times & \left[ \mathbf{e}_r \sum_{k=1}^{\infty} \sum_{l=-k}^k P_{kl}^{(n,m)}(r) Y_k^l(\theta, \phi) \right] \\ & + \mathbf{e}_r \sum_{k=1}^{\infty} \sum_{l=-k}^k T_{kl}^{(n,m)}(r) Y_k^l(\theta, \phi) + \nabla \Phi^{(n,m)}(r, \theta, \phi). \end{aligned} \tag{B28}$$

It follows from (2.44) that

$$\begin{aligned} \Delta \Phi^{(n,m)}(r, \theta, \phi) = & - \sum_{k=1}^{\infty} \sum_{l=-k}^k \nabla \cdot [T_{kl}^{(n,m)}(r) Y_k^l(\theta, \phi) \mathbf{e}_r] \\ = & - \sum_{k=1}^{\infty} \sum_{l=-k}^k [T_{kl}^{(n,m)'}(r) + 2r^{-1} T_{kl}^{(n,m)}(r)] Y_k^l(\theta, \phi). \end{aligned} \tag{B29}$$

In fact, (B29) involves only terms with  $l = 0$  as  $T_{kl}^{(n,m)}(r) = 0$  for  $l \neq 0$ .

We assume that

$$\Phi^{(n,m)}(r, \theta, \phi) = \sum_{k=1}^{\infty} \sum_{l=-k}^k \Phi_{kl}^{(n,m)}(r) Y_k^l(\theta, \phi). \tag{B30}$$

Substituting (B30) into (B29), using (B24) and keeping only non-zero terms, one has

$$\Phi_{k0}^{(n,m)''}(r) + \frac{2}{r} \Phi_{k0}^{(n,m)'}(r) - \frac{k(k+1)}{r^2} \Phi_{k0}^{(n,m)}(r) = H_k^{(n,m)}(r), \tag{B31}$$

where

$$\begin{aligned} H_k^{(n,m)}(r) = & -T_{k0}^{(n,m)'}(r) - 2r^{-1} T_{k0}^{(n,m)}(r) \\ = & -(k+3) r^k C_{3k}^{(n,m)}(r) + (k-2) r^{-k-1} C_{4k}^{(n,m)}(r). \end{aligned} \tag{B32}$$

Equation (B31) is solved by the method of variation of parameters, which results in

$$\Phi_{k0}^{(n,m)}(r) = r^k C_{5k}^{(n,m)}(r) + r^{-k-1} C_{6k}^{(n,m)}(r), \tag{B33}$$

where  $C_{5k}^{(n,m)}(r)$  and  $C_{6k}^{(n,m)}(r)$  obey the equations

$$r^k C_{5k}^{(n,m)'}(r) + r^{-k-1} C_{6k}^{(n,m)'}(r) = 0, \tag{B34}$$

$$kr^{k-1} C_{5k}^{(n,m)'}(r) - (k+1)r^{-k-2} C_{6k}^{(n,m)'}(r) = H_k^{(n,m)}(r). \tag{B35}$$

Solving (B34) and (B35) gives

$$C_{5k}^{(n,m)}(r) = \bar{C}_{5k}^{(n,m)} + \frac{1}{2k+1} \int_{R_0}^r s^{1-k} H_k^{(n,m)}(s) ds, \tag{B36}$$

$$C_{6k}^{(n,m)}(r) = \bar{C}_{6k}^{(n,m)} - \frac{1}{2k+1} \int_{R_0}^r s^{k+2} H_k^{(n,m)}(s) ds. \tag{B37}$$

The constant  $\bar{C}_{6k}^{(n,m)}$  is calculated by boundary conditions at the bubble surface; see below.

From the condition that the acoustic streaming vanishes at infinity, one finds

$$\bar{C}_{5k}^{(n,m)} = -\frac{1}{2k+1} \int_{R_0}^{\infty} s^{1-k} H_k^{(n,m)}(s) ds. \tag{B38}$$

Substituting (B32) into (B38) and using (B26), one obtains

$$\bar{C}_{5k}^{(n,m)} = -\frac{(k-2)\bar{C}_{4k}^{(n,m)}}{(4k^2-1)R_0^{2k-1}} + I_k^{(n,m)}, \tag{B39}$$

$$I_k^{(n,m)} = \frac{k+3}{2k+1} \int_{R_0}^{\infty} r C_{3k}^{(n,m)}(r) dr + \frac{k-2}{(2k+1)^2} \int_{R_0}^{\infty} \left[ \int_{R_0}^r s^{k+1} G_k^{(n,m)}(s) ds \right] \frac{dr}{r^{2k}}. \tag{B40}$$

Substitution of (B30) into (B28) yields

$$\begin{aligned} v_E^{(n,m)} = & \sum_{k=1}^{\infty} \sum_{l=-k}^k \left\{ \mathbf{e}_r \left[ T_{kl}^{(n,m)}(r) + \Phi_{kl}^{(n,m)'}(r) \right] Y_k^l(\theta, \phi) \right. \\ & + \frac{\Phi_{kl}^{(n,m)}(r)}{r} \left[ \mathbf{e}_\theta \frac{\partial Y_k^l(\theta, \phi)}{\partial \theta} + \frac{\mathbf{e}_\phi}{\sin \theta} \frac{\partial Y_k^l(\theta, \phi)}{\partial \phi} \right] \\ & \left. + \frac{P_{kl}^{(n,m)}(r)}{r} \left[ \frac{\mathbf{e}_\theta}{\sin \theta} \frac{\partial Y_k^l(\theta, \phi)}{\partial \phi} - \mathbf{e}_\phi \frac{\partial Y_k^l(\theta, \phi)}{\partial \theta} \right] \right\}. \end{aligned} \tag{B41}$$

Keeping only non-zero terms (those with  $l=0$ ) and using (D1) and (D9), one obtains

$$v_{Er}^{(n,m)} = \frac{1}{2\sqrt{\pi}} \sum_{k=1}^{\infty} \sqrt{2k+1} \left[ T_{k0}^{(n,m)}(r) + \Phi_{k0}^{(n,m)'}(r) \right] P_k(\cos \theta), \tag{B42}$$

$$v_{E\theta}^{(n,m)} = \frac{1}{2\sqrt{\pi}r} \sum_{k=1}^{\infty} \sqrt{2k+1} \Phi_{k0}^{(n,m)}(r) P_k^1(\cos \theta), \tag{B43}$$

$$v_{E\phi}^{(n,m)} = -\frac{1}{2\sqrt{\pi}r} \sum_{k=1}^{\infty} \sqrt{2k+1} P_{k0}^{(n,m)}(r) P_k^1(\cos \theta). \tag{B44}$$

Equation (B42) involves  $\Phi_{k0}^{(n,m)}/(r)$ , which is calculated by (B33) and (B34) to be

$$\Phi_{k0}^{(n,m)}/(r) = kr^{k-1}C_{5k}^{(n,m)}(r) - (k+1)r^{-k-2}C_{6k}^{(n,m)}(r). \tag{B45}$$

In order to go on with the calculation, we need to apply boundary conditions for acoustic streaming at the bubble surface. To do this, we need to know the Stokes drift velocity (Longuet-Higgins 1998), which is calculated by (Doinikov *et al.* 2019a)

$$\mathbf{v}_S^{(n,m)} = \frac{1}{2\omega} \operatorname{Re} \left\{ i \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,m)*} \right\}. \tag{B46}$$

Equation (B46) gives

$$v_{Sr}^{(n,m)} = -\frac{1}{2\omega} \operatorname{Im} \left\{ v_{1r}^{(n,m)} \frac{\partial v_{1r}^{(n,m)*}}{\partial r} + \frac{v_{1\theta}^{(n,m)}}{r} \frac{\partial v_{1r}^{(n,m)*}}{\partial \theta} + \frac{v_{1\phi}^{(n,m)}}{r \sin \theta} \frac{\partial v_{1r}^{(n,m)*}}{\partial \phi} \right\}, \tag{B47}$$

$$v_{S\theta}^{(n,m)} = -\frac{1}{2\omega} \operatorname{Im} \left\{ v_{1r}^{(n,m)} \frac{\partial v_{1\theta}^{(n,m)*}}{\partial r} + \frac{v_{1\theta}^{(n,m)}}{r} \frac{\partial v_{1\theta}^{(n,m)*}}{\partial \theta} + \frac{v_{1\phi}^{(n,m)}}{r \sin \theta} \frac{\partial v_{1\theta}^{(n,m)*}}{\partial \phi} + \frac{v_{1r}^{(n,m)*} v_{1\theta}^{(n,m)}}{r} \right\}, \tag{B48}$$

$$v_{S\phi}^{(n,m)} = -\frac{1}{2\omega} \operatorname{Im} \left\{ v_{1r}^{(n,m)} \frac{\partial v_{1\phi}^{(n,m)*}}{\partial r} + \frac{v_{1\theta}^{(n,m)}}{r} \frac{\partial v_{1\phi}^{(n,m)*}}{\partial \theta} + \frac{v_{1\phi}^{(n,m)}}{r \sin \theta} \frac{\partial v_{1\phi}^{(n,m)*}}{\partial \phi} + \frac{v_{1\phi}^{(n,m)} v_{1r}^{(n,m)*}}{r} + \frac{\cos \theta v_{1\phi}^{(n,m)} v_{1\theta}^{(n,m)*}}{r \sin \theta} \right\}. \tag{B49}$$

