



# Physics of turbulent flow : exercises

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**<http://acoustique.ec-lyon.fr>**

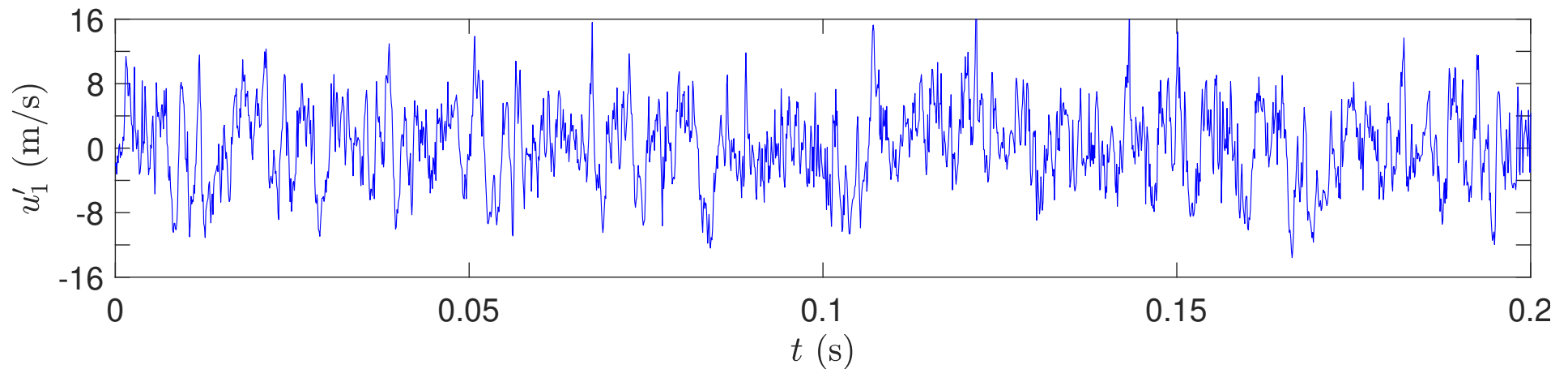
● **Fluctuating velocity signal in the shear layer of a subsonic round jet**

(measured by crossed-wire probes at  $x_1 = 2D$ ,  $x_2 = D/2$ ,  $x_3 = 0$ )

Nozzle diameter  $D = 50$  mm, exit velocity  $U_j = 30$  m.s<sup>-1</sup>

↷ Reynolds number  $Re_D = 10^5$

$u'_1(t)$

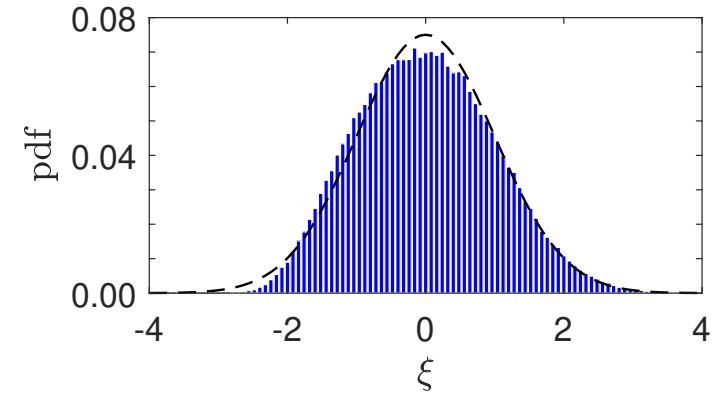
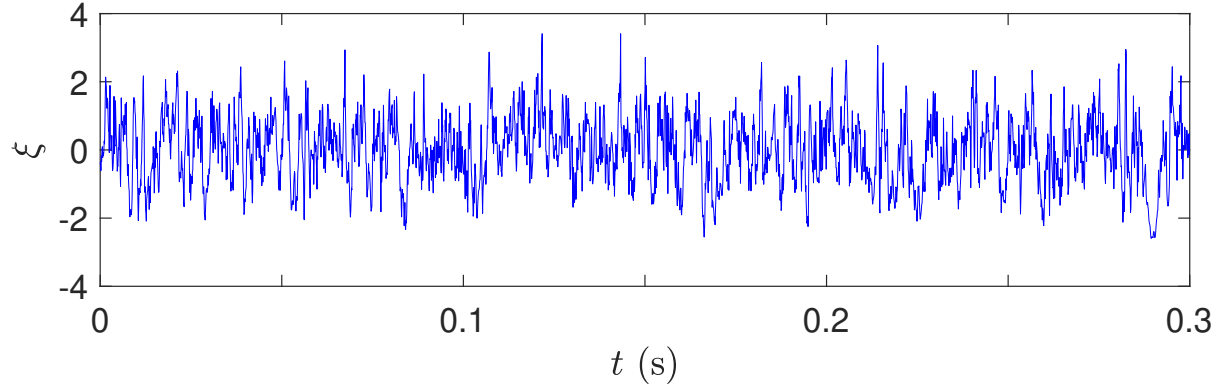