Substituting (A5), (A16) and (A17) into (B47)–(B49) and using (D6), one obtains

$$v_{Sr}^{(n,m)} = -\frac{1}{2\omega} \operatorname{Re} \left\{ i f_{nm}^* f'_{nm} Y_n^m Y_n^{m*} + \frac{i f_{nm} g_{nm}^*}{r} \left( \frac{\partial Y_n^m}{\partial \theta} \frac{\partial Y_n^{m*}}{\partial \theta} + \frac{m^2 Y_n^m Y_n^{m*}}{\sin^2 \theta} \right) \right\}, \tag{B50}$$

$$v_{S\theta}^{(n,m)} = -\frac{1}{4\omega} \operatorname{Re} \left\{ i \left[ f_{nm}^* g'_{nm} - \frac{(f_{nm}^* - n(n+1)g_{nm}^*)g_{nm}}{r} \right] \frac{\partial (Y_n^m Y_n^{m*})}{\partial \theta} \right\}, \tag{B51}$$

$$v_{S\phi}^{(n,m)} = \frac{m}{2\omega} \operatorname{Re} \left\{ f_{nm}^* \left( g'_{nm} - \frac{g_{nm}}{r} \right) \frac{Y_n^m Y_n^{m*}}{\sin \theta} + \frac{g_{nm} g_{nm}^*}{r \sin \theta} \left( \frac{\partial Y_n^m}{\partial \theta} \frac{\partial Y_n^{m*}}{\partial \theta} + \frac{m^2 Y_n^m Y_n^{m*}}{\sin^2 \theta} - \frac{2 \cos \theta}{\sin \theta} Y_n^m \frac{\partial Y_n^{m*}}{\partial \theta} \right) \right\}. \tag{B52}$$

With the help of (B10) and (D17), (B50) is represented by

$$\begin{aligned} v_{Sr}^{(n,m)} &= -\frac{1}{2\omega} \operatorname{Re} \left\{ i \left[ f_{nm}^* f'_{nm} + \frac{n(n+1) f_{nm} g_{nm}^*}{r} \right] Y_n^m Y_n^{m*} - \frac{i f_{nm} g_{nm}^*}{2r} L^2 [Y_n^m Y_n^{m*}] \right\} \\ &= \frac{1}{2\omega} \operatorname{Re} \sum_{k=1}^{\infty} \sum_{l=-k}^k i A_{kl}^{nmm} \left[ \frac{k(k+1) - 2n(n+1)}{2r} f_{nm} g_{nm}^* - f_{nm}^* f'_{nm} \right] Y_k^l(\theta, \phi). \end{aligned} \tag{B53}$$

Keeping only non-zero terms and using (D1), one obtains

$$v_{Sr}^{(n,m)} = \frac{1}{4\sqrt{\pi}\omega} \sum_{k=1}^{\infty} \sqrt{2k+1} A_{k0}^{nmnm} \times \operatorname{Re} \left\{ i f_{nm}^* (r) \left[ \frac{2n(n+1) - k(k+1)}{2r} g_{nm}(r) - f'_{nm}(r) \right] \right\} P_k(\cos \theta). \tag{B54}$$

Substitution of (D17) into (B51) yields

$$v_{S\theta}^{(n,m)} = \frac{1}{4\omega} \operatorname{Re} \sum_{k=1}^{\infty} \sum_{l=-k}^k i A_{kl}^{nmnm} \left\{ \frac{g_{nm} [f_{nm}^* - n(n+1)g_{nm}^*]}{r} - f_{nm}^* g'_{nm} \right\} \frac{\partial Y_k^l(\theta, \phi)}{\partial \theta}. \tag{B55}$$

Keeping only non-zero terms and using (D1) and (D9), one obtains

$$v_{S\theta}^{(n,m)} = \frac{1}{8\sqrt{\pi}\omega} \operatorname{Re} \left\{ i f_{nm}^* (r) \left[ \frac{g_{nm}(r)}{r} - g'_{nm}(r) \right] \right\} \sum_{k=1}^{\infty} \sqrt{2k+1} A_{k0}^{nmnm} P_k^1(\cos \theta). \tag{B56}$$

With the help of (B10), (B52) is represented by

$$v_{S\phi}^{(n,m)} = \frac{m}{2\omega} \operatorname{Re} \left\{ \left[ f_{nm}^* \left( g'_{nm} - \frac{g_{nm}}{r} \right) + \frac{n(n+1)|g_{nm}|^2}{r} \right] \frac{Y_n^m Y_n^{m*}}{\sin \theta} + \frac{|g_{nm}|^2}{r} \frac{\partial}{\partial \theta} \left( \frac{Y_n^{m*}}{\sin \theta} \frac{\partial Y_n^m}{\partial \theta} \right) \right\}. \tag{B57}$$

Note that  $v_{S\phi}^{(n,m)} = 0$  for  $m = 0$ . For  $n = m = 1$ , with the help of (D1), (B57) is represented by

$$v_{S\phi}^{(1,1)} = E^{(1,1)}(r) P_1^1(\cos \theta), \tag{B58}$$

$$E^{(1,1)}(r) = \frac{3}{16\pi\omega r} \operatorname{Re} \left\{ f_{11}^*(r) [g_{11}(r) - r g'_{11}(r)] - |g_{11}(r)|^2 \right\}. \tag{B59}$$

For  $n > 1$ , by using (D23), (D24), (D1), (D3) and (D15), keeping only non-zero terms, (B57) is represented by

$$v_{S\phi}^{(n,m)} = \sum_{k=1}^{\infty} E_k^{(n>1,m)}(r) P_k^1(\cos \theta), \tag{B60}$$

where

$$E_k^{(n>1,m)}(r) = \frac{m\sqrt{2k+1}}{4\sqrt{\pi}\omega r} \left\{ \left[ n C_{(n+1)m} B_{k0}^{(n+1)mnm} - (n+1) C_{nm} B_{k0}^{(n+1)mnm} \right] |g_{nm}(r)|^2 - \sqrt{\frac{(2n+1)(n-m)!}{(n+m)!}} \operatorname{Re} \left\{ f_{nm}^*(r) [g_{nm}(r) - r g'_{nm}(r)] - n(n+1)|g_{nm}(r)|^2 \right\} \times \frac{1}{\sqrt{k(k+1)}} \sum_{s=1}^{\left[ \frac{(n-m+2)}{2} \right]} \sqrt{\frac{(2n-4s+3)(n+m-2s)!}{(n-m-2s+2)!}} A_{k(-1)}^{(n-2s+1)(m-1)nm} \right\}. \tag{B61}$$

Equations (B58) and (B60) can be combined as follows:

$$v_{S\phi}^{(n,m)} = \sum_{k=1}^{\infty} E_k^{(n,m)}(r) P_k^1(\cos \theta), \tag{B62}$$

where

$$E_k^{(n,m)}(r) = \begin{cases} E^{(1,1)}(r) \delta_{1k}, & n = 1, \\ E_k^{(n>1,m)}(r), & n > 1. \end{cases} \tag{B63}$$

We can now apply the boundary conditions for the acoustic streaming at the bubble surface. They are given by

$$v_{Lr}^{(n,m)} = 0 \quad \text{at } r = R_0, \tag{B64}$$

$$\sigma_{Lr\theta}^{(n,m)} = \eta \left( \frac{1}{r} \frac{\partial v_{Lr}^{(n,m)}}{\partial \theta} + \frac{\partial v_{L\theta}^{(n,m)}}{\partial r} - \frac{v_{L\theta}^{(n,m)}}{r} \right) = 0 \quad \text{at } r = R_0, \tag{B65}$$

$$\sigma_{Lr\phi}^{(n,m)} = \eta \left( \frac{\partial v_{L\phi}^{(n,m)}}{\partial r} + \frac{1}{r \sin \theta} \frac{\partial v_{Lr}^{(n,m)}}{\partial \phi} - \frac{v_{L\phi}^{(n,m)}}{r} \right) = 0 \quad \text{at } r = R_0, \tag{B66}$$

where  $\mathbf{v}_L^{(n,m)} = \mathbf{v}_E^{(n,m)} + \mathbf{v}_S^{(n,m)}$  is the Lagrangian streaming velocity, and  $\sigma_{Lr\theta}^{(n,m)}$  and  $\sigma_{Lr\phi}^{(n,m)}$  are the tangential components of the stress produced by  $\mathbf{v}_L^{(n,m)}$ . We use (B64)–(B66) in order to calculate the constants  $\bar{C}_{2k}^{(n,m)}$ ,  $\bar{C}_{4k}^{(n,m)}$  and  $\bar{C}_{6k}^{(n,m)}$ .

Substituting (B42) and (B54) into (B64), one obtains

$$T_{k0}^{(n,m)}(R_0) + \Phi_{k0}^{(n,m)'}(R_0) = Q_k^{(n,m)}, \tag{B67}$$

where

$$Q_k^{(n,m)} = \frac{A_{k0}^{nmnm}}{2\omega} \operatorname{Re} \left\{ i f_{nm}^* (R_0) \left[ f_{nm}' (R_0) + \frac{k(k+1) - 2n(n+1)}{2R_0} g_{nm} (R_0) \right] \right\}. \tag{B68}$$

To calculate  $\sigma_{Lr\theta}^{(n,m)}$ , we use (B42), (B43), (B54) and (B56):

$$\begin{aligned} \sigma_{Lr\theta}^{(n,m)} = & \frac{\eta}{2\sqrt{\pi}} \sum_{k=1}^{\infty} \sqrt{2k+1} P_k^1(\cos \theta) \left\{ \frac{T_{k0}^{(n,m)}(r)}{r} + \frac{2\Phi_{k0}^{(n,m)'}(r)}{r} - \frac{2\Phi_{k0}^{(n,m)}(r)}{r^2} \right. \\ & + \frac{A_{k0}^{nmnm}}{4\omega r} \operatorname{Re} \left\{ i f_{nm}^* (r) [g_{nm}(r) - r g_{nm}'(r)] \right. \\ & \left. \left. + i f_{nm}^* (r) \left[ \frac{2n(n+1) - k(k+1) - 2}{r} g_{nm}(r) + 2g_{nm}'(r) - r g_{nm}''(r) - 2f_{nm}'(r) \right] \right\} \right\}. \end{aligned} \tag{B69}$$

Substitution of (B69) into (B65) yields

$$T_{k0}^{(n,m)}(R_0) + 2\Phi_{k0}^{(n,m)'}(R_0) - \frac{2}{R_0} \Phi_{k0}^{(n,m)}(R_0) = S_k^{(n,m)}, \tag{B70}$$

where

$$S_k^{(n,m)} = \frac{A_{k0}^{nmnm}}{4\omega} \operatorname{Re} \left\{ i f_{nm}^{*/} (R_0) \left[ R_0 g_{nm}' (R_0) - g_{nm} (R_0) \right] + i f_{nm}^* (R_0) \right. \\ \left. \times \left[ \frac{2+k(k+1)-2n(n+1)}{R_0} g_{nm} (R_0) - 2g_{nm}' (R_0) + R_0 g_{nm}'' (R_0) + 2f_{nm}' (R_0) \right] \right\}. \tag{B71}$$

Combining (B67) and (B70), and using (B24), (B33), (B39) and (B45), one finds

$$\overline{C}_{4k}^{(n,m)} = \frac{(2k-1)R_0^k}{(k+1)(2k+1)} \left[ 2(k+2)Q_k^{(n,m)} - (k+1)S_k^{(n,m)} - (k+3)R_0^{k+1}\overline{C}_{3k}^{(n,m)} \right. \\ \left. - 2(2k+1)R_0^{k-1}I_k^{(n,m)} \right], \tag{B72}$$

$$\overline{C}_{6k}^{(n,m)} = \frac{R_0^2}{k+1} \left[ \frac{(k+1)(3k-1)}{4k^2-1}\overline{C}_{4k}^{(n,m)} + R_0^{2k+1}\overline{C}_{3k}^{(n,m)} + kR_0^{2k-1}I_k^{(n,m)} - R_0^k Q_k^{(n,m)} \right]. \tag{B73}$$

To calculate  $\sigma_{Lr\phi}^{(n,m)}$ , we use (B44) and (B62):

$$\sigma_{Lr\phi}^{(n,m)} = \frac{\eta}{r^2} \sum_{k=1}^{\infty} P_k^1 (\cos \theta) \left\{ \frac{\sqrt{2k+1}}{2\sqrt{\pi}} \left[ 2P_{k0}^{(n,m)} (r) - rP_{k0}^{(n,m)'} (r) \right] \right. \\ \left. - rE_k^{(n,m)} (r) + r^2 E_k^{(n,m)'} (r) \right\}, \tag{B74}$$

where  $P_{k0}^{(n,m)'} (r)$  and  $E_k^{(n,m)'} (r)$  are calculated by

$$P_{k0}^{(n,m)'} (r) = (k+1)r^k C_{1k}^{(n,m)} (r) - kr^{-k-1} C_{2k}^{(n,m)} (r), \tag{B75}$$

$$E_k^{(n,m)'} (r) = \begin{cases} E^{(1,1)'} (r) \delta_{1k}, & n = 1, \\ E_k^{(n>1,m)'} (r), & n > 1, \end{cases} \tag{B76}$$

$$E^{(1,1)'} (r) = \frac{3}{16\pi\omega r^2} \operatorname{Re} \left\{ f_{11}^* (r) \left[ r g_{11}' (r) - r^2 g_{11}'' (r) - g_{11} (r) \right] \right. \\ \left. + r f_{11}^{*/} (r) \left[ g_{11} (r) - r g_{11}' (r) \right] + g_{11}^* (r) \left[ g_{11} (r) - 2r g_{11}' (r) \right] \right\}, \tag{B77}$$

$$E_k^{(n>1,m)'} (r) = -\frac{E_k^{(n>1,m)} (r)}{r} \\ + \frac{m\sqrt{2k+1}}{4\sqrt{\pi}\omega r} \left\{ 2 \operatorname{Re} \{ g_{nm}' (r) g_{nm}^* (r) \} \left[ n C_{(n+1)m} B_{k0}^{(n+1)mnm} - (n+1) C_{nm} B_{k0}^{(n+1)mnm} \right] \right. \\ - \sqrt{\frac{(2n+1)(n-m)!}{(n+m)!}} \operatorname{Re} \left\{ f_{nm}^{*/} (r) \left[ g_{nm} (r) - r g_{nm}' (r) \right] - r f_{nm}^* (r) g_{nm}'' (r) \right. \\ \left. - 2n(n+1) g_{nm}' (r) g_{nm}^* (r) \right\} \\ \left. \times \frac{1}{\sqrt{k(k+1)}} \sum_{s=1}^{\left[ \frac{(n-m+2)}{2} \right]} \sqrt{\frac{(2n-4s+3)(n+m-2s)!}{(n-m-2s+2)!}} A_{k(-1)}^{(n-2s+1)(m-1)nm} \right\}. \tag{B78}$$

Substituting (B74) into (B66), and using (B18) and (B75), one finds

$$\overline{C}_{2k}^{(n,m)} = \frac{R_0^{k+1}}{k+2} \left\{ (k-1) R_0^k \overline{C}_{1k}^{(n,m)} + \frac{2\sqrt{\pi}}{\sqrt{2k+1}} \left[ E_k^{(n,m)}(R_0) - R_0 E_k^{(n,m)'}(R_0) \right] \right\}. \tag{B79}$$

**Appendix C. Solving the equations of acoustic streaming for the cross terms**

To solve (2.64) and (2.65), we first need to calculate their right-hand sides.

The calculation of  $\mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,-m)}$  yields

$$\begin{aligned} & \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,-m)} \\ &= \left( v_{1r}^{(n,m)} \frac{\partial}{\partial r} + \frac{v_{1\theta}^{(n,m)}}{r} \frac{\partial}{\partial \theta} + \frac{v_{1\phi}^{(n,m)}}{r \sin \theta} \frac{\partial}{\partial \phi} \right) \left( v_{1r}^{(n,-m)} \mathbf{e}_r + v_{1\theta}^{(n,-m)} \mathbf{e}_\theta + v_{1\phi}^{(n,-m)} \mathbf{e}_\phi \right) \\ &= \mathbf{e}_r \left( v_{1r}^{(n,m)} \frac{\partial v_{1r}^{(n,-m)}}{\partial r} + \frac{v_{1\theta}^{(n,m)}}{r} \frac{\partial v_{1r}^{(n,-m)}}{\partial \theta} + \frac{v_{1\phi}^{(n,m)}}{r \sin \theta} \frac{\partial v_{1r}^{(n,-m)}}{\partial \phi} \right. \\ &\quad \left. - \frac{v_{1\theta}^{(n,m)} v_{1\theta}^{(n,-m)} + v_{1\phi}^{(n,m)} v_{1\phi}^{(n,-m)}}{r} \right) \\ &+ \mathbf{e}_\theta \left( v_{1r}^{(n,m)} \frac{\partial v_{1\theta}^{(n,-m)}}{\partial r} + \frac{v_{1\theta}^{(n,m)}}{r} \frac{\partial v_{1\theta}^{(n,-m)}}{\partial \theta} + \frac{v_{1\phi}^{(n,m)}}{r \sin \theta} \frac{\partial v_{1\theta}^{(n,-m)}}{\partial \phi} + \frac{v_{1\theta}^{(n,m)} v_{1r}^{(n,-m)}}{r} \right. \\ &\quad \left. - \frac{\cos \theta v_{1\phi}^{(n,m)} v_{1\phi}^{(n,-m)}}{r \sin \theta} \right) \\ &+ \mathbf{e}_\phi \left( v_{1r}^{(n,m)} \frac{\partial v_{1\phi}^{(n,-m)}}{\partial r} + \frac{v_{1\theta}^{(n,m)}}{r} \frac{\partial v_{1\phi}^{(n,-m)}}{\partial \theta} + \frac{v_{1\phi}^{(n,m)}}{r \sin \theta} \frac{\partial v_{1\phi}^{(n,-m)}}{\partial \phi} + \frac{v_{1\phi}^{(n,m)} v_{1r}^{(n,-m)}}{r} \right. \\ &\quad \left. + \frac{\cos \theta v_{1\phi}^{(n,m)} v_{1\theta}^{(n,-m)}}{r \sin \theta} \right). \tag{C1} \end{aligned}$$

Substituting (2.30)–(2.32) and (2.41)–(2.43) into (C1), and averaging over time, one obtains

$$\begin{aligned} & \left\langle \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,-m)} \right\rangle \\ &= \frac{(-1)^m}{2} \operatorname{Re} \left\{ \mathbf{e}_r \varepsilon \left\{ V_n V_n'^* (Y_n^m)^2 + \frac{W_n (V_n^* - W_n^*)}{r} \left[ \left( \frac{\partial Y_n^m}{\partial \theta} \right)^2 + \frac{1}{\sin^2 \theta} \left( \frac{\partial Y_n^m}{\partial \phi} \right)^2 \right] \right\} \right. \\ &+ \mathbf{e}_\theta \varepsilon \left\{ \left( V_n W_n'^* + \frac{W_n V_n^*}{r} \right) Y_n^m \frac{\partial Y_n^m}{\partial \theta} \right. \\ &+ \frac{|W_n|^2}{r} \left[ \frac{\partial Y_n^m}{\partial \theta} \frac{\partial^2 Y_n^m}{\partial \theta^2} + \frac{1}{\sin^2 \theta} \frac{\partial Y_n^m}{\partial \phi} \frac{\partial^2 Y_n^m}{\partial \theta \partial \phi} - \frac{\cos \theta}{\sin^3 \theta} \left( \frac{\partial Y_n^m}{\partial \phi} \right)^2 \right] \left. \right\} \\ &+ \frac{\mathbf{e}_\phi \varepsilon}{\sin \theta} \left\{ \left( V_n W_n'^* + \frac{W_n V_n^*}{r} \right) Y_n^m \frac{\partial Y_n^m}{\partial \phi} + \frac{|W_n|^2}{r} \left( \frac{\partial Y_n^m}{\partial \theta} \frac{\partial^2 Y_n^m}{\partial \theta \partial \phi} + \frac{1}{\sin^2 \theta} \frac{\partial Y_n^m}{\partial \phi} \frac{\partial^2 Y_n^m}{\partial \phi^2} \right) \right\} \left. \right\}, \tag{C2} \end{aligned}$$

where  $\varepsilon = s^{(n,m)} s^{(n,-m)*}$ . For simplicity, we drop the arguments of the functions in (C2).