Courtesy of Emmanuel Jondeau (LMFA) for the data

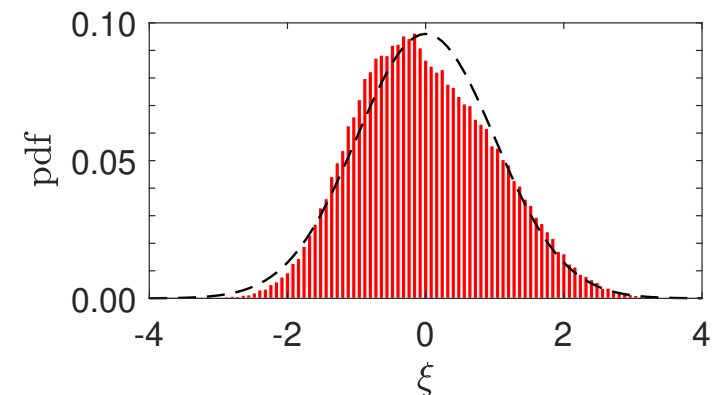
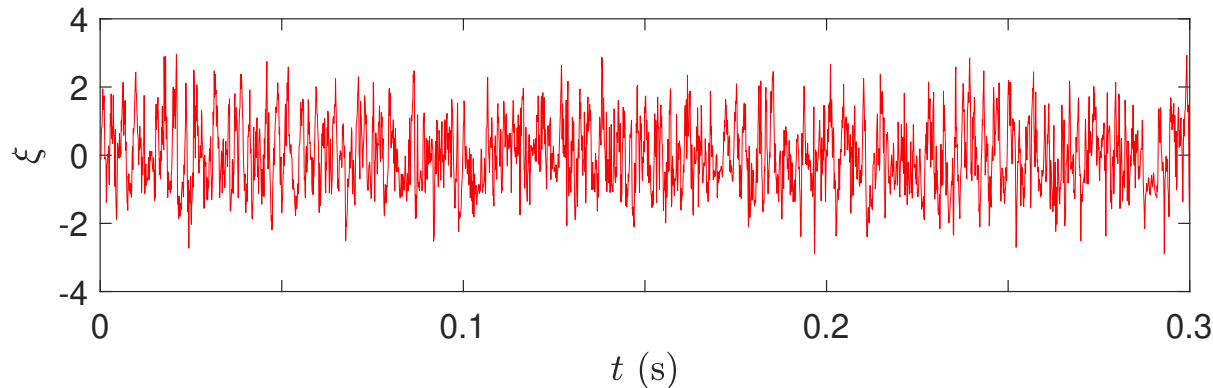
● **Fluctuating velocity signal in the shear layer of a jet (cont.)**

$u'_1(t)$  and  $u'_2(t)$  with  $\xi = u'_\alpha(t)/u_{\alpha rms}$

$S_{u_1} \simeq 0.21$        $T_{u_1} \simeq 2.74$



$S_{u_2} \simeq 0.24$        $T_{u_2} \simeq 2.76$



Interpretation?