The calculation of the curl of (C2) results in

$$\begin{aligned} \nabla \times \langle \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,-m)} \rangle &= \frac{(-1)^m}{2} \operatorname{Re} \left\{ \frac{\mathbf{e}_\theta \varepsilon}{r \sin \theta} \left\{ \left[ 2V_n V_n'^* - (rV_n W_n'^* + W_n V_n^*)' \right] Y_n^m \frac{\partial Y_n^m}{\partial \phi} \right. \right. \\ &+ \left. \left[ \frac{2W_n (V_n^* - W_n^*)}{r} - (W_n W_n^*)' \right] \left( \frac{\partial Y_n^m}{\partial \theta} \frac{\partial^2 Y_n^m}{\partial \theta \partial \phi} + \frac{1}{\sin^2 \theta} \frac{\partial Y_n^m}{\partial \phi} \frac{\partial^2 Y_n^m}{\partial \phi^2} \right) \right\} \\ &+ \frac{\mathbf{e}_\phi \varepsilon}{r} \left\{ \left[ (rV_n W_n'^* + W_n V_n^*)' - 2V_n V_n'^* \right] Y_n^m \frac{\partial Y_n^m}{\partial \theta} + \left[ (W_n W_n^*)' - \frac{2W_n (V_n^* - W_n^*)}{r} \right] \right. \\ &\times \left. \left[ \frac{\partial Y_n^m}{\partial \theta} \frac{\partial^2 Y_n^m}{\partial \theta^2} + \frac{1}{\sin^2 \theta} \frac{\partial Y_n^m}{\partial \phi} \frac{\partial^2 Y_n^m}{\partial \theta \partial \phi} - \frac{\cos \theta}{\sin^3 \theta} \left( \frac{\partial Y_n^m}{\partial \phi} \right)^2 \right] \right\}. \end{aligned} \quad (\text{C3})$$

Since (C3) does not contain a radial component, (2.64) leads to

$$P_{kl}^{(\times)''} (r) - \frac{k(k+1) P_{kl}^{(\times)} (r)}{r^2} = 0. \quad (\text{C4})$$

A solution to (C4) is given by

$$P_{kl}^{(\times)} (r) = \bar{C}_{1k}^{(\times)} r^{k+1} + \bar{C}_{2k}^{(\times)} r^{-k}, \quad (\text{C5})$$

where  $\bar{C}_{1k}^{(\times)}$  and  $\bar{C}_{2k}^{(\times)}$  are constants. From the condition that the acoustic streaming vanishes at infinity, it follows that

$$\bar{C}_{1k}^{(\times)} = 0, \quad (\text{C6})$$

while  $\bar{C}_{2k}^{(\times)}$  is calculated by boundary conditions at the bubble surface; see below.

The calculation of the  $r$ -component of  $\nabla \times \nabla \times \langle \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,-m)} \rangle$  results in

$$\begin{aligned} \mathbf{e}_r \cdot \left[ \nabla \times \nabla \times \langle \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,-m)} \rangle \right] &= \frac{(-1)^m}{4r^2} \operatorname{Re} \left\{ \varepsilon \left[ 2V_n V_n'^* - (rV_n W_n'^* + W_n V_n^*)' \right] L^2 \left[ (Y_n^m)^2 \right] \right. \\ &+ \left. \varepsilon \left[ \frac{2W_n (V_n^* - W_n^*)}{r} - (W_n W_n^*)' \right] L^2 \left[ \left( \frac{\partial Y_n^m}{\partial \theta} \right)^2 + \frac{1}{\sin^2 \theta} \left( \frac{\partial Y_n^m}{\partial \phi} \right)^2 \right] \right\}, \end{aligned} \quad (\text{C7})$$

where the operator  $L^2$  is given by (B9).

The  $r$ -component of  $\nabla \times \nabla \times \langle \mathbf{v}_1^{(n,-m)} \cdot \nabla \mathbf{v}_1^{(n,m)} \rangle$  is calculated from (C7) by swapping  $m$  with  $-m$ . Doing so and using (D3), one obtains

$$\begin{aligned} \mathbf{e}_r \cdot \left[ \nabla \times \nabla \times \langle \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,-m)} + \mathbf{v}_1^{(n,-m)} \cdot \nabla \mathbf{v}_1^{(n,m)} \rangle \right] &= \frac{(-1)^m}{4r^2} \\ &\times \operatorname{Re} \left\{ \varepsilon \left[ 2V_n V_n'^* + 2V_n^* V_n' - (rV_n W_n'^* + W_n V_n^*)' - (rV_n^* W_n' + W_n^* V_n)' \right] L^2 \left[ (Y_n^m)^2 \right] \right. \\ &+ \left. 2\varepsilon \left[ \frac{V_n W_n^* + V_n^* W_n - 2W_n W_n^*}{r} - (W_n W_n^*)' \right] L^2 \left[ \left( \frac{\partial Y_n^m}{\partial \theta} \right)^2 - \frac{m^2 (Y_n^m)^2}{\sin^2 \theta} \right] \right\}. \end{aligned} \quad (\text{C8})$$

By using (D5), it can be shown that the following identity holds:

$$\left(\frac{\partial Y_n^m}{\partial \theta}\right)^2 - \frac{m^2 (Y_n^m)^2}{\sin^2 \theta} = n(n+1) (Y_n^m)^2 - \frac{1}{2} L^2 [(Y_n^m)^2]. \quad (C9)$$

Substitution of (C9) into (C8) yields

$$\begin{aligned} e_r \cdot \left[ \nabla \times \nabla \times \left\{ \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,-m)} + \mathbf{v}_1^{(n,-m)} \cdot \nabla \mathbf{v}_1^{(n,m)} \right\} \right] &= \frac{(-1)^m}{4r^2} \\ &\times \text{Re} \left\{ \varepsilon L^2 [(Y_n^m)^2] \left\{ 2V_n V_n'^* + 2V_n^* V_n' - (r V_n W_n'^* + V_n^* W_n + r V_n^* W_n' + V_n W_n^*)' \right. \right. \\ &+ 2n(n+1) \left. \left[ \frac{V_n W_n^* + V_n^* W_n - 2W_n W_n^*}{r} - (W_n W_n^*)' \right] \right\} \\ &+ \varepsilon L^4 [(Y_n^m)^2] \left[ (W_n W_n^*)' - \frac{V_n W_n^* + V_n^* W_n - 2W_n W_n^*}{r} \right] \right\}. \quad (C10) \end{aligned}$$

Substituting (C10) into (2.65), expressing  $(Y_n^m)^2$  by (D25), and using the identity  $L^2 Y_k^l = k(k+1)Y_k^l$ , one obtains

$$T_{kl}^{(\times) //} (r) - \frac{k(k+1)}{r^2} T_{kl}^{(\times)} (r) = D_{kl}^{nmnm} G_k^{(\times)} (r), \quad (C11)$$

where the constant coefficients  $D_{kl}^{nmnm}$  are calculated by (D27), and  $G_k^{(\times)}(r)$  is given by

$$\begin{aligned} G_k^{(\times)} (r) &= \frac{(-1)^m \varepsilon}{2\nu} \text{Re} \left\{ V_n^* (r) \left[ 2V_n' (r) - 2W_n' (r) - r W_n'' (r) \right] - V_n'^* (r) \left[ W_n (r) + r W_n' (r) \right] \right. \\ &+ \left. \frac{2n(n+1) - k(k+1)}{r} W_n^* (r) \left[ V_n (r) - W_n (r) - r W_n' (r) \right] \right\}. \quad (C12) \end{aligned}$$

A solution to (C11) is given by

$$T_{kl}^{(\times)} (r) = D_{kl}^{nmnm} \left[ r^{k+1} C_{3k}^{(\times)} (r) + r^{-k} C_{4k}^{(\times)} (r) \right], \quad (C13)$$

$$C_{3k}^{(\times)} (r) = \bar{C}_{3k}^{(\times)} + \frac{1}{2k+1} \int_{R_0}^r s^{-k} G_k^{(\times)} (s) ds, \quad (C14)$$

$$C_{4k}^{(\times)} (r) = \bar{C}_{4k}^{(\times)} - \frac{1}{2k+1} \int_{R_0}^r s^{k+1} G_k^{(\times)} (s) ds. \quad (C15)$$

The constant  $\bar{C}_{3k}^{(\times)}$  is calculated from the condition that the acoustic streaming vanishes at infinity,

$$\bar{C}_{3k}^{(\times)} = -\frac{1}{2k+1} \int_{R_0}^{\infty} s^{-k} G_k^{(\times)} (s) ds, \quad (C16)$$

and the constant  $\bar{C}_{4k}^{(\times)}$  is calculated by boundary conditions at the bubble surface; see below.

From (2.63), it follows that

$$\mathbf{v}_E^{(\times)} = \text{Re} \left\{ \nabla \times \left[ \mathbf{e}_r \sum_{k=1}^{\infty} \sum_{l=-k}^k P_{kl}^{(\times)}(r) Y_k^l(\theta, \phi) \right] + \mathbf{e}_r \sum_{k=1}^{\infty} \sum_{l=-k}^k T_{kl}^{(\times)}(r) Y_k^l(\theta, \phi) + \nabla \Phi^{(\times)}(r, \theta, \phi) \right\}. \quad (\text{C17})$$

Substitution of (C17) into (2.44) yields

$$\begin{aligned} \Delta \Phi^{(\times)}(r, \theta, \phi) &= - \sum_{k=1}^{\infty} \sum_{l=-k}^k \nabla \cdot \left[ T_{kl}^{(\times)}(r) Y_k^l(\theta, \phi) \mathbf{e}_r \right] \\ &= - \sum_{k=1}^{\infty} \sum_{l=-k}^k \left[ T_{kl}^{(\times)'}(r) + 2r^{-1} T_{kl}^{(\times)}(r) \right] Y_k^l(\theta, \phi). \end{aligned} \quad (\text{C18})$$

$$\Phi^{(\times)}(r, \theta, \phi) = \sum_{k=1}^{\infty} \sum_{l=-k}^k \Phi_{kl}^{(\times)}(r) Y_k^l(\theta, \phi). \quad (\text{C19})$$

Substituting (C19) into (C18), and using (C13), one obtains

$$\Phi_{kl}^{(\times)'}(r) + \frac{2}{r} \Phi_{kl}^{(\times)}(r) - \frac{k(k+1)}{r^2} \Phi_{kl}^{(\times)}(r) = D_{kl}^{nmnm} H_k^{(\times)}(r), \quad (\text{C20})$$

$$H_k^{(\times)}(r) = -(k+3)r^k C_{3k}^{(\times)}(r) + (k-2)r^{-k-1} C_{4k}^{(\times)}(r). \quad (\text{C21})$$

Equation (C20) is solved by the method of variation of parameters, which results in

$$\Phi_{kl}^{(\times)}(r) = D_{kl}^{nmnm} \left[ r^k C_{5k}^{(\times)}(r) + r^{-k-1} C_{6k}^{(\times)}(r) \right], \quad (\text{C22})$$

where  $C_{5k}^{(\times)}(r)$  and  $C_{6k}^{(\times)}(r)$  obey the equations

$$r^k C_{5k}^{(\times)'}(r) + r^{-k-1} C_{6k}^{(\times)'}(r) = 0, \quad (\text{C23})$$

$$kr^{k-1} C_{5k}^{(\times)'}(r) - (k+1)r^{-k-2} C_{6k}^{(\times)'}(r) = H_k^{(\times)}(r). \quad (\text{C24})$$

Solutions to (C23) and (C24) are given by

$$C_{5k}^{(\times)}(r) = \bar{C}_{5k}^{(\times)} + \frac{1}{2k+1} \int_{R_0}^r s^{1-k} H_k^{(\times)}(s) ds, \quad (\text{C25})$$

$$C_{6k}^{(\times)}(r) = \bar{C}_{6k}^{(\times)} - \frac{1}{2k+1} \int_{R_0}^r s^{k+2} H_k^{(\times)}(s) ds, \quad (\text{C26})$$

where  $\bar{C}_{5k}^{(\times)}$  and  $\bar{C}_{6k}^{(\times)}$  are constants. The constant  $\bar{C}_{6k}^{(\times)}$  is calculated by boundary conditions at the bubble surface; see below. The constant  $\bar{C}_{5k}^{(\times)}$  is calculated from the condition that the acoustic streaming vanishes at infinity, which gives

$$\bar{C}_{5k}^{(\times)} = - \frac{1}{2k+1} \int_{R_0}^{\infty} s^{1-k} H_k^{(\times)}(s) ds. \quad (\text{C27})$$

Substituting (C21) into (C27), and using (C15), one obtains

$$\overline{C}_{5k}^{(\times)} = -\frac{(k-2)\overline{C}_{4k}^{(\times)}}{(4k^2-1)R_0^{2k-1}} + I_k^{(\times)}, \tag{C28}$$

$$I_k^{(\times)} = \frac{k+3}{2k+1} \int_{R_0}^{\infty} r C_{3k}^{(\times)}(r) dr + \frac{k-2}{(2k+1)^2} \int_{R_0}^{\infty} r^{-2k} \left[ \int_{R_0}^r s^{k+1} G_k^{(\times)}(s) ds \right] dr. \tag{C29}$$

Substitution of (C19) into (C17) yields

$$v_{Er}^{(\times)} = \text{Re} \sum_{k=1}^{\infty} \sum_{l=-k}^k \left[ T_{kl}^{(\times)}(r) + \Phi_{kl}^{(\times)'}(r) \right] Y_k^l(\theta, \phi), \tag{C30}$$

$$v_{E\theta}^{(\times)} = \text{Re} \sum_{k=1}^{\infty} \sum_{l=-k}^k \left[ \frac{\Phi_{kl}^{(\times)}(r)}{r} \frac{\partial Y_k^l(\theta, \phi)}{\partial \theta} + \frac{P_{kl}^{(\times)}(r)}{r \sin \theta} \frac{\partial Y_k^l(\theta, \phi)}{\partial \phi} \right], \tag{C31}$$

$$v_{E\phi}^{(\times)} = \text{Re} \sum_{k=1}^{\infty} \sum_{l=-k}^k \left[ \frac{\Phi_{kl}^{(\times)}(r)}{r \sin \theta} \frac{\partial Y_k^l(\theta, \phi)}{\partial \phi} - \frac{P_{kl}^{(\times)}(r)}{r} \frac{\partial Y_k^l(\theta, \phi)}{\partial \theta} \right]. \tag{C32}$$

The function  $\Phi_{kl}^{(\times)'}(r)$ , which appears in (C30), is calculated by (C22) and (C23) to be

$$\Phi_{kl}^{(\times)'}(r) = D_{kl}^{nmnm} \left[ kr^{k-1} C_{5k}^{(\times)}(r) - (k+1)r^{-k-2} C_{6k}^{(\times)}(r) \right]. \tag{C33}$$

In order to go on with the calculation, we need to apply the boundary conditions for the acoustic streaming at the bubble surface. To do this, we need to know the Stokes drift velocity, which is calculated by

$$\mathbf{v}_S^{(\times)} = \frac{1}{2\omega} \text{Re} \left\{ i \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,-m)*} + i \mathbf{v}_1^{(n,-m)} \cdot \nabla \mathbf{v}_1^{(n,m)*} \right\}. \tag{C34}$$

The expression  $\text{Re}\{i \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,-m)*}\}$  is calculated by

$$\begin{aligned} & \text{Re} \left\{ i \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,-m)*} \right\} \\ &= \text{Re} \left\{ \mathbf{e}_r i \left( v_{1r}^{(n,m)} \frac{\partial v_{1r}^{(n,-m)*}}{\partial r} + \frac{v_{1\theta}^{(n,m)}}{r} \frac{\partial v_{1r}^{(n,-m)*}}{\partial \theta} + \frac{v_{1\phi}^{(n,m)}}{r \sin \theta} \frac{\partial v_{1r}^{(n,-m)*}}{\partial \phi} - \frac{v_{1\theta}^{(n,m)} v_{1\theta}^{(n,-m)*}}{r} \right. \right. \\ & \quad \left. \left. - \frac{v_{1\phi}^{(n,m)} v_{1\phi}^{(n,-m)*}}{r} \right) \right. \\ & \quad \left. + \mathbf{e}_\theta i \left( v_{1r}^{(n,m)} \frac{\partial v_{1\theta}^{(n,-m)*}}{\partial r} + \frac{v_{1\theta}^{(n,m)}}{r} \frac{\partial v_{1\theta}^{(n,-m)*}}{\partial \theta} + \frac{v_{1\phi}^{(n,m)}}{r \sin \theta} \frac{\partial v_{1\theta}^{(n,-m)*}}{\partial \phi} + \frac{v_{1\theta}^{(n,m)} v_{1r}^{(n,-m)*}}{r} \right. \right. \\ & \quad \left. \left. - \frac{\cos \theta v_{1\phi}^{(n,m)} v_{1\phi}^{(n,-m)*}}{r \sin \theta} \right) \right\} \end{aligned}$$

$$\begin{aligned}
 & + \mathbf{e}_\phi i \left( v_{1r}^{(n,m)} \frac{\partial v_{1\phi}^{(n,-m)*}}{\partial r} + \frac{v_{1\theta}^{(n,m)}}{r} \frac{\partial v_{1\phi}^{(n,-m)*}}{\partial \theta} + \frac{v_{1\phi}^{(n,m)}}{r \sin \theta} \frac{\partial v_{1\phi}^{(n,-m)*}}{\partial \phi} + \frac{v_{1\phi}^{(n,m)} v_{1r}^{(n,-m)*}}{r} \right. \\
 & \left. + \frac{\cos \theta v_{1\phi}^{(n,m)} v_{1\theta}^{(n,-m)*}}{r \sin \theta} \right) \Bigg\}. \tag{C35}
 \end{aligned}$$