● **Probability density function (pdf)**

For a centered variable  $x'_i \equiv x_i - \bar{X}_i$  of root-mean-square deviation  $x'_{i,rms} = \sigma_{x_i}$ , the **skewness**  $S$  and the **flatness or kurtosis**  $T$  factors are defined by

$$S_{x_i} \equiv \frac{\overline{x_i'^3}}{x_{i,rms}^3} \qquad T_{x_i} \equiv \frac{\overline{x_i'^4}}{x_{i,rms}^4}$$

Skewness is a measure of the asymmetry of the pdf about its mean, and flatness is a measure of the tailedness of the pdf.

The reference is the **Gaussian (normal) distribution**, the pdf is

$$p(\xi) = \frac{1}{\sqrt{2\pi}\sigma_{x_i}} \exp\left(-\frac{\xi^2}{2\sigma_{x_i}^2}\right) \qquad x'_{i,rms} = \sigma_{x_i} \qquad S_{x_i} = 0 \qquad T_{x_i} = 3$$

$$1 = \int_{-\infty}^{+\infty} p(\xi) d\xi \qquad \overline{x_i'^n} = \int_{-\infty}^{+\infty} \xi^n p(\xi) d\xi$$

● Probability density function (cont.)

$$\int_{\xi_1}^{\xi_2} p(\xi) d\xi = \frac{\text{nbr of expts in which } \xi_1 \leq x'_i \leq \xi_2}{\text{total number of expts}}$$

● Reynolds stress tensor in the shear layer

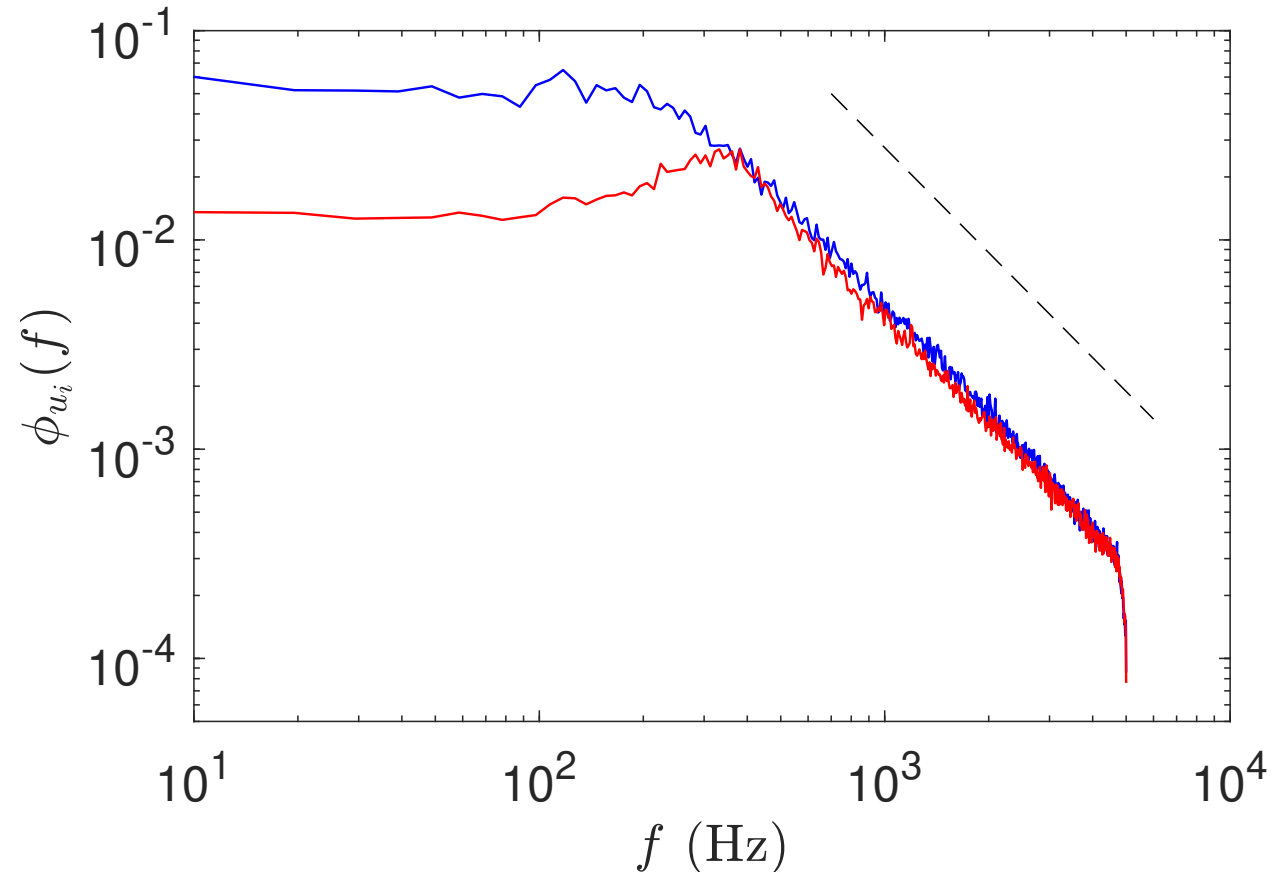
$$\frac{\sqrt{|u'_i u'_j|}}{U_j} \simeq \begin{pmatrix} 0.18 & 0.10 & 0.10 \\ 0.10 & 0.14 & - \\ 0.10 & - & 0.13 \end{pmatrix}$$