Substituting (2.30)–(2.32) and (2.41)–(2.43) into (C35), and using (C9), one obtains

$$\begin{aligned}
 \text{Re} \left\{ i \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,-m)*} \right\} &= (-1)^m \\
 & \times \text{Re} \left\{ \mathbf{e}_r i \varepsilon \left\{ \left[ V_n V_n'^* + \frac{n(n+1) W_n (V_n^* - W_n^*)}{r} \right] (Y_n^m)^2 - \frac{W_n (V_n^* - W_n^*)}{2r} L^2 [(Y_n^m)^2] \right\} \right. \\
 & + \mathbf{e}_\theta \frac{i \varepsilon}{2} \frac{\partial}{\partial \theta} \left\{ \left[ V_n W_n'^* + \frac{W_n (V_n^* + n(n+1) W_n^*)}{r} \right] (Y_n^m)^2 - \frac{W_n W_n^*}{2r} L^2 [(Y_n^m)^2] \right\} \\
 & \left. + \mathbf{e}_\phi \frac{i \varepsilon}{2 \sin \theta} \frac{\partial}{\partial \phi} \left\{ \left[ V_n W_n'^* + \frac{W_n (V_n^* + n(n+1) W_n^*)}{r} \right] (Y_n^m)^2 - \frac{W_n W_n^*}{2r} L^2 [(Y_n^m)^2] \right\} \right\}. \tag{C36}
 \end{aligned}$$

The expression  $\text{Re}\{i \mathbf{v}_1^{(n,m)} \cdot \nabla \mathbf{v}_1^{(n,-m)*}\}$  is calculated from (C36) by swapping  $m$  with  $-m$ . Doing so, and using (D3), one obtains

$$\begin{aligned}
 v_{Sr}^{(\times)} &= \frac{(-1)^m}{2\omega} \text{Re} \left\{ i \varepsilon \left\{ \left[ V_n V_n'^* - V_n^* V_n' - \frac{n(n+1)(V_n W_n^* - V_n^* W_n)}{r} \right] (Y_n^m)^2 \right. \right. \\
 & \left. \left. + \frac{V_n W_n^* - V_n^* W_n}{2r} L^2 [(Y_n^m)^2] \right\} \right\} \tag{C37}
 \end{aligned}$$

$$v_{S\theta}^{(\times)} = \frac{(-1)^m}{4\omega} \text{Re} \left\{ i \varepsilon \left[ V_n W_n'^* - V_n^* W_n' - \frac{V_n W_n^* - V_n^* W_n}{r} \right] \frac{\partial (Y_n^m)^2}{\partial \theta} \right\}, \tag{C38}$$

$$v_{S\phi}^{(\times)} = \frac{(-1)^m}{4\omega} \text{Re} \left\{ i \varepsilon \left[ V_n W_n'^* - V_n^* W_n' - \frac{V_n W_n^* - V_n^* W_n}{r} \right] \frac{1}{\sin \theta} \frac{\partial (Y_n^m)^2}{\partial \phi} \right\}. \tag{C39}$$

With the help of (D25) and the identity  $L^2 Y_k^l = k(k+1) Y_k^l$ , (C37)–(C39) are transformed to

$$v_{Sr}^{(\times)} = \text{Re} \sum_{k=1}^{\infty} S_k^{(\times)}(r) \sum_{l=-k}^k D_{kl}^{nmnm} Y_k^l(\theta, \phi), \tag{C40}$$

$$v_{S\theta}^{(\times)} = \text{Re} \left\{ U_{nm}(r) \sum_{k=1}^{\infty} \sum_{l=-k}^k D_{kl}^{nmnm} \frac{\partial Y_k^l(\theta, \phi)}{\partial \theta} \right\}, \tag{C41}$$

$$v_{S\phi}^{(\times)} = \text{Re} \left\{ i U_{nm}(r) \sum_{k=1}^{\infty} \sum_{l=-k}^k l D_{kl}^{nmnm} \frac{Y_k^l(\theta, \phi)}{\sin \theta} \right\}, \quad (\text{C42})$$

$$S_k^{(\times)}(r) = \frac{(-1)^m \varepsilon}{\omega} \text{Im} \left\{ V_n^*(r) \left[ V_n'(r) - \frac{n(n+1)}{r} W_n(r) \right] + \frac{k(k+1)}{2r} V_n^*(r) W_n(r) \right\}, \quad (\text{C43})$$

$$U_{nm}(r) = \frac{(-1)^m \varepsilon}{2\omega} \text{Im} \left\{ V_n^*(r) \left[ W_n'(r) - \frac{W_n(r)}{r} \right] \right\}. \quad (\text{C44})$$

Equations (C41) and (C42) are convenient to use in the boundary conditions at the bubble surface. However, for the numerical calculation of  $v_{S\theta}^{(\times)}$  and  $v_{S\phi}^{(\times)}$ , it is convenient to transform (C41) and (C42).

With the help of (D9), (C41) is transformed to

$$v_{S\theta}^{(\times)} = \frac{1}{2} \text{Re} \left\{ U_{nm}(r) \times \sum_{k=1}^{\infty} \sum_{l=-k}^k D_{kl}^{nmnm} \left[ \sqrt{k(k+1) - l(l+1)} Y_k^{l+1}(\theta, \phi) e^{-i\phi} - \sqrt{k(k+1) - l(l-1)} Y_k^{l-1}(\theta, \phi) e^{i\phi} \right] \right\}. \quad (\text{C45})$$

With the help of (D16), (C42) is transformed to

$$v_{S\phi}^{(\times)} = -\text{Re} \left\{ i U_{nm}(r) e^{i\phi} \sum_{k=1}^{\infty} \sum_{l=-k}^k l \sqrt{\frac{(2k+1)(k-l)!}{(k+l)!}} D_{kl}^{nmnm} \times \sum_{s=1}^{[(k-l+2)/2]} \sqrt{\frac{(2k-4s+3)(k+l-2s)!}{(k-l-2s+2)!}} Y_{k-2s+1}^{l-1}(\theta, \phi) \right\}. \quad (\text{C46})$$

We can now apply the boundary conditions for the acoustic streaming at the bubble surface.

They are given by

$$v_{Lr}^{(\times)} = 0 \quad \text{at } r = R_0, \quad (\text{C47})$$

$$\sigma_{Lr\theta}^{(\times)} = \eta \left( \frac{1}{r} \frac{\partial v_{Lr}^{(\times)}}{\partial \theta} + \frac{\partial v_{L\theta}^{(\times)}}{\partial r} - \frac{v_{L\theta}^{(\times)}}{r} \right) = 0 \quad \text{at } r = R_0, \quad (\text{C48})$$

$$\sigma_{Lr\phi}^{(\times)} = \eta \left( \frac{\partial v_{L\phi}^{(\times)}}{\partial r} + \frac{1}{r \sin \theta} \frac{\partial v_{Lr}^{(\times)}}{\partial \phi} - \frac{v_{L\phi}^{(\times)}}{r} \right) = 0 \quad \text{at } r = R_0, \quad (\text{C49})$$

where  $\mathbf{v}_L^{(\times)} = \mathbf{v}_E^{(\times)} + \mathbf{v}_S^{(\times)}$  is the Lagrangian streaming velocity, and  $\sigma_{Lr\theta}^{(\times)}$  and  $\sigma_{Lr\phi}^{(\times)}$  are the tangential components of the stress produced by  $\mathbf{v}_L^{(\times)}$ . We use (C47)–(C49) in order to calculate the constants  $\overline{C}_{2k}^{(\times)}$ ,  $\overline{C}_{4k}^{(\times)}$  and  $\overline{C}_{6k}^{(\times)}$ .

Substituting (C30) and (C40) into (C47), and using (C13), (C28) and (C33), one obtains

$$\frac{(k+1)(3k-1)}{4k^2-1} \overline{C}_{4k}^{(\times)} - (k+1) R_0^{-2} \overline{C}_{6k}^{(\times)} = -R_0^{2k+1} \overline{C}_{3k}^{(\times)} - k R_0^{2k-1} I_k^{(\times)} - R_0^k S_k^{(\times)}(R_0). \quad (\text{C50})$$

The calculation of  $\sigma_{Lr\theta}^{(\times)}$  and  $\sigma_{Lr\phi}^{(\times)}$  results in

$$\sigma_{Lr\theta}^{(\times)} = \eta \operatorname{Re} \sum_{k=1}^{\infty} \sum_{l=-k}^k \left\{ D_{kl}^{nmnm} \left[ r^k C_{3k}^{(\times)}(r) + r^{-k-1} C_{4k}^{(\times)}(r) + 2(k-1)r^{k-2} C_{5k}^{(\times)}(r) - 2(k+2)r^{-k-3} C_{6k}^{(\times)}(r) + \frac{S_k^{(\times)}(r) - U_{nm}(r) + rU'_{nm}(r)}{r} \right] \frac{\partial Y_k^l(\theta, \phi)}{\partial \theta} - il(k+2) \overline{C}_{2k}^{(\times)} r^{-k-2} \frac{Y_k^l(\theta, \phi)}{\sin \theta} \right\}, \quad (C51)$$

$$\sigma_{Lr\phi}^{(\times)} = \eta \operatorname{Re} \sum_{k=1}^{\infty} \sum_{l=-k}^k \left\{ D_{kl}^{nmnm} \left[ r^k C_{3k}^{(\times)}(r) + r^{-k-1} C_{4k}^{(\times)}(r) + 2(k-1)r^{k-2} C_{5k}^{(\times)}(r) - 2(k+2)r^{-k-3} C_{6k}^{(\times)}(r) + \frac{S_k^{(\times)}(r) - U_{nm}(r) + rU'_{nm}(r)}{r} \right] \frac{i l Y_k^l}{\sin \theta} + (k+2) \overline{C}_{2k}^{(\times)} r^{-k-2} \frac{\partial Y_k^l}{\partial \theta} \right\}. \quad (C52)$$

Equations (C51) and (C52) show that (C48) and (C49) are satisfied if  $\overline{C}_{2k}^{(\times)} = 0$ . In this case, (C48) and (C49) give

$$\frac{2k^2 + 6k - 5}{4k^2 - 1} \overline{C}_{4k}^{(\times)} - 2(k+2)R_0^{-2} \overline{C}_{6k}^{(\times)} = -R_0^{2k+1} \overline{C}_{3k}^{(\times)} - 2(k-1)R_0^{2k-1} I_k^{(\times)} - R_0^k \left[ S_k^{(\times)}(R_0) - U_{nm}(R_0) + R_0 U'_{nm}(R_0) \right]. \quad (C53)$$

Combining (C50) and (C53), one obtains

$$\overline{C}_{4k}^{(\times)} = -\frac{(k+3)(2k-1)}{(k+1)(2k+1)} R_0^{2k+1} \overline{C}_{3k}^{(\times)} - \frac{2(2k-1)}{k+1} R_0^{2k-1} I_k^{(\times)} - \frac{2k-1}{2k+1} R_0^k \left[ \frac{k+3}{k+1} S_k^{(\times)}(R_0) + U_{nm}(R_0) - R_0 U'_{nm}(R_0) \right], \quad (C54)$$

$$\overline{C}_{6k}^{(\times)} = \frac{3k-1}{4k^2-1} R_0^2 \overline{C}_{4k}^{(\times)} + \frac{R_0^{k+2}}{k+1} \left[ R_0^{k+1} \overline{C}_{3k}^{(\times)} + k R_0^{k-1} I_k^{(\times)} + S_k^{(\times)}(R_0) \right], \quad (C55)$$

where

$$U'_{nm}(r) = \frac{(-1)^m \varepsilon}{2\omega} \operatorname{Im} \left\{ V_n^{/*}(r) \left[ W'_n(r) - \frac{W_n(r)}{r} \right] + V_n^*(r) \left[ W_n''(r) - \frac{W'_n(r)}{r} + \frac{W_n(r)}{r^2} \right] \right\}. \quad (C56)$$

Since  $\overline{C}_{1k}^{(\times)} = \overline{C}_{2k}^{(\times)} = 0$  and hence  $P_{kl}^{(\times)}(r) \equiv 0$ ,  $v_{E\theta}^{(\times)}$  and  $v_{E\phi}^{(\times)}$ , given by (C31) and (C32), are represented by using (D9) and (D16) as follows:

$$v_{E\theta}^{(\times)} = \operatorname{Re} \sum_{k=1}^{\infty} \sum_{l=-k}^k \frac{\Phi_{kl}^{(\times)}(r)}{r} \frac{\partial Y_k^l(\theta, \phi)}{\partial \theta} = \operatorname{Re} \sum_{k=1}^{\infty} \sum_{l=-k}^k \frac{\Phi_{kl}^{(\times)}(r)}{2r} \times \left[ \sqrt{k(k+1) - l(l+1)} Y_k^{l+1}(\theta, \phi) e^{-i\phi} - \sqrt{k(k+1) - l(l-1)} Y_k^{l-1}(\theta, \phi) e^{i\phi} \right], \tag{C57}$$

$$\begin{aligned} v_{E\phi}^{(\times)} &= \operatorname{Re} \sum_{k=1}^{\infty} \sum_{l=-k}^k \frac{il\Phi_{kl}^{(\times)}(r) Y_k^l(\theta, \phi)}{r \sin \theta} \\ &= -\operatorname{Re} \sum_{k=1}^{\infty} \sum_{l=-k}^k \frac{il\Phi_{kl}^{(\times)}(r) e^{i\phi}}{r} \sqrt{\frac{(2k+1)(k-l)!}{(k+l)!}} \\ &\quad \times \sum_{s=1}^{[(k-l+2)/2]} \sqrt{\frac{(2k-4s+3)(k+l-2s)!}{(k-l-2s+2)!}} Y_{k-2s+1}^{l-1}(\theta, \phi). \end{aligned} \tag{C58}$$

**Appendix D. Mathematical identities used in calculations**

In our derivation, the function  $Y_n^m(\theta, \phi)$  is defined by the following equations (Varshalovich *et al.* 1988):

$$Y_n^m(\theta, \phi) = \sqrt{\frac{(2n+1)(n-m)!}{4\pi(n+m)!}} e^{im\phi} P_n^m(\cos \theta), \quad 0 \leq m \leq n, \tag{D1}$$

$$P_n^m(\mu) = (-1)^m (1-\mu^2)^{m/2} \frac{d^m P_n(\mu)}{d\mu^m}, \quad m \geq 0, \tag{D2}$$

$$Y_n^{-m}(\theta, \phi) = (-1)^m Y_n^m(\theta, -\phi) = (-1)^m Y_n^{m*}(\theta, \phi), \tag{D3}$$

$$\int_0^{2\pi} d\phi \int_0^\pi d\theta \sin \theta Y_{n_1}^{m_1}(\theta, \phi) Y_{n_2}^{m_2*}(\theta, \phi) = \delta_{n_1 n_2} \delta_{m_1 m_2}, \tag{D4}$$

where  $P_n(\mu)$  is the Legendre polynomial of degree  $n$ ,  $P_n^m(\mu)$  is the associated Legendre polynomial of order  $m$  and degree  $n$ ,  $\mu = \cos \theta$ ,  $\delta_{nm}$  is the Kronecker delta, and the asterisk denotes the complex conjugate.

In the process of calculations, the following identities are used (Varshalovich *et al.* 1988):

$$\frac{\partial^2 Y_n^m(\theta, \phi)}{\partial \theta^2} + \cot \theta \frac{\partial Y_n^m(\theta, \phi)}{\partial \theta} = \frac{m^2 Y_n^m(\theta, \phi)}{\sin^2 \theta} - n(n+1) Y_n^m(\theta, \phi), \tag{D5}$$

$$\frac{dP_n(\mu)}{d\mu} = \sum_{k=1}^{[(n+1)/2]} (2n-4k+3) P_{n-2k+1}(\mu), \quad n \geq 1, \tag{D6}$$

$$\begin{aligned} &\int_0^{2\pi} d\phi \int_0^\pi d\theta \sin \theta Y_{n_1}^{m_1}(\theta, \phi) Y_{n_2}^{m_2}(\theta, \phi) Y_{n_3}^{m_3*}(\theta, \phi) \\ &= \sqrt{\frac{(2n_1+1)(2n_2+1)}{4\pi(2n_3+1)}} C_{n_1 0 n_2 0}^{n_3 0} C_{n_1 m_1 n_2 m_2}^{n_3 m_3}, \end{aligned} \tag{D7}$$

$$\sin \theta \frac{\partial Y_n^m(\theta, \phi)}{\partial \theta} = n C_{(n+1)m} Y_{n+1}^m(\theta, \phi) - (n+1) C_{nm} Y_{n-1}^m(\theta, \phi), \quad n \geq 1, \quad (\text{D8})$$

$$\begin{aligned} \frac{\partial Y_n^m(\theta, \phi)}{\partial \theta} &= \frac{1}{2} \sqrt{n(n+1) - m(m+1)} Y_n^{m+1}(\theta, \phi) e^{-i\phi} \\ &\quad - \frac{1}{2} \sqrt{n(n+1) - m(m-1)} Y_n^{m-1}(\theta, \phi) e^{i\phi}, \end{aligned} \quad (\text{D9})$$

$$\cos \theta Y_n^m(\theta, \phi) = C_{(n+1)m} Y_{n+1}^m(\theta, \phi) + C_{nm} Y_{n-1}^m(\theta, \phi), \quad (\text{D10})$$

where  $C_{nm}$  is defined by

$$C_{nm} = \sqrt{\frac{n^2 - m^2}{(2n-1)(2n+1)}}. \quad (\text{D11})$$

Here,  $[ \ ]$  means the integer part of an expression in brackets, and  $C_{n_1 m_1 n_2 m_2}^{n_3 m_3} = \langle n_1 m_1 n_2 m_2 | n_3 m_3 \rangle$  are the Clebsch–Gordan coefficients. The Clebsch–Gordan coefficients are zero unless the following conditions are satisfied:  $m_3 = m_1 + m_2$ ,  $n_1 + n_2 - n_3 \geq 0$ ,  $n_1 - n_2 + n_3 \geq 0$ ,  $-n_1 + n_2 + n_3 \geq 0$ ,  $|m_1| \leq n_1$ ,  $|m_2| \leq n_2$ ,  $|m_3| \leq n_3$ .