- $\overline{u'_1 u'_2} > 0$ , in agreement with Boussinesq's hypothesis  
 $-\overline{u'_1 u'_2} = \nu_t \partial \overline{U}_1 / \partial x_2$  (okay, at least for the sign!)
- The Schwarz inequality is (must be!) satisfied,  
 $|\overline{u'_1 u'_2}|^2 \leq \overline{u'^2_1} \times \overline{u'^2_2}$
- Turbulence intensity  $u'_{1,\text{rms}}/U_j \simeq 0.18$

● Spectra of  $u'_1$  and  $u'_2$

$f_s = 1/\Delta t = 10^4$  Hz,  $n_{\text{fft}} = 1024$ ,  $\Delta f = f_s/n_{\text{fft}}$ ,  $f_{\text{max}} = f_s/2 = 5$  kHz

( $l_\eta \simeq 2.4 \times 10^{-5}$  m,  $f_\eta = 2.6 \times 10^4$  Hz)



$$\int_0^\infty \phi_{u_1}(f) df = u_{u_1, \text{rms}}'^2 \quad (\text{Parseval})$$

● Spectra of  $u'_1$  and  $u'_2$

```
%.. number of points for the Fourier transform
nfft = 1024;

dt = t(2)-t(1);
fs = 1./dt;

%.. Power spectral density
window = ones(nfft,1);
noverlap = nfft/2;

[PSDu f] = pwelch(u,window,noverlap,nfft,1./dt);
PSDu_int = trapz(f,PSDu);

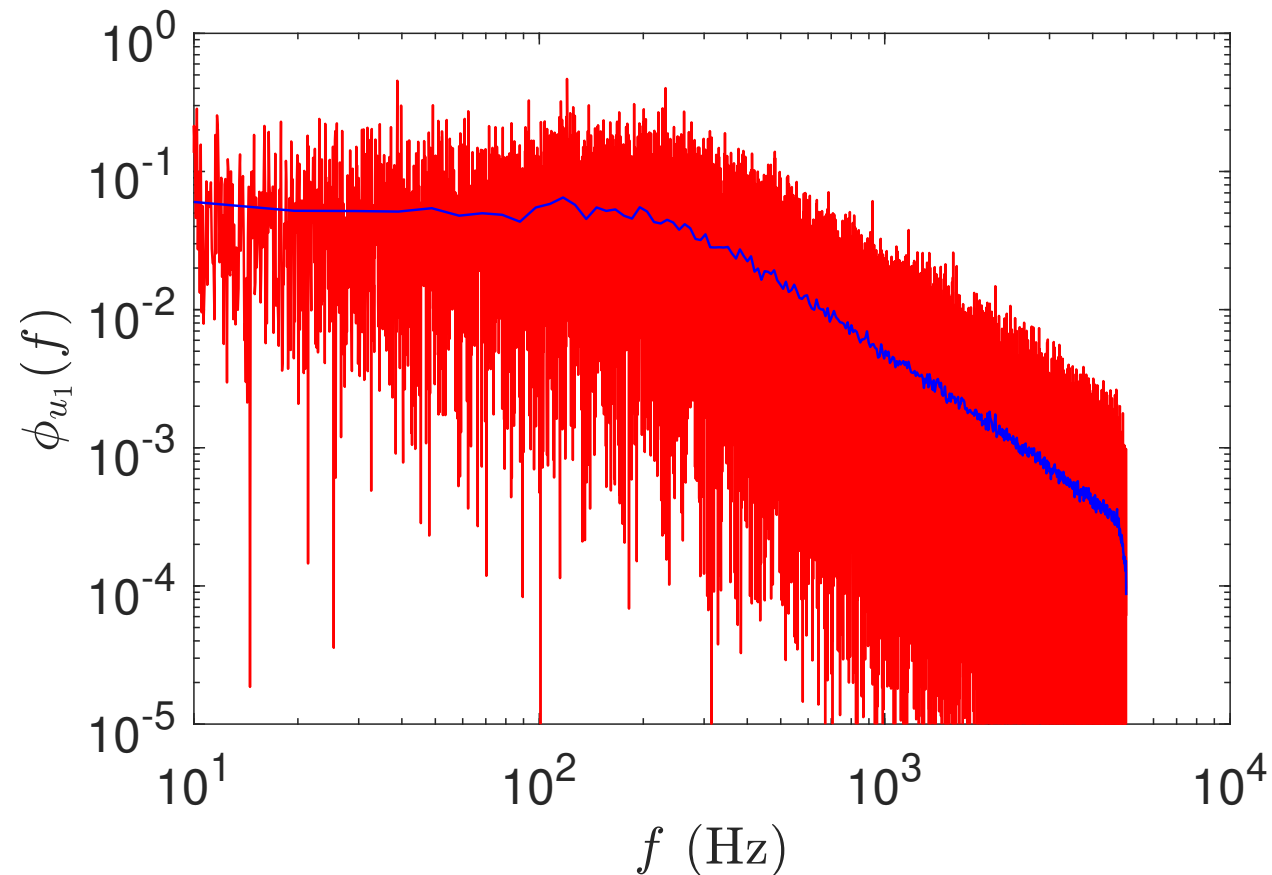
disp(['PSD - Welch E = ',num2str(PSDu_int)]);
disp(['df = ',num2str(1/(nfft*dt)), ' fmax = ',num2str(1/(2*dt))]);
```



● Do not confuse a single fft and the power spectral density estimation

FFT<sup>2</sup> of  $u_1'(t)$  over  $n_{\text{fft}} = 150000$  points (with all the signal points)

FFT<sup>2</sup>  $\neq$  PSD power spectral density  $\phi_{u_1 u_1}(f)$ !



● **Power spectral density for a stationary random process**

(signal of infinite energy)

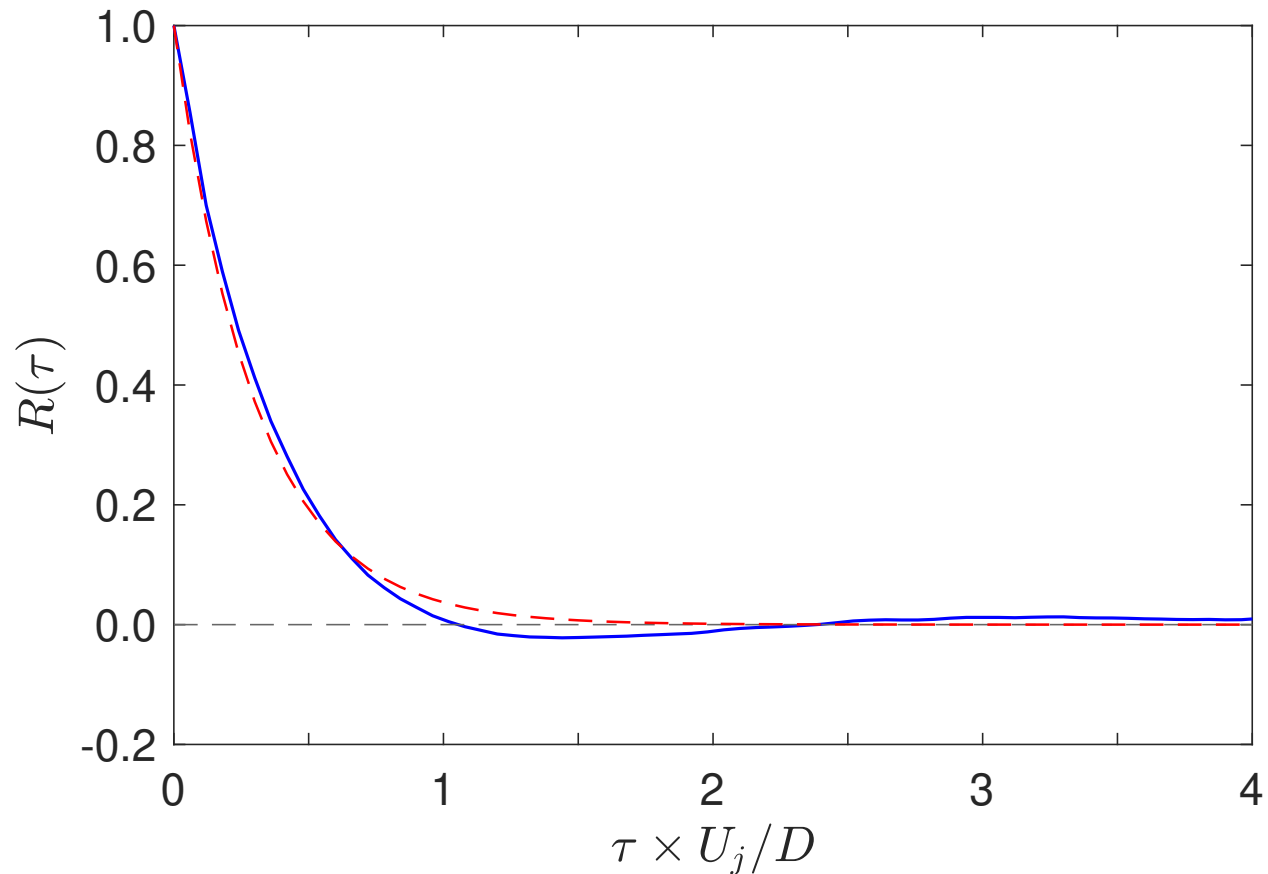
Fourier transform calculated for a truncated signal of duration  $T$   
 $\hat{u}_1(f, k)$  is the DFT of  $u_1(t)$  for the  $k$ -th block,  $n_K$  block averages

One-sided power spectral density ( $f > 0$ )

$$\phi_{u_1}(f) = \lim_{T \rightarrow \infty} \frac{2}{T} E \left[ \hat{u}_1^*(f, k) \hat{u}_1(f, k) \right] \simeq \frac{2}{n_K T} \sum_{k=1}^{n_K} \hat{u}_1^*(f, k) \hat{u}_1(f, k)$$

$$\int_0^{\infty} \phi_{u_1}(f) df = u_{u_1, \text{rms}}'^2 \quad (\text{Parseval})$$