In our derivation, we use the fact that an arbitrary function  $f(\theta, \phi)$  can be expanded in spherical harmonics by

$$f(\theta, \phi) = \sum_{n=0}^{\infty} \sum_{m=-n}^n a_{nm} Y_n^m(\theta, \phi), \quad (\text{D12})$$

where the expansion coefficients are calculated by

$$a_{nm} = \int_0^{2\pi} d\phi \int_0^\pi d\theta \sin \theta Y_n^{m*}(\theta, \phi) f(\theta, \phi). \quad (\text{D13})$$

From (D13), by using (D3), one obtains

$$a_{n(-m)} = (-1)^m \left[ \int_0^{2\pi} d\phi \int_0^\pi d\theta \sin \theta Y_n^{m*}(\theta, \phi) f^*(\theta, \phi) \right]^*. \quad (\text{D14})$$

If  $f(\theta, \phi)$  is a real function, then it follows from (D14) that

$$a_{n(-m)} = (-1)^m a_{nm}^*. \quad (\text{D15})$$

With the help of (D1), (D2) and (D6), one obtains

$$\begin{aligned} \frac{Y_n^m(\theta, \phi)}{\sin \theta} &= \frac{1}{\sqrt{1-\mu^2}} \sqrt{\frac{(2n+1)(n-m)!}{4\pi(n+m)!}} e^{im\phi} (-1)^m (1-\mu^2)^{\frac{m}{2}} \frac{d^m P_n(\mu)}{d\mu^m} \\ &= -e^{i\phi} \sqrt{\frac{(2n+1)(n-m)!}{4\pi(n+m)!}} e^{i(m-1)\phi} (-1)^{m-1} (1-\mu^2)^{\frac{m-1}{2}} \frac{d^{m-1} P_n(\mu)}{d\mu^{m-1}} \left( \frac{dP_n(\mu)}{d\mu} \right) \end{aligned}$$

$$\begin{aligned}
 &= -e^{i\phi} \sqrt{\frac{(2n+1)(n-m)!}{4\pi(n+m)!}} e^{i(m-1)\phi} (-1)^{m-1} (1-\mu^2)^{\frac{m-1}{2}} \\
 &\quad \times \sum_{k=1}^{[(n+1)/2]} (2n-4k+3) \frac{d^{m-1} P_{n-2k+1}(\mu)}{d\mu^{m-1}} \\
 &= -e^{i\phi} \sqrt{\frac{(2n+1)(n-m)!}{(n+m)!}} \sum_{k=1}^{[(n-m+2)/2]} \sqrt{\frac{(2n-4k+3)(n+m-2k)!}{(n-m-2k+2)!}} \\
 &\quad \times Y_{n-2k+1}^{m-1}(\theta, \phi), \quad n, m \geq 1.
 \end{aligned} \tag{D16}$$

Let us expand  $Y_{n_1}^{m_1}(\theta, \phi) Y_{n_2}^{m_2*}(\theta, \phi)$  in spherical harmonics. According to (D12) and (D13), we obtain

$$Y_{n_1}^{m_1}(\theta, \phi) Y_{n_2}^{m_2*}(\theta, \phi) = \sum_{n=0}^{\infty} \sum_{m=-n}^n A_{nm}^{n_1 m_1 n_2 m_2} Y_n^m(\theta, \phi), \tag{D17}$$

where

$$A_{nm}^{n_1 m_1 n_2 m_2} = \int_0^{2\pi} d\phi \int_0^\pi d\theta \sin\theta Y_n^{m*}(\theta, \phi) Y_{n_1}^{m_1}(\theta, \phi) Y_{n_2}^{m_2*}(\theta, \phi). \tag{D18}$$

It follows from (D7) that

$$\begin{aligned}
 &\int_0^{2\pi} d\phi \int_0^\pi d\theta \sin\theta Y_n^{m*}(\theta, \phi) Y_{n_1}^{m_1}(\theta, \phi) Y_{n_2}^{m_2*}(\theta, \phi) \\
 &= \sqrt{\frac{(2n+1)(2n_2+1)}{4\pi(2n_1+1)}} C_{n0n_20}^{n_10} C_{nmn_2m_2}^{n_1m_1}.
 \end{aligned} \tag{D19}$$

This equation is non-zero only if  $m+m_2=m_1$  and  $|n_1-n_2| \leq n \leq n_1+n_2$ . Therefore,  $A_{nm}^{n_1 m_1 n_2 m_2}$  is calculated by

$$A_{nm}^{n_1 m_1 n_2 m_2} = \begin{cases} \sqrt{\frac{(2n+1)(2n_2+1)}{4\pi(2n_1+1)}} C_{n0n_20}^{n_10} C_{nmn_2m_2}^{n_1m_1}, & m = m_1 - m_2 \text{ and } |n_1 - n_2| \\ \leq n \leq n_1 + n_2, \\ 0, & m \neq m_1 - m_2 \\ \text{or } n < |n_1 - n_2| \text{ or } n > n_1 + n_2. \end{cases} \tag{D20}$$

Note that  $A_{nm}^{n_1 m_1 n_2 m_2}$  is real. It also follows from the properties of the Clebsch–Gordan coefficients that  $A_{nm}^{n_1 m_1 n_2 m_2} = 0$  unless  $|m_1| \leq n_1$ ,  $|m_2| \leq n_2$  and  $|m| \leq n$ . This fact should be kept in mind when implementing a numerical code.

The use of (D16) and (D17) gives the expansion

$$\frac{Y_{n_1}^{m_1}(\theta, \phi) Y_{n_2}^{m_2*}(\theta, \phi)}{\sin^2\theta} = \sum_{n=0}^{\infty} \sum_{m=-n}^n B_{nm}^{n_1 m_1 n_2 m_2} Y_n^m(\theta, \phi), \quad n_{1,2}, m_{1,2} \geq 1, \tag{D21}$$

where

$$\begin{aligned}
 B_{nm}^{n_1 m_1 n_2 m_2} &= \sqrt{\frac{(2n_1 + 1)(2n_2 + 1)(n_1 - m_1)!(n_2 - m_2)!}{(n_1 + m_1)!(n_2 + m_2)!}} \times \sum_{k_1=1}^{[(n_1 - m_1 + 2)/2]} \sum_{k_2=1}^{[(n_2 - m_2 + 2)/2]} \\
 &\times \sqrt{\frac{(2n_1 - 4k_1 + 3)(2n_2 - 4k_2 + 3)(n_1 + m_1 - 2k_1)!(n_2 + m_2 - 2k_2)!}{(n_1 - m_1 - 2k_1 + 2)!(n_2 - m_2 - 2k_2 + 2)!}} \\
 &\times A_{nm}^{(n_1 - 2k_1 + 1)(m_1 - 1)(n_2 - 2k_2 + 1)(m_2 - 1)}. \tag{D22}
 \end{aligned}$$

Note that  $B_{nm}^{n_1 m_1 n_2 m_2}$  is real. It should be emphasised that (D21) and (D22) are not valid if  $m_1 = 0$  or  $m_2 = 0$ . In our derivation, such terms vanish. However, in order to avoid problems in numerical simulations, one should specify  $B_{nm}^{n_1 m_1 n_2 m_2} = 0$  if  $m_1 = 0$  or  $m_2 = 0$ . It also follows from (D21) that  $B_{nm}^{n_1 m_1 n_2 m_2} = 0$  if  $|m_1| > n_1$  or  $|m_2| > n_2$  or  $|m| > n$ .

In order to transform the angle-dependent functions that appear in (B64), we apply the following equations.

With the help of (D16) and (D17), we obtain the identity

$$\begin{aligned}
 \frac{Y_{n_1}^{m_1}(\theta, \phi) Y_{n_2}^{m_2*}(\theta, \phi)}{\sin \theta} &= -\sqrt{\frac{(2n_1 + 1)(n_1 - m_1)!}{(n_1 + m_1)!}} \sum_{n=0}^{\infty} \sum_{m=-n}^n Y_n^m(\theta, \phi) e^{i\phi} \\
 &\times \sum_{k=1}^{[(n_1 - m_1 + 2)/2]} \sqrt{\frac{(2n_1 - 4k + 3)(n_1 + m_1 - 2k)!}{(n_1 - m_1 - 2k + 2)!}} \\
 &\times A_{nm}^{(n_1 - 2k + 1)(m_1 - 1)n_2 m_2}, \quad n_1, m_1 \geq 1. \tag{D23}
 \end{aligned}$$

The use of (D8) and (D21) gives

$$\begin{aligned}
 &\frac{1}{\sin \theta} \frac{\partial Y_{n_1}^{m_1}(\theta, \phi)}{\partial \theta} Y_{n_2}^{m_2*}(\theta, \phi) \\
 &= \sum_{n=0}^{\infty} \sum_{m=-n}^n \left[ n_1 C_{(n_1+1)m_1} B_{nm}^{(n_1+1)m_1 n_2 m_2} - (n_1 + 1) C_{n_1 m_1} B_{nm}^{(n_1-1)m_1 n_2 m_2} \right] Y_n^m(\theta, \phi). \tag{D24}
 \end{aligned}$$

Let us expand  $Y_{n_1}^{m_1}(\theta, \phi) Y_{n_2}^{m_2}(\theta, \phi)$  in spherical harmonics. According to (D12) and (D13), we obtain

$$Y_{n_1}^{m_1}(\theta, \phi) Y_{n_2}^{m_2}(\theta, \phi) = \sum_{k=0}^{\infty} \sum_{l=-k}^k D_{kl}^{n_1 m_1 n_2 m_2} Y_k^l(\theta, \phi), \tag{D25}$$

$$D_{kl}^{n_1 m_1 n_2 m_2} = \int_0^{2\pi} d\phi \int_0^\pi d\theta \sin \theta Y_k^{l*}(\theta, \phi) Y_{n_1}^{m_1}(\theta, \phi) Y_{n_2}^{m_2}(\theta, \phi). \tag{D26}$$

$$D_{kl}^{n_1 m_1 n_2 m_2} = \sqrt{\frac{(2n_1 + 1)(2n_2 + 1)}{4\pi(2k + 1)}} C_{n_1 0 n_2 0}^{k0} C_{n_1 m_1 n_2 m_2}^{kl}. \tag{D27}$$

The coefficients  $D_{kl}^{n_1 m_1 n_2 m_2}$  are non-zero only if the following conditions are satisfied:  $l = m_1 + m_2$ ,  $|n_1 - n_2| \leq k \leq n_1 + n_2$ ,  $|m_1| \leq n_1$ ,  $|m_2| \leq n_2$ ,  $|l| \leq k$ .

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