● Autocorrelation function of  $u'_1$



$$R(\tau) = \frac{\overline{u'_1(t)u'_1(t + \tau)}}{u'_{1\text{rms}}{}^2}$$

—  $R(\tau)$

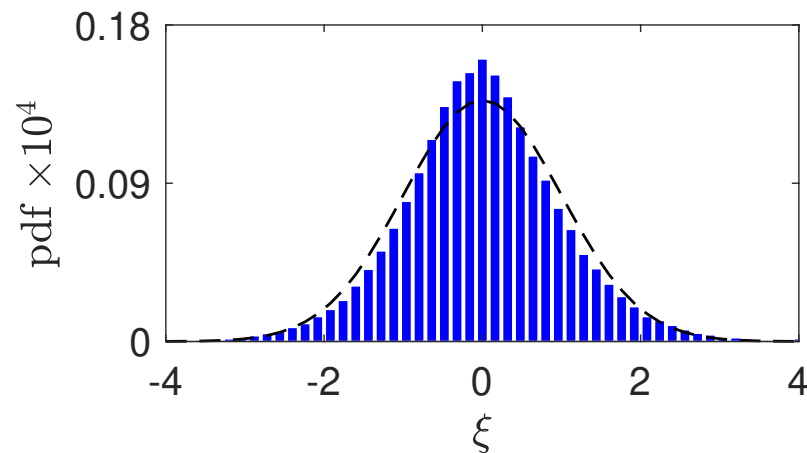
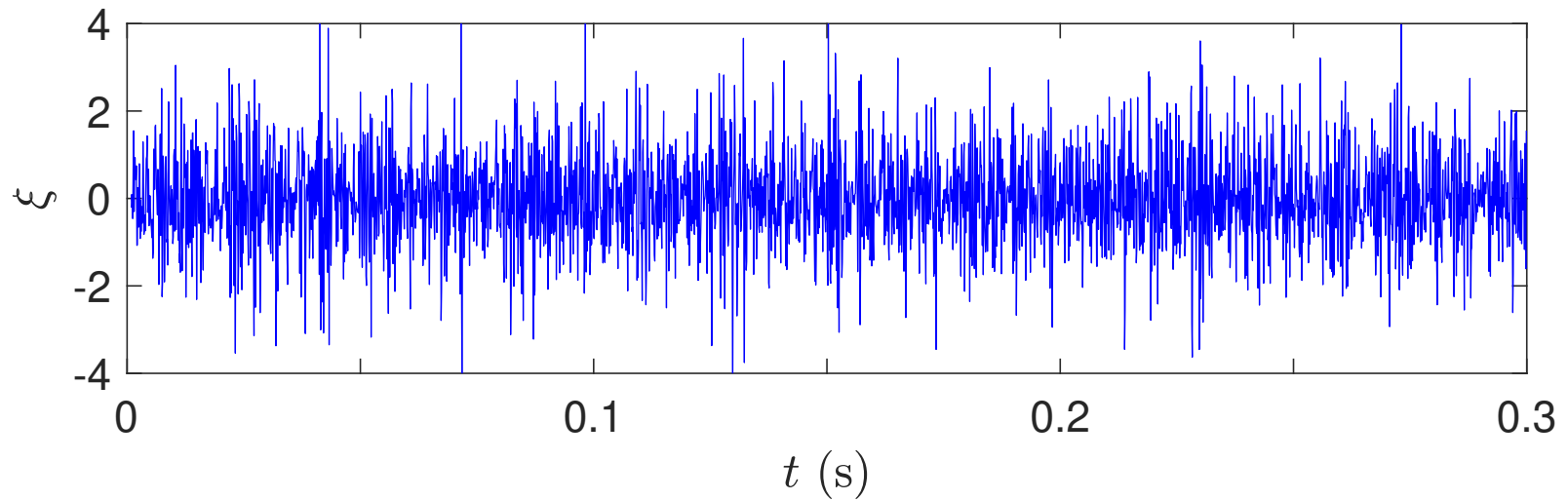
---  $\exp(-\tau/\Theta)$

$$\Theta = \int_0^{\tau^*} R(\tau) d\tau$$

$\Theta \simeq 5 \times 10^{-4}$  s,  $\Theta \simeq 0.3D/U_j$  (the integral time  $\Theta$  is not the turbulence lifetime)  
 and the corresponding integral space length  $L_f \simeq \overline{U}_1 \times \Theta \simeq 1.5 \times 10^{-2}$  m

● Time derivative of  $u'_1$

$$\xi = \partial_t u'_1 / \partial_t u'_1 \Big|_{\text{rms}} \quad S_{\partial_t u'_1} \simeq 0.07 \quad T_{\partial_t u'_1} \simeq 4.03$$



● **Spectrum of  $du'_1/dt$**

can be computed from the signal  $du'_1/dt$  (using a finite difference scheme, e.g. 11-pt stencil, 4th order),

can be directly obtained from the spectrum of  $u'_1$  using  $\phi_{\partial_t u'_1}(f) = (2\pi f)^2 \phi_{u'_1}(f)$